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August 14, 2024

**BY ELECTRONIC FILING**

Hon. Bernard J. Logan, Clerk  
State Corporation Commission  
Tyler Building, 1st Floor  
1300 East Main Street  
Richmond, VA 23219

**Re: Application of Virginia Electric and Power Company for Approval and Certification of Electric Transmission Facilities: Aquia Harbour – Possum Point Lines #29, #252, #2083, and #568 Rebuild – Case No. PUR-2024-00142.**

Dear Mr. Logan:

Please find enclosed for electronic filing in the above-captioned proceeding the application for approval of electric facilities on behalf of Virginia Electric and Power Company (the “Company”). This filing contains the Application, Appendix, Direct Testimony, and DEQ Supplement, including attachments.

As indicated in Section II.A.12.b of the Appendix, electronic copies of the Virginia Department of Transportation “General Highway Map” for Stafford County, Prince William County, and the City of Fredericksburg, as well as the digital geographic information system (“GIS”) map required by Va. Code § 56-46.1, which is Attachment II.A.2 to the Appendix, were provided via an e-room to the Commission’s Division of Public Utility Regulation.

If you have any questions or need further information, please feel free to contact us.

Sincerely,

Andrew J. Flavin



Timothy L. McHugh



Enclosures

cc: William H. Chambliss, Esq.  
Mr. David Essah (without enclosures)  
Mr. Neil Joshipura (without enclosures)  
Mr. Michael A. Cizenski (without enclosures)  
David J. DePippo, Esq.  
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William H. Smith, III, Esq.



# Dominion Energy®

Application, Appendix,  
DEQ Supplement, Direct  
Testimony and Exhibits of  
Virginia Electric and Power  
Company

Before the State Corporation  
Commission of Virginia

Aquia Harbour – Possum Point  
Lines #29, #252, #2083, and  
#568 Rebuild

Application No. 339

Case No. PUR-2024-00142

Filed: August 14, 2024

Volume 1 of 2



COMMONWEALTH OF VIRGINIA  
BEFORE THE  
STATE CORPORATION COMMISSION

APPLICATION OF  
VIRGINIA ELECTRIC AND POWER COMPANY  
FOR APPROVAL AND CERTIFICATION  
OF ELECTRIC TRANSMISSION FACILITIES

Aquia Harbour – Possum Point  
Lines #29, #252, #2083, and #568 Rebuild

Application No. 339

Case No. PUR-2024-00142

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COMMONWEALTH OF VIRGINIA  
STATE CORPORATION COMMISSION

APPLICATION OF	)	
	)	
VIRGINIA ELECTRIC AND POWER	)	Case No. PUR-2024-00142
COMPANY	)	
	)	
For approval and certification of electric	)	
transmission facilities: Aquia Harbour –	)	
Possum Point Lines #29, #252, #2083,	)	
and #568 Rebuild	)	

**APPLICATION OF VIRGINIA ELECTRIC AND POWER COMPANY  
FOR APPROVAL AND CERTIFICATION OF  
ELECTRIC TRANSMISSION FACILITIES:  
AQUIA HARBOUR – POSSUM POINT  
LINES #29, #252, #2083, AND #568 REBUILD**

Pursuant to § 56-46.1 of the Code of Virginia (“Va. Code”) and the Utility Facilities Act, Va. Code §§ 56-265.1 *et seq.*, Virginia Electric and Power Company (“Dominion Energy Virginia” or the “Company”), by counsel, files with the State Corporation Commission of Virginia (the “Commission”) this application for approval and certification of electric transmission facilities (the “Application”). In support of its Application, Dominion Energy Virginia respectfully shows as follows:

1. Dominion Energy Virginia is a public service corporation organized under the laws of the Commonwealth of Virginia furnishing electric service to the public within its Virginia service territory. The Company also furnishes electric service to the public in portions of North Carolina. Dominion Energy Virginia's electric system—consisting of facilities for the generation, transmission, and distribution of electric energy—is interconnected with the electric systems of neighboring utilities and is a part of the interconnected network of electric systems serving the continental United States. By reason of its operation in two states and its interconnections with other utilities, the Company is engaged in interstate commerce.

2. In order to perform its legal duty to furnish adequate and reliable electric service, Dominion Energy Virginia must, from time to time, replace existing transmission facilities or construct new transmission facilities in its system.

3. In this Application, in order to: (a) maintain the structural integrity and reliability of the networked transmission system; (b) resolve identified violations of the mandatory North American Electric Reliability Corporation (“NERC”) Reliability Standards; and (c) provide for future load growth in the Woodbridge Load Area, Virginia Electric and Power Company (“Dominion Energy Virginia” or the “Company”) proposes, in Stafford County, Prince William County, and the City of Fredericksburg, to rebuild its existing transmission corridor between Fredericksburg Substation and Possum Point Switching Station by:

- Rebuilding, primarily within existing right-of-way or on Company-owned property, approximately 11.4 miles of the existing Fredericksburg-Possum Point 115 kilovolt (“kV”) Line #29<sup>1</sup> on double circuit monopole structures utilizing current 230 kV standards, from the Company’s existing Aquia Harbour Switching Station<sup>2</sup> (“Aquia Harbour Station”) to Structure #29/1850, and then 0.5 mile from Structure #29/1850 to the Company’s existing Possum Point Station 230 kV switchyard.
- Removing approximately 0.6 mile of 115 kV Line #29 from Structure #29/1850 to the Possum Point Station 115 kV switchyard.
- Rebuilding a 0.2 mile segment of Line #29, between Structure #29/1835 and the Company’s existing Fuller Road Substation, using an additional 50 feet of right-of-way.
- Rebuilding, primarily within existing right-of-way or on Company-owned property, approximately 11.4 miles of the existing Aquia Harbour-Possum Point 230 kV Line #252, on double circuit monopole structures utilizing current 230 kV standards, from Aquia Harbour Station to Structure #252/5583, and then 0.5 mile from Structure #252/5583 to the Company’s Possum Point Station 230 kV switchyard.
- Rebuilding a 0.2 mile segment of Line #252 between Structure #252/5568 and Fuller

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<sup>1</sup> The segments of Line #29 that will be rebuilt as part of the Rebuild Project will be renamed to Line #2309.

<sup>2</sup> This Appendix discusses two different facilities with similar names: the Aquia Harbour Switching Station and the Aquia Substation. Both are discussed in detail in Section I.C.

Road Substation using an additional 50 feet of right-of-way.<sup>3</sup>

- Relocating and rebuilding, entirely within existing right-of-way or on Company-owned property, approximately 6.8 miles of the existing Ladysmith-Possum Point 500 kV Line #568 on single circuit monopole structures, between Aquia Harbour Station and Possum Point Station.
- Rebuilding, entirely within existing right-of-way or on Company-owned property, approximately 0.7 mile of 230 kV Fredericksburg-Birchwood Non-Utility Generator (“NUG”) Line #2083 on double circuit monopole structures (with vacant arms) between the Company’s Fredericksburg Substation and Mary Washington Boulevard and Hospital Drive (“Hospital Junction”), located within the City of Fredericksburg.

(collectively, the “Rebuild Project”).<sup>4</sup>

4. The Rebuild Project will replace aging infrastructure that is at the end of its service life to comply with the Company’s mandatory electric transmission planning criteria (the “Planning Criteria”), thereby enabling the Company to maintain the overall long-term reliability of its transmission system. Specifically, Lines #29 and Line #252 between Aquia Harbour Station and Possum Point Station 115 kV and 230 kV switchyards were constructed in in 1978 mostly on

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<sup>3</sup> The Company further proposes to rebuild the existing 0.1 mile segment of Lines #252 and #29 northwest of Fuller Road Substation using additional right-of-way that increases linearly to form a triangular area of additional right-of-way. Starting at Structure #252/5566 (#29/1833), there is no additional right-of-way. As Lines #252 and #29 travel east, the right-of-way will expand to include up to an additional 67 feet of width at the eastern edge of Mars Station Road.

<sup>4</sup> The Rebuild Project is the second phase of the work the Company plans to undertake as described in its Application filed on March 14, 2024, in Case No. PUR-2024-00035, *Application of Virginia Electric and Power Company for Approval and Certification of Electric Facilities: Fredericksburg-Aquia Harbour Lines #29, #2104, and #2157 Partial Rebuild*.

The Company will also perform work associated with the Rebuild Project at the Fredericksburg, Cranes Corner, Aquia, Ladysmith, and Fuller Road Substations, and Possum Point and Aquia Harbour Stations. This work, while not included as part of the Rebuild Project, is discussed in Section II.C (the Cranes Corner work is discussed immediately below). Additionally, the Company intends to add one backbone structure outside of the Company’s Cranes Corner Substation in the existing right-of-way to maximize capacity and minimize line crossings in the corridor. Finally, the Company intends to install approximately 0.3 mile of a new 115 kV line starting at the Fuller Road Substation to feed Marine Corps Base Quantico (“MCBQ”) once the entire corridor has been upgraded to 230 kV. The Company’s work associated with the relocation of the backbone structure at Cranes Corner Substation and the new 0.3 mile 115 kV line to feed MCBQ are not components of the Rebuild Project. The Company considers this work to qualify as an “ordinary extension[] or improvement[] in the usual course of business (*i.e.*, “ordinary course”) pursuant to § 56-265.2 A 1 of the Code of Virginia (“Va. Code”) and, therefore, does not require approval pursuant to Va. Code § 56-46.1 B or a CPCN from the Commission. Because this work is not a component of the proposed Rebuild Project, the costs associated with this work are not included in the total Rebuild Project costs.

wooden steel tower structures and on some wooden H-frame or 3-pole structures that are approaching the end of their useful life based on industry standards, which are 35–55 years for wood structures and 40-60 years for COR-TEN<sup>®</sup> steel structures.

5. The Rebuild Project is also needed to comply with mandatory NERC Reliability standards. The 2026 PJM Interconnection, L.L.C. (“PJM”) Regional Transmission Expansion Plan (“RTEP”) Analysis identified that an N-1-1 loss of Lines #252 and #2157 between Fredericksburg and Cranes Corner Substation will drop more than 300 megawatts (“MW”) of load in the Fredericksburg to Possum Point transmission corridor (“F2PPC”), resulting in a NERC criteria violation. To mitigate the potential violation, a new 230 kV source is required in the corridor to split the load. The proposed solution, which was awarded to Dominion Energy Virginia through PJM’s 2021 competitive Reliability Open Window, is to convert Line #29 from 115 kV to 230 kV operation. The Rebuild Project implements this proposed solution from Aquia Harbour Station to Possum Point Station by rebuilding Line #29 utilizing current 230 kV standards.

6. Finally, the Rebuild Project is needed so that the Company can continue to provide reliable service for the significant load growth anticipated in the area. In 2023, the Company received multiple Delivery Point (“DP”) requests in the transmission corridor between the Company’s Fredericksburg Substation and Possum Point Station associated with new data center developments. The Company’s Load-Serving Entity (“Dom LSE” or “Dominion Distribution”) submitted DP requests to either interconnect or evaluate the feasibility of interconnection for at least ten new substations in the F2PPC. Dom LSE also received customer load requests that would necessitate (i) 13 new substations in the corridor south of Fredericksburg Substation and (ii) three new substations east of the F2PPC. To

accommodate this rapidly growing load, the Company proposes to rebuild the following lines in the corridor—Lines #29, #252, and #2083—on double circuit monopole structures.<sup>5</sup> In addition, to optimize space in the right-of-way for an additional circuit, the Company proposes to relocate and rebuild Line #568 on single circuit monopole structures approximately 50 feet to the east.

7. By replacing the single circuit structures for Lines #29, #252, and #2083 with double circuit structures during the corridor’s scheduled rebuild, the Company will be able to accommodate imminent load growth. Without the additional circuits installed as part of the Rebuild Project, the Company would have to replace some or all of these facilities in the near term to add transmission lines to support regional growth. Moreover, installing new conductors as part of the Rebuild Project allows the Company to reduce costs, outages, and impacts to environmental, historical, and cultural resources. The ability to energize a future 230 kV circuit to accommodate the significant load growth preserves the option to address future reliability issues and is consistent with prudent utility planning for the future.

8. Except for the 0.2 mile segment of Lines #29 and #252 between Structure #29/1835 (#252/5568) and Fuller Road Substation, and the 0.1 mile segment west of Fuller Road Substation, the Rebuild Project, spanning approximately 24.5 miles, will primarily be located on existing transmission line right-of-way or on Company-owned property.<sup>6</sup> Given the availability of existing rights-of-way and the statutory preference to use of existing rights-of-way, and because additional costs and environmental impacts would be associated with the acquisition and construction of new

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<sup>5</sup> Lines #29, #252, and #2083 currently use single circuit structures.

<sup>6</sup> For a complete discussion of the additional 0.2 mile of 50-foot right-of-way and 0.1 mile of 67-foot right-of-way, see Section II.A.4 of the Appendix.

rights-of-way, the Company did not consider any alternate routes requiring new rights-of-way for this Rebuild Project.

9. The desired in-service target date for the Rebuild Project is January 31, 2029. The Company estimates it will take approximately 46 months after a final order from the State Corporation Commission (“Commission”) for detailed engineering, materials procurement, permitting, real estate, and construction of the Rebuild Project. Accordingly, to support this estimated construction timeline and construction plan, the Company respectfully requests a final order by February 28, 2025. Should the Commission issue a final order by February 28, 2025, the Company estimates that construction should begin in March 2026 with the Rebuild Project to be completed by the in-service target date of January 31, 2029. This schedule is contingent upon obtaining the necessary permits and careful coordination of outages, the latter of which may be particularly challenging due to the amount of new load growth, rebuilds, and new builds scheduled to occur in this load area. Dates may need to be adjusted based on permitting delays or design modifications to comply with additional agency requirements identified during the permitting application process, as well as the ability to schedule outages, and unpredictable delays due labor shortages or materials/supply issues. Based on the Rebuild Project’s complexity, there may be delays with procurement of materials.

10. Any adjustments to the Rebuild Project schedule resulting from these or similar challenges could necessitate a minimum of a six- to twelve-month delay in the targeted in-service date. Accordingly, for purposes of judicial economy, the Company requests that the Commission issue a final order approving both a desired in-service target date (*i.e.*, December 31, 2029) and an authorization sunset date (*i.e.*, January 31, 2030) for energization of the Rebuild Project.

11. In addition, the Company is actively monitoring regulatory changes and requirements associated with the Northern Long Eared Bat (“NLEB”) and how it could potentially impact construction timing associated with time of year restrictions (“TOYRs”). The U.S. Fish and Wildlife Service (“USFWS”) previously indicated that it planned to issue final NLEB guidance to replace the interim guidance by April 1, 2024; however, the interim guidance has been extended by USFWS until late summer 2024. In the meantime, the USFWS issued several draft guidance documents for public review and comment. The Company actively is tracking updates from the USFWS with respect to the final guidance. Once issued, the Company plans to review and follow the final guidance to the extent it applies to the Company’s projects. Until the final guidance is issued, the Company will continue following the interim guidance. For projects that may require additional coordination, the Company will coordinate with the USFWS. The Company is also continuing to track potential regulatory changes associated with the potential up-listing of the Tricolored bat (“TCB”). On September 14, 2022, the USFWS published the proposed rule to the Federal Register to list the TCB as endangered under the Endangered Species Act (“ESA”). On April 1, 2024, the USFWS issued draft guidance for the NLEB and TCB for public review and comment. The USFWS also recently extended its Final Rule issuance target from September 2023 to September 2024. The Company is actively tracking this ruling and evaluating the effects of potential outcomes on Company projects’ permitting, construction, and in-service dates, including electric transmission projects.

12. The estimated conceptual cost of the Rebuild Project is approximately \$205.5 million (in 2024 dollars).



13. The proposed Rebuild Project will afford the best means of meeting the continuing need for reliable service while reasonably minimizing adverse impact on the scenic, environmental, and historic assets of the area.

14. Based on consultations with the Virginia Department of Environmental Quality (“DEQ”), the Company has developed a supplement (“DEQ Supplement”) containing information designed to facilitate review and analysis of the proposed facilities by the DEQ and other relevant agencies. The DEQ Supplement is attached to this Application.

15. Based on the Company’s experience, the advice of consultants, and a review of published studies by experts in the field, the Company believes that there is no causal link to harmful health or safety effects from electric and magnetic fields generated by the Company’s existing or proposed facilities. Section IV of the Appendix provides further details on Dominion Energy Virginia’s consideration of the health aspects of electric and magnetic fields.

16. Section V of the Appendix provides a proposed route description for public notice purposes and a list of federal, state, and local agencies and officials that the Company has notified or will notify about the Application.

17. In addition to the information provided in the Appendix and the DEQ Supplement, this Application is supported by the pre-filed direct testimony of Company Witnesses Mark R. Gill, Rebecca A. O’Neal, Brian Obermeier, and Blair Parks filed with this Application.

18. Because this Application seeks approval to rebuild existing lines primarily within existing right-of-way or Company-owned property, the Company respectfully requests, in the interest of judicial economy, that the Commission issue an Order for Notice and Comment setting forth a procedural schedule in this proceeding without a scheduled evidentiary hearing, but with an opportunity for interested persons to request an evidentiary hearing if the issues raised cannot be

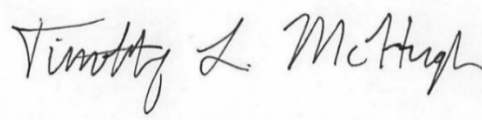
addressed adequately without a hearing. An Order for Notice and Comment will still allow the Company, Commission Staff, and any interested parties that join the proceeding to develop a complete record without prejudice, as Commission Staff or any party may file with the Commission a request for hearing.

WHEREFORE, Dominion Energy Virginia respectfully requests that the Commission:

- a) direct that notice of this Application be given as required by Va. Code § 56-46.1;
- b) approve pursuant to Va. Code § 56-46.1 the construction of the Rebuild Project; and
- c) grant a certificate of public convenience and necessity for the Rebuild Project under the Utility Facilities Act, Va. Code §§ 56-265.1, *et seq.*, by February 28, 2025, if possible.

**VIRGINIA ELECTRIC AND POWER COMPANY**

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Aquia Harbour – Possum Point  
Lines #29, #252, #2083, and #568 Rebuild

Application No. 339

Appendix

Containing Information in Response to  
“Guidelines for Transmission Line Applications Filed Under Title 56 of the Code of Virginia”

Case No. PUR-2024-00142

Filed: August 14, 2024

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## EXECUTIVE SUMMARY

In order to: (a) maintain the structural integrity and reliability of the networked transmission system; (b) resolve identified violations of the mandatory North American Electric Reliability Corporation (“NERC”) Reliability Standards; and (c) provide for future load growth in the Woodbridge Load Area, Virginia Electric and Power Company (“Dominion Energy Virginia” or the “Company”) proposes, in Stafford County, Prince William County, and the City of Fredericksburg, to rebuild its existing transmission corridor between Fredericksburg Substation and Possum Point Switching Station<sup>1</sup> by:

- (i) Rebuilding, primarily within existing right-of-way or on Company-owned property, approximately 11.4 miles of the existing Fredericksburg-Possum Point 115 kilovolt (“kV”) Line #29<sup>2</sup> on double circuit monopole structures utilizing current 230 kV standards, from the Company’s existing Aquia Harbour Switching Station<sup>3</sup> (“Aquia Harbour Station”) to Structure #29/1850, and then 0.5 mile from Structure #29/1850 to the Company’s existing Possum Point Station 230 kV switchyard.
- (ii) Removing approximately 0.6 mile of 115 kV Line #29 from Structure #29/1850 to the Possum Point Station 115 kV switchyard.
- (iii) Rebuilding a 0.2 mile segment of Line #29, between Structure #29/1835 and the Company’s existing Fuller Road Substation, using an additional 50 feet of right-of-way.
- (iv) Rebuilding, primarily within existing right-of-way or on Company-owned property, approximately 11.4 miles of the existing Aquia Harbour-Possum Point 230 kV Line #252, on double circuit monopole structures utilizing current 230 kV standards, from Aquia Harbour Station to Structure #252/5583, and then 0.5 mile from Structure #252/5583 to the Company’s Possum Point Station 230 kV switchyard.
- (v) Rebuilding a 0.2 mile segment of Line #252 between Structure #252/5568 and Fuller Road Substation using an additional 50 feet of right-of-way.<sup>4</sup>

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<sup>1</sup> The Possum Point Switching Station is located on the Company’s Possum Point Power Station parcel and contains the 115 kV and 230 kV switchyards (the “Possum Point Switching Station” or “Possum Point Station”).

<sup>2</sup> The segments of Line #29 that will be rebuilt as part of the Rebuild Project will be renamed to Line #2309.

<sup>3</sup> This Appendix discusses two different facilities with similar names: the Aquia Harbour Switching Station and the Aquia Substation. Both are discussed in detail in Section I.C.

<sup>4</sup> The Company further proposes to rebuild the existing 0.1 mile segment of Lines #252 and #29 northwest of Fuller Road Substation using additional right-of-way that increases linearly to form a triangular area of additional right-of-way. Starting at Structure #252/5566 (#29/1833), there is no additional right-of-way. As Lines #252 and #29 travel east, the right-of-way will expand to include up to an additional 67 feet of width at the eastern edge of Mars Station Road.

- (vi) Relocating and rebuilding, entirely within existing right-of-way or on Company-owned property, approximately 6.8 miles of the existing Ladysmith-Possum Point 500 kV Line #568 on single circuit monopole structures, between Aquia Harbour Station and Possum Point Station.
- (vii) Rebuilding, entirely within existing right-of-way or on Company-owned property, approximately 0.7 mile of 230 kV Fredericksburg-Birchwood Non-Utility Generator (“NUG”) Line #2083 on double circuit monopole structures (with vacant arms) between the Company’s Fredericksburg Substation and Mary Washington Boulevard and Hospital Drive (“Hospital Junction”), located within the City of Fredericksburg.

(collectively, the “Rebuild Project”).<sup>5</sup>

The proposed Rebuild Project is necessary for three primary reasons.

#### Compliance with the Company’s Mandatory Planning Criteria

The Rebuild Project will replace aging infrastructure that is at the end of its service life to comply with the Company’s mandatory electric transmission planning criteria (the “Planning Criteria”), thereby enabling the Company to maintain the overall long-term reliability of its transmission system. Specifically, Lines #29 and Line #252 between Aquia Harbour Station and Possum Point Station 115 kV and 230 kV switchyards were constructed in 1978 mostly on wooden steel tower structures and on some wooden H-frame or 3-pole structures that are approaching the end of their useful life based on industry standards, which are 35–55 years for wood structures and 40-60 years for COR-TEN<sup>®</sup> steel structures.

#### Compliance with Mandatory NERC Reliability Standards

The proposed Rebuild Project is also needed to comply with mandatory NERC Reliability

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<sup>5</sup> The Rebuild Project is the second phase of the work the Company plans to undertake as described in its Application filed on March 14, 2024, in Case No. PUR-2024-00035, *Application of Virginia Electric and Power Company for Approval and Certification of Electric Facilities: Fredericksburg-Aquia Harbour Lines #29, #2104, and #2157 Partial Rebuild*.

The Company will also perform work associated with the Rebuild Project at the Fredericksburg, Cranes Corner, Aquia, Ladysmith, and Fuller Road Substations, and Possum Point and Aquia Harbour Stations. This work, while not included as part of the Rebuild Project, is discussed in Section II.C (the Cranes Corner work is discussed immediately below).

Additionally, the Company intends to add one backbone structure outside of the Company’s Cranes Corner Substation in the existing right-of-way to maximize capacity and minimize line crossings in the corridor. Finally, the Company intends to install approximately 0.3 mile of a new 115 kV line starting at the Fuller Road Substation to feed Marine Corps Base Quantico (“MCBQ”) once the entire corridor has been upgraded to 230 kV. The Company’s work associated with the relocation of the backbone structure at Cranes Corner Substation and the new 0.3 mile 115 kV line to feed MCBQ are not components of the Rebuild Project. The Company considers this work to qualify as an “ordinary extension[] or improvement[] in the usual course of business (*i.e.*, “ordinary course”) pursuant to § 56-265.2 A 1 of the Code of Virginia (“Va. Code”) and, therefore, does not require approval pursuant to Va. Code § 56-46.1 B or a CPCN from the Commission. Because this work is not a component of the proposed Rebuild Project, the costs associated with this work are not included in the total Rebuild Project costs.

standards.

The 2026 PJM Interconnection, L.L.C. (“PJM”) Regional Transmission Expansion Plan (“RTEP”) Analysis identified that an N-1-1 loss of Lines #252 (Aquia Harbour-Possum Point) and #2157 (Fredericksburg-Cranes Corner) will drop more than 300 megawatts (“MW”) of load in the Fredericksburg to Possum Point transmission corridor (“F2PPC”), resulting in a NERC criteria violation. To mitigate the potential violation, a new 230 kV source is required in the corridor to split the load. The proposed solution, which was awarded to Dominion Energy Virginia through PJM’s 2021 competitive Reliability Open Window, is to convert Line #29 from 115 kV to 230 kV operation. The Rebuild Project implements this proposed solution from Aquia Harbour Station to Possum Point Station by rebuilding Line #29 utilizing current 230 kV standards. The Rebuild Project, together with the filing referenced in footnote 5, will rebuild the entire Line #29 and convert it to 230 kV standards.

### Significant Anticipated Load Growth

Finally, the Rebuild Project is needed so that the Company can continue to provide reliable service for the significant load growth anticipated in the area. In 2023, the Company received multiple Delivery Point (“DP”) requests in the transmission corridor between the Company’s Fredericksburg Substation and Possum Point Station associated with new data center developments. The Company’s Load-Serving Entity (“Dom LSE” or “Dominion Distribution”) submitted DP requests to either interconnect or evaluate the feasibility of interconnection for at least ten new substations in the F2PPC. Dom LSE also received customer load requests that would necessitate (i) 13 new substations in the corridor south of Fredericksburg Substation and (ii) three new substations east of the F2PPC.

To accommodate this rapidly growing load, the Company proposes to rebuild the following lines in the corridor—Lines #29, #252, and #2083—on double circuit monopole structures.<sup>6</sup> The Company proposes to rebuild Line #568 on single circuit monopole structures approximately 50 feet to the east to collocate Lines #29 and #252 on the same series of double circuit monopole structures. Together, these actions will optimize space within the corridor for the addition of two new 230 kV circuits on a parallel series of double circuit monopole structures. The Company intends to install new conductors for the two additional circuits parallel to Lines #29 and #252, but will not energize the new conductors until the rebuild of the entire corridor between Fredericksburg Substation and Possum Point Station is complete.

By replacing the single circuit structures for Lines #29, #252, and #2083 with double circuit structures during construction of the Rebuild Project, the Company will be able to accommodate imminent load growth. Without the additional circuits installed as part of the Rebuild Project, the Company would have to replace some or all of these facilities in the near term to add transmission lines to support regional growth. Moreover, installing new conductors as part of the Rebuild Project allows the Company to reduce costs, outages, and impacts to environmental, historical, and cultural resources. The ability to energize a future 230 kV circuit to accommodate the significant load growth preserves the option to address future reliability issues and is consistent with prudent

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<sup>6</sup> Lines #29, #252, and #2083 currently use single circuit structures.



utility planning for the future.

Except for the 0.2 mile segment of Lines #29 and 252 between Structure #29/1835 (#252/5568) and Fuller Road Substation, and the 0.1 mile segment west of Fuller Road Substation, the Rebuild Project will be located within existing transmission line rights-of-way or on Company-owned property.<sup>7</sup> Because of the availability of existing rights-of-way and the statutory preference given to use of existing rights-of-way, and because of the additional costs and environmental impacts that would be associated with the acquisition and construction of new rights-of-way, the Company did not consider any alternate routes requiring new rights-of-way for this Rebuild Project.

The estimated conceptual cost of the Rebuild Project is approximately \$205.5 million (in 2024 dollars).<sup>8</sup>

The desired in-service target date for the Rebuild Project is January 31, 2029. The Company estimates it will take approximately 46 months after a final order from the State Corporation Commission (“Commission”) for detailed engineering, materials procurement, permitting, real estate, and construction of the Rebuild Project. Accordingly, to support this estimated construction timeline and construction plan, the Company respectfully requests a final order by February 28, 2025. Should the Commission issue a final order by February 28, 2025, the Company estimates that construction should begin in March 2026 with the Rebuild Project to be completed by the in-service target date of January 31, 2029. This schedule is contingent upon obtaining the necessary permits and careful coordination of outages, the latter of which may be particularly challenging due to the amount of new load growth, rebuilds, and new builds scheduled to occur in this load area. Dates may need to be adjusted based on permitting delays or design modifications to comply with additional agency requirements identified during the permitting application process, as well as the ability to schedule outages, and unpredictable delays due labor shortages or materials/supply issues. Based on the Rebuild Project’s complexity, there may be delays with procurement of materials.

Any adjustments to the Rebuild Project schedule resulting from these or similar challenges could necessitate a minimum of a six- to twelve-month delay in the targeted in-service date. Accordingly, for purposes of judicial economy, the Company requests that the Commission issue a final order approving both a desired in-service target date (*i.e.*, January 31, 2029) and an authorization sunset date (*i.e.*, January 31, 2030) for energization of the Rebuild Project.

In addition, the Company is actively monitoring regulatory changes and requirements associated with the Northern Long Eared Bat (“NLEB”) and how it could potentially impact construction timing associated with time of year restrictions (“TOYRs”). The U.S. Fish and Wildlife Service (“USFWS”) previously indicated that it planned to issue final NLEB guidance to replace the interim guidance by April 1, 2024; however, the interim guidance has been extended by USFWS

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<sup>7</sup> The Company will need approximately 6.5 acres of land to install the new approximately 0.3 mile 115 kV circuit to feed MCBQ from the Fuller Road Substation. As discussed above, this work is not included as part of the Rebuild Project, and the Company considers it to qualify as an “ordinary extension[] or improvement[] in the usual course of business (*i.e.*, “ordinary course”) pursuant to § 56-265.2 A 1 of the Code of Virginia (“Va. Code”) and, therefore, does not require approval pursuant to Va. Code § 56-46.1 B or a CPCN from the Commission.

<sup>8</sup> The cost of the work associated with the Fredericksburg, Cranes Corner, Aquia, Ladysmith, and Fuller Road Substations, and Possum Point and Aquia Harbour Stations, is approximately \$96.8 million (in 2024 dollars).

until late summer 2024. In the meantime, the USFWS issued several draft guidance documents for public review and comment. The Company actively is tracking updates from the USFWS with respect to the final guidance. Once issued, the Company plans to review and follow the final guidance to the extent it applies to the Company's projects. Until the final guidance is issued, the Company will continue following the interim guidance. For projects that may require additional coordination, the Company will coordinate with the USFWS.

The Company is also continuing to track potential regulatory changes associated with the potential up-listing of the Tricolored bat ("TCB"). On September 14, 2022, the USFWS published the proposed rule to the Federal Register to list the TCB as endangered under the Endangered Species Act ("ESA"). On April 1, 2024, the USFWS issued draft guidance for the NLEB and TCB for public review and comment. The USFWS also recently extended its Final Rule issuance target from September 2023 to September 2024. The Company is actively tracking this ruling and evaluating the effects of potential outcomes on Company projects' permitting, construction, and in-service dates, including electric transmission projects.

## **I. NECESSITY FOR THE PROPOSED PROJECT**

- A. State the primary justification for the proposed project (for example, the most critical contingency violation including the first year and season in which the violation occurs). In addition, identify each transmission planning standard(s) (of the Applicant, regional transmission organization (“RTO”), or North American Electric Reliability Corporation) projected to be violated absent construction of the facility.**

Response: The proposed Rebuild Project is necessary to: (a) maintain the structural integrity and reliability of the networked transmission system; (b) resolve identified violations of the mandatory North American Electric Reliability Corporation (“NERC”) Reliability Standards; and (c) provide for future load growth in the area. See Attachment I.A.1 for an overview map of the Rebuild Project.

Dominion Energy Virginia’s transmission system is responsible for providing transmission service: (i) for redelivery to the Company’s retail customers; (ii) to Appalachian Power Company, Old Dominion Electric Cooperative, Northern Virginia Electric Cooperative, Central Virginia Electric Cooperative, and Virginia Municipal Electric Association for redelivery to their retail customers in Virginia; and, (iii) to North Carolina Electric Membership Corporation and North Carolina Eastern Municipal Power Agency for redelivery to their retail customers in North Carolina (collectively, the “Dom Zone”). The Company needs to be able to maintain the overall, long-term reliability of its transmission system to meet its customers’ evolving power needs in the future.

Dominion Energy Virginia is part of PJM Interconnection L.L.C. (“PJM”), the regional transmission organization that provides service to a large portion of the eastern United States. PJM currently is responsible for ensuring the reliability of, and coordinating the movement of, electricity through all or parts of Delaware, Illinois, Indiana, Kentucky, Maryland, Michigan, New Jersey, North Carolina, Ohio, Pennsylvania, Tennessee, Virginia, West Virginia, and the District of Columbia. This service area has a population of approximately 65 million and, on August 2, 2006, set a record high of 165,563 MW for summer peak demand, of which Dominion Energy Virginia’s load portion was approximately 19,256 MW. On July 28, 2023, the Company set a record high of 21,993 MW for summer peak demand. On December 24, 2022, the Company set a winter and all-time record demand of 22,189 MW. Based on the 2024 PJM load forecast, the Dominion Energy Zone is expected to grow with average growth rates of 5.6% summer and 5.1% winter over the next 10 years compared to the PJM average of 1.7% and 2.0% over the same period for the summer and winter, respectively.

Dominion Energy Virginia is also part of the Eastern Interconnection transmission grid, meaning its transmission system is interconnected, directly or indirectly, with all of the other transmission systems in the United States and Canada between the Rocky Mountains and the Atlantic Coast, except for Quebec and most of Texas. All of the transmission systems in the Eastern Interconnection are dependent on

each other for moving bulk power through the transmission system and for reliability support. Dominion Energy Virginia's service to its customers is extremely reliant on a robust and reliable regional transmission system.

NERC has been designated by the Federal Energy Regulatory Commission ("FERC") as the electric reliability organization for the United States. Accordingly, NERC requires that the planning authority and transmission planner develop planning criteria to ensure compliance with NERC Reliability Standards. Mandatory NERC Reliability Standards require that a transmission owner ("TO") develop facility interconnection requirements that identify load and generation interconnection minimum requirements for a TO's transmission system, as well as the TO's reliability criteria.<sup>9</sup>

Federally mandated NERC Reliability Standards constitute minimum criteria with which all public utilities must comply as components of the interstate electric transmission system. Moreover, the Energy Policy Act of 2005 mandates that electric utilities follow these NERC Reliability Standards and imposes fines for noncompliance of approximately \$1.3 million per day per violation.

PJM's Regional Transmission Expansion Plan ("RTEP") is the culmination of an annual transmission planning process, approved by FERC, which includes extensive analysis of the electric transmission system to determine any needed improvements.<sup>10</sup> PJM's annual RTEP is based on the effective criteria in place at the time of the analyses, including applicable standards and criteria of NERC, PJM, and local reliability planning criteria, among others.<sup>11</sup> Projects identified through the RTEP process are developed by the TO in coordination with PJM, and are presented at the Transmission Expansion Advisory Committee ("TEAC") meetings prior to inclusion in the RTEP that is then presented for approval by the PJM Board of Managers (the "PJM Board"). PJM's generation deliverability test for reliability analysis ensures the transmission system is capable of delivering the aggregate system generating capacity at peak load with all firm transmission service modeled. Generation deliverability is a critical system condition test that is part of the PJM reliability standards and, thus, also is required to be satisfied by NERC Reliability Standards.

Outcomes of the RTEP process include three types of transmission system upgrades or projects: (i) baseline upgrades are those that resolve a system reliability criteria violation, which can include planning criteria from NERC, Reliability-First Corporation, SERC Reliability Corporation, PJM, and TOs; (ii) network upgrades

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<sup>9</sup> See FAC-001-3 (R1, R3) (effective April 1, 2021), which can be found at <https://cdn-dominionenergy-prd-001.azureedge.net/-/media/pdfs/virginia/parallel-generation/facility-interconnection-requirements-signed.pdf>.

<sup>10</sup> PJM Manual 14B (effective July 1, 2021) focuses on the RTEP process and can be found at <https://www.pjm.com/-/media/documents/manuals/m14b.ashx>.

<sup>11</sup> See PJM Manual 14B, Attachment D: PJM Reliability Planning Criteria.

are new or upgraded facilities required primarily to eliminate reliability criteria violations caused by proposed generation, merchant transmission, or long-term firm transmission service requests; (iii) supplemental projects are projects initiated by the TO in order to interconnect new customer load, address degraded equipment performance, improve operational flexibility and efficiency, and increase infrastructure resilience. While supplemental projects are included in the RTEP, the PJM Board does not provide formal approval for such projects. As discussed in more detail below, certain components of the Rebuild Project are classified as a baseline project resolving system reliability criteria violations, and other aspects of the Rebuild Project are classified as supplemental. See Section I.J for a discussion of the PJM process as it relates to this Rebuild Project.

### **Need for the Rebuild Project**

The proposed Rebuild Project is needed to maintain the structural integrity and reliability of the networked transmission system; to comply with mandatory NERC Reliability Standards; and to provide for future load growth in the Woodbridge Load Area, which is generally defined as the area which includes, roughly, all of Prince William and Stafford Counties, eastern Fauquier County, southern Loudoun County, and the City of Fredericksburg. For purposes of the Rebuild Project, the load area of interest is the Fredericksburg to Possum Point Corridor (or “F2PPC”) which, as its name implies, is the electric transmission corridor between the Company’s Fredericksburg Substation to the south and its Possum Point Substation to the north. As discussed in Section I.C and depicted in Attachment I.G.1, the F2PPC contains one 230 kV source, comprised of multiple 230 kV lines in series, and one 115 kV source, feeding the various substations between the Fredericksburg and Possum Point terminals. The area served by the substations in the F2PPC is defined, generally, as the area in Stafford County paralleling Interstate 95, north of the Rappahannock River, east to the Potomac River and west along Route 17 to Hartwood Road. It also includes the areas, both north and south, around Stafford Regional Airport, as well as the area around Garrisonville Substation, north to Marine Corps Base Quantico (“MCBQ”) in Stafford County and the Town of Quantico and MCBQ in Prince William County.

The following is a discussion of each Rebuild Project driver, which were developed to address: (1) aging infrastructure that is at the end of its service life based on the Company’s mandatory Planning Criteria, (2) an overload identified in the PJM RTEP Summer 2026 Generator Deliverability study to comply with mandatory NERC Reliability Standards, and (3) future load growth anticipated in the area.

### **Compliance with the Company’s Mandatory Planning Criteria**

The Company has created a plan to address its end-of-life facilities, setting target completion dates for end-of-life projects based on the condition of the facilities, the Company’s resources, and the need to schedule outages. 115 kV Line #29 travels for approximately 24.5 miles between Fredericksburg Substation and Possum Point Stations and serves approximately 452 customers. 230 kV Line #252 travels for

approximately 11.9 miles between Aquia Harbour Station and Possum Point Station and serves approximately 3,800 customers.

The Rebuild Project will rebuild approximately 11.9 miles of 115 kV Line #29 and 230 kV Line #252 between Aquia Harbour Station and the Possum Point Station 230kV switchyard, and also 0.6 mile of 115 kV Line #29 between structure #29/1850 and Possum Point Station 115 kV switchyard, utilizing 230 kV standards. These segments of Line #29 and Line #252 were constructed in 1978 mostly on wooden steel tower structures and some wooden H-frame or 3-pole structures, which are nearing their end-of-life.

Section C.2.9 of the Planning Criteria addresses electric transmission infrastructure approaching its end of life:<sup>12</sup>

Electric transmission infrastructure reaches its end of life as a result of many factors. Some factors such as extreme weather and environmental conditions can *shorten* infrastructure life, while others such as maintenance activities can *lengthen* its life. Once end of life is recognized, in order to ensure continued reliability of the transmission grid, a decision must be made regarding the best way to address this end-of-life asset.

For this criterion, “end of life” is defined as the point at which infrastructure is at risk of failure, and continued maintenance and/or refurbishment of the infrastructure is no longer a valid option to extend the life of the facilities consistent with Good Utility Practice and Dominion Energy Virginia Transmission Planning Criteria. The infrastructure to be evaluated under this end-of-life criteria are all transmission lines at 500 kV and above.

The decision point of this criterion is based on satisfying two metrics:

1. *Facility is nearing, or has already passed, its end of life, and*
2. *Continued operation risks negatively impacting reliability of the transmission system.*

For facilities that satisfy both of these metrics, this criterion mandates either replacing these facilities with in-kind infrastructure that meets current Dominion Energy Virginia standards or employing an alternative solution to ensure the Dominion Energy Virginia transmission system satisfies all applicable reliability criteria.

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<sup>12</sup> The Company’s Transmission Planning Criteria (effective January 1, 2024) can be found in Attachment 1 of the Company’s Facility Interconnection Requirements (“FIR”) document, which is available online at <https://cdn-dominionenergy-prd-001.azureedge.net/-/media/pdfs/virginia/parallel-generation/facility-connection-requirements.pdf>.

Effective March 24, 2020, the Company updated its Planning Criteria so that infrastructure to be evaluated under end-of-life criteria changed from “all transmission lines at 69 kV and above” to “all regional transmission lines operated at 500 kV and above.” The remaining transmission lines between 100 kV and 500 kV are evaluated under the Company’s Attachment M-3 End-of-Life Planning Criteria. The latest version of this criteria was presented at the December 13, 2023, PJM Sub-Regional RTEP meeting. See Attachment I.A.2 for updated slides presented by the Company at that meeting. As discussed in Attachment I.A.2, end-of-life projects between 100 kV and 500 kV are classified as supplemental projects. The process, however, for determining that an asset has reached its end of life remains the same; therefore, the Company continues to use the criteria evaluation process outlined in Section C.2.9 of the Planning Criteria.

The Company submitted the Rebuild Project in accordance with the PJM RTEP process to address the end-of-life criteria.

*1. Facility is nearing, or has already passed, its end of life.*

The Company proposes to rebuild approximately 11.9 miles of existing 115 kV transmission Line #29 between Aquia Harbour Station and Possum Point Station 230 kV switchyard and approximately 11.9 miles of existing 230 kV Line #252 between Aquia Harbour Station and the Possum Point Station 230 kV switchyard, located primarily within the existing right-of-way or on Company-owned property, to current 230 kV standards with minimum summer emergency ratings of 1,573 MVA. The Company will expand its existing right of way by approximately 50 feet between Structure #252/5568 (Structure #29/1835) and Fuller Road Substation to rebuild a 0.2 mile segment of Lines #29 and 252. These sections of Lines #29 and #252 were constructed in 1978 mostly on wooden steel tower structures and some wooden H-frame or 3-pole structures and have 2-bundled 721 ACAR conductors with a 3#6 Alumoweld static wire and 12-fibers Fiber Optic Ground Wire; and an existing summer rating of 360 MVA and 720 MVA, respectively. Industry guidelines indicate equipment life for: wood structures is 35-55 years, COR-TEN<sup>®</sup> steel structures is 40-60 years, conductor and connectors are 40-60 years, and porcelain insulators is 50 years. The structures supporting these segments of Lines #29 and #252 are approaching their end of life, driving the Company’s need to rebuild the line.

*2. Continued operation risks negatively impacting reliability of the transmission system.*

Regarding the second metric of the Company’s Planning Criteria addressing end of life, Line #29 provides service to approximately 452 customers. Addressing aging infrastructure through the Rebuild Project will support the Company’s ability to continue providing reliable transmission service to these customers.

The need to rebuild these segments of Line #29 and Line #252 was first presented to the PJM stakeholders at the Transmission Expansion Advisory Committee

(“TEAC”) Meeting on August 10, 2021. The proposed solution to rebuild Lines #29 and #252 was presented at the October 5, 2021, TEAC Meeting. This section of the Rebuild Project was presented as an end-of-life rebuild project with a proposed solution to rebuild the approximately 11.9 mile segment to current (at the time) 230 kV standards. Attachments I.A.3 and I.A.4 include the slides that were initially presented at the TEAC meetings. The project was issued supplemental upgrade identification number “s2705” by PJM.

Line #252 is the source for Aquia Substation and Fuller Road Substation which serve approximately 3,374 and 424 customers, respectively. Addressing aging infrastructure through the Rebuild Project will support the Company’s ability to continue providing reliable transmission service to these customers.

In summary, the Rebuild Project will replace aging infrastructure at the end of its service life to comply with the Company’s mandatory Planning Criteria, thereby enabling the Company to maintain the overall long-term reliability of its transmission system.

#### Compliance with Mandatory NERC Reliability Standards

PJM’s reliability analysis of the summer 2026 RTEP model has identified that an N-1-1 loss of Lines #252 and #2157 will drop more than 300 MW of load in the F2PPC transmission corridor, resulting in a NERC criteria violation. To mitigate the potential violation, a new 230 kV source is required in the corridor to split the load. The proposed solution, which was awarded to Dominion Energy Virginia through PJM’s 2021 competitive Reliability Open Window, is to convert Line #29 from 115 kV to 230 kV operation.

The Rebuild Project was issued baseline upgrade identification number “b3694” by PJM and first presented to the PJM stakeholders at the TEAC Meeting on November 02, 2021, and again on November 30, 2021. Attachments I.A.5 and I.A.6 include the slides that were presented at the TEAC Meetings. Additionally, Attachment I.A.7 includes the pertinent excerpts from the PJM Staff White Paper of TEAC Recommendations to the PJM Board, where the project was approved by the Board of Managers at its February 16, 2022, meeting.

#### Significant Load Growth

As described previously, the Rebuild Project is in the F2PPC of the Company’s Woodbridge Load Area. The portion of the F2PPC in Stafford County, which represents approximately two-thirds of the overall transmission corridor total (the City of Fredericksburg is approximately 5% and Prince William County is approximately 28%) has experienced increased interest from data center developers since approximately 2022. Dom LSE submitted DP requests to either interconnect or evaluate the feasibility and develop a plan to interconnect at least ten new substations in the Stafford portion of the F2PPC load area, six of which are associated with the proposed Stafford Technology Park. Additionally, Dom LSE



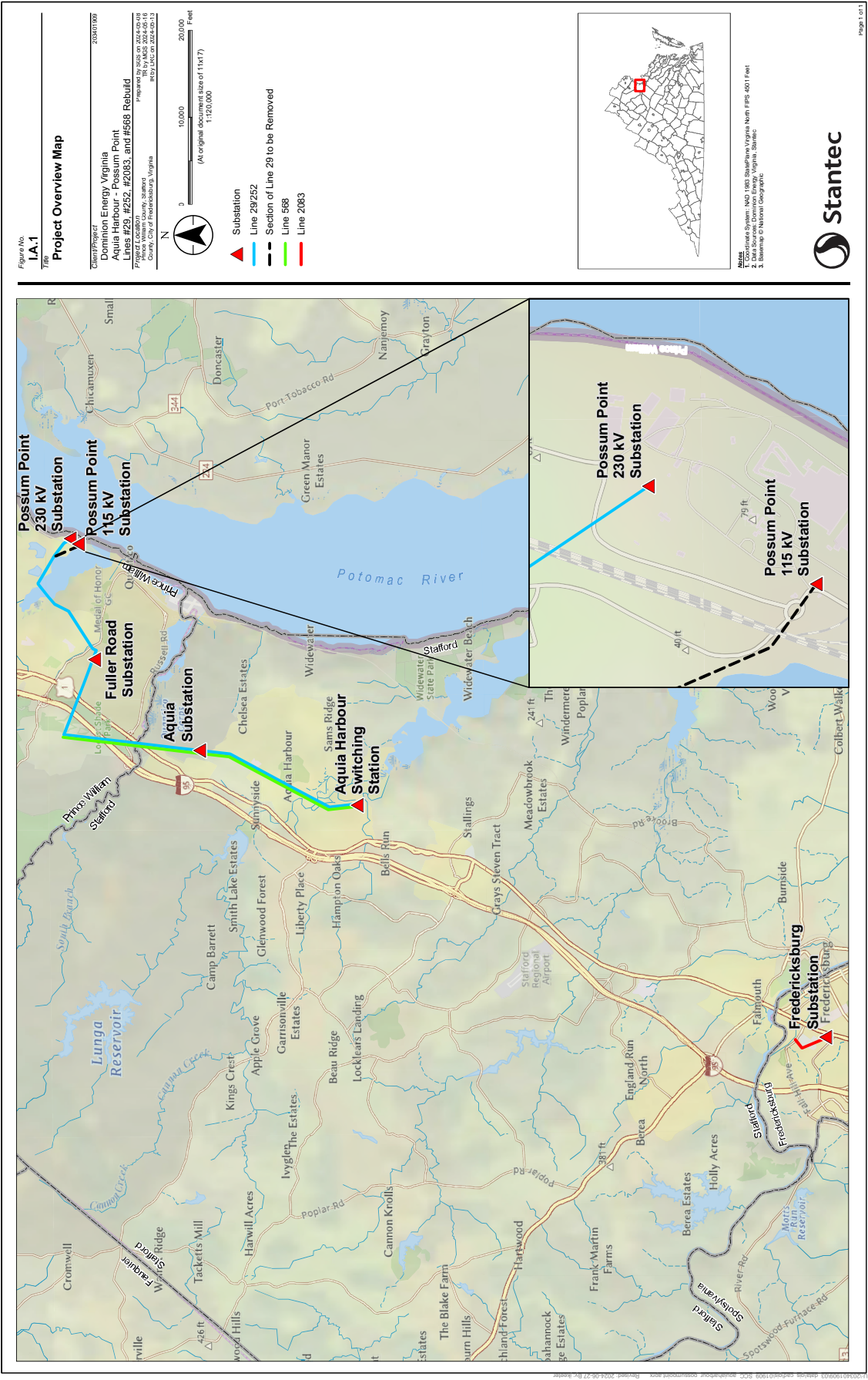
and Rappahannock Electric Cooperative (“REC”) have submitted an additional 16 DP requests in areas east and south of the Company’s Fredericksburg Substation which are expected to impact the F2PPC.

Based on the load growth described above and in Section I.C, the Company determined that rebuilding Lines #29 and #252 on double circuit monopole structures and installing additional circuits/conductors as part of the Rebuild Project will provide significant cost savings, compared to rebuilding the Lines on double circuit-capable structures and subsequently installing the additional circuits in the future. The conceptual Need for additional circuits/conductors in the F2PP Corridor was first presented to the PJM stakeholders at the TEAC Meeting on April 30, 2024, with an Operational Flexibility driver. Attachment I.A.8 includes the “Need” slides that were presented at that meeting. Attachment I.A.9 includes the proposed “Solution” slides that will be presented at the August 6, 2024, TEAC Meeting. The Solution slide contains a one-line diagram that shows the currently submitted/approved projects in the F2PP Corridor and the additional work required to accommodate the additional circuits being proposed as part of Rebuild Project. Once PJM has performed their Do-No-Harm analysis on the proposed Operational Flexibility Solution and determined that no harm is created, they will issue a supplemental (“s”) number. Pending comments from the stakeholders, the Solution will be submitted to the Local Plan for integration into PJM’s Regional Transmission Expansion Plan (“RTEP”).

Rebuilding Lines #29 and #252 also requires rebuilding a small portion of 230 kV Line #2083 (0.7 mile) between Fredericksburg Substation and Hospital Junction. This work is needed so Lines #29 and #252 can terminate at the Fredericksburg Substation without unnecessary line crossings near Fredericksburg Substation.

Line #2083 will be rebuilt on double circuit monopole structures with vacant arms. Additionally, rebuilding Line #2083 on a double circuit monopole will allow for future expansion when necessary. Relocating and rebuilding a portion of Line #568 is also needed to accommodate the rebuild of Lines #29 and #252 on double circuit monopole structures. This will allow the Company to satisfy the growing demand for electricity in the F2PPC while minimizing the need to rework customer interconnections, reducing outage durations, minimizing environmental impacts, and prudently reducing overall costs as compared to retroactively installing double circuit monopole structures as part of a future project.

In summary, the Rebuild Project is needed to: (a) comply with the Company’s mandatory Planning Criteria; (b) comply with mandatory NERC Reliability standards; and (c) allow the Company to continue providing reliable service based on the significant load growth anticipated in the area.



# Dominion Energy

PJM Southern Sub-Regional RTEP Meeting

Planning Assumptions

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SRRTEP South – Dominion Assumptions 12/13/2023



# Planning Criteria and Assumptions

- PJM Assumptions Apply
- All analysis and solutions must satisfy
  - NERC TPL standards
  - PJM Planning Criteria in Attachment D & G of PJM Manual 14B
  - [Dominion Energy's Facility Interconnection Requirements](#)
    - Requirements to connect to Dominion's Transmission system
    - Attachment 1 – Dominion's FERC Form 715 Planning Criteria
    - Attachment 3 – Generation Interconnection Protection Requirements
    - Attachment 4 – Generator Ride-Through Requirements
    - Attachment 5 – Generator Interconnection Data Communication and Data Exchange Requirements
    - Supplemental Project Drivers as Described Below
- PJM and Dominion validate each other's study results to ensure solutions resolve specific need and create no other harm to system
- Proposed solutions are presented
  - TEAC for facilities 230 kV and above
  - Southern Sub-regional for facilities below 230 kV

# Dominion Energy's FERC Form 715

## End of Life Planning Criteria

- Infrastructure to be evaluated under this end-of-life criteria are all regional transmission lines operated at 500 kV and above
- The decision point of this criterion is based on satisfying two metrics:
  - 1) Facility is nearing, or has already passed, its end of life, and
  - 2) Continued operation risks negatively impacting reliability of the transmission system, including our ability to serve local load.
- Projects approved by PJM under this criteria are classified as baseline
- Detailed discussion on the End of Life criteria can be found in Attachment 1, section C.2.9 of [Dominion Energy's Facility Interconnection Requirements](#) document
- All other asset management of transmission infrastructure is covered by the M-3 Supplemental process
- The Appendix lists transmission lines expected to be evaluated using the FERC Form No. 715 End of Life criteria in the 2024 RTEP cycle

# Supplemental Project Drivers

SRRTEP South – Dominion Assumptions 12/13/2023





# Summary of Supplemental Project Drivers

## I. Customer Service

- Service to new and existing customers. Interconnect new customer load. Address distribution load growth, customer outage exposure, equipment loading

## II. Equipment Material Condition, Performance and Risk

- Degraded equipment performance, material condition, obsolescence, equipment failure, employee and public safety and environmental impact
- Substation Assets, Transmission Line Assets, Transmission Transformers

## III. Operational Flexibility and Efficiency

- Optimizing system configuration, equipment duty cycles and restoration capability, minimize outages

## IV. Infrastructure Resilience

- Improve system ability to anticipate, absorb, adapt to, and/or rapidly recover from a potentially disruptive event, including severe weather, geo-magnetic disturbances, electromagnetic pulses, physical and cyber security challenges, critical infrastructure reduction.

## V. Other

- Meet objectives not included in other definitions

## II. Equipment Material Condition, Performance and Risk

- Degraded equipment performance, material condition, obsolescence, equipment failure, employee and public safety and environmental impact
- Substation Assets, Transmission Line Assets, Transmission Transformers



# Equipment Material Condition, Performance and Risk

- End of Life
  - Transmission Lines operated at or above 100 kV and below 500 kV
  - Transformers with high-side operated at or above 100 kV
- Other Asset Management
  - Types of equipment assessed include but not limited to:*
  - Transmission Lines below 100 kV
  - Line Components
    - Capbanks
    - Wave Traps
    - Relaying
  - Transformers below 100 kV
    - Switches
  - Breakers
    - Bus Work, Leads
  - Circuit Switchers
    - FACTS Devices
  - Reactors

# Equipment Material Condition, Performance and Risk

## Project Drivers

- EOL and Asset Management projects include the replacement, modification, upgrade or addition of transmission equipment for the following purposes:
  - Replacement of equipment due to eminent failure
  - Safety concerns
  - Compliance (internal and external)
  - Reliability
  - Operating Flexibility
  - Obsolescence
  - Other

## Dominion Energy's Attachment M-3 End of Life Planning Criteria for Transmission Lines

- Infrastructure to be evaluated under this end-of-life criteria are all transmission lines operated at or above 100kV and below 500 kV
- Projects must satisfy the following two decision point metrics:
  - 1) Facility is nearing, or has already passed, its end of life, and
  - 2) Continued operation risks negatively impacting reliability of the transmission system, including our ability to serve local load.
- Projects will be classified as supplemental

# Transmission Line Facilities

## Project Development Process

- All project requests and inputs are reviewed
- Records of inspections, component failures, refurbishments/repairs, tower loading studies, COR-TEN corrosion studies and other relevant information are reviewed
- Field sampling and inspections are performed
- Perform analysis to determine condition of individual lines and a ranking to support remediation

# Transmission Line Components

## Project Development Process

- Industry typical “expected” service life are considered:
  - Steel structures 40 to 60 years
  - Conductors 60 years
  - Connectors 40 to 60 years
  - Insulators (Porcelain/Glass) 50 years+ (Polymer) 30 years
  - Fiber 30 years
  - Wood 55 years with maintenance
- However, the actual service life is dependent upon many variables and ongoing inspection to evaluate condition is the best determinant of end of service life.

# Dominion Supplemental Projects

Transmission Expansion Advisory  
Committee  
August 10, 2021

## Needs

Stakeholders must submit any comments within 10 days of this meeting in order to provide time necessary to consider these comments prior to the next phase of the M-3 process

# Dominion Transmission Zone: Supplemental Equipment Material Condition, Performance and Risk

**Need Number:** DOM-2021-0058

**Process Stage:** Need Meeting 8/10/2021

**Project Driver:** Equipment Material Condition, Performance and Risk

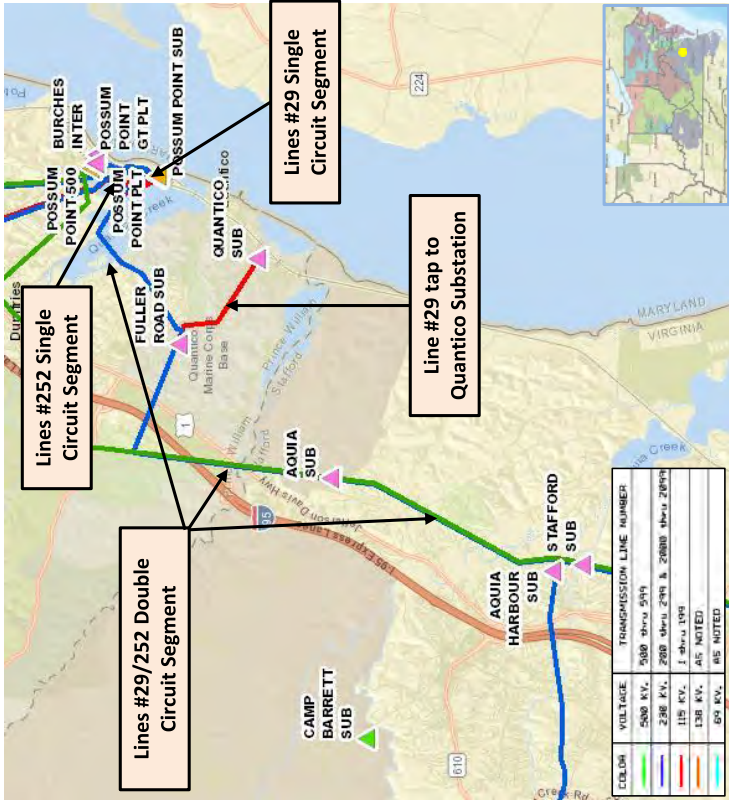
**Specific Assumption References:**

See details on Equipment Material Condition, Performance and Risk in Dominion's Planning Assumptions presented in December 2020.

**Problem Statement:**

Dominion Energy has identified the need to rebuild approximately 12.0 miles of 115kV Line #29 and 230kV Line #252 between Aquia Harbor to Possum Point and the approximately 1.7 miles of 115kV tap line to Quantico Substation based on the Company's End of Life Criteria.

- Lines #29 and #252 were mostly constructed on double circuit CORTEN steel structures in 1978. The 115kV tap line to Quantico Substation was constructed on wood structures in 1978.
- A recent field inspection indicated continued degradation of structures where steel members are delaminating and cracking, and wood structures are showing woodpecker damage.
- Industry guidelines indicate equipment life for wood structures is 35-55 years, conductor and connectors are 40-60 years, and porcelain insulators are 50 years. A 50-year cycle for CORTEN steel structures is often cited.
- Line #29 is the only feed to the customers at Quantico Substation.





Appendix



## High level M-3 Meeting Schedule

### Assumptions

Activity	Timing
Posting of TO Assumptions Meeting information	20 days before Assumptions Meeting
Stakeholder comments	10 days after Assumptions Meeting

### Needs

Activity	Timing
TOs and Stakeholders Post Needs Meeting slides	10 days before Needs Meeting
Stakeholder comments	10 days after Needs Meeting

### Solutions

Activity	Timing
TOs and Stakeholders Post Solutions Meeting slides	10 days before Solutions Meeting
Stakeholder comments	10 days after Solutions Meeting

### Submission of Supplemental Projects & Local Plan

Activity	Timing
Do No Harm (DNH) analysis for selected solution	Prior to posting selected solution
Post selected solution(s)	Following completion of DNH analysis
Stakeholder comments	10 days prior to Local Plan Submission for integration into RTEP
Local Plan submitted to PJM for integration into RTEP	Following review and consideration of comments received after posting of selected solutions

TEAC – Dominion Supplemental 08/10/2021



# Revision History

- 07/30/2021 – V1 – Original version posted to pjm.com.
- 08/04/2021 – V2 – Removed slides 11 and 12 (Solution for DOM-2021-0025)



# Dominion Supplemental Projects

Transmission Expansion Advisory  
Committee  
October 5, 2021

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TEAC – Dominion Supplemental 10/05/2021



# Solution Slides

# Dominion Transmission Zone: Supplemental Equipment Material Condition, Performance and Risk

**Need Number:** DOM-2021-0058

**Process Stage:** Solution Meeting 10/05/2021

**Project Driver:** Equipment Material Condition, Performance and Risk

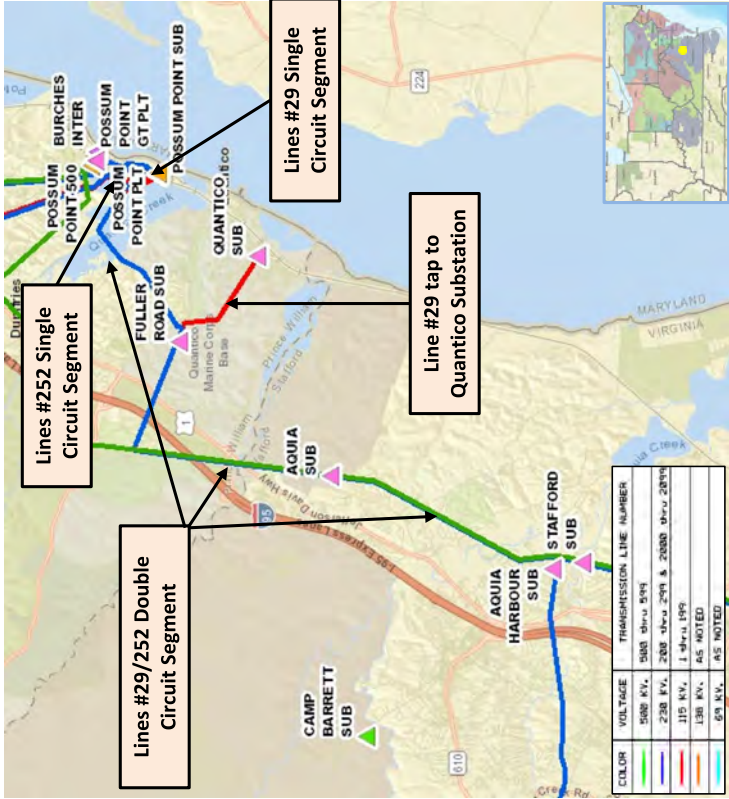
**Specific Assumption References:**

See details on Equipment Material Condition, Performance and Risk in Dominion’s Planning Assumptions presented in December 2020.

**Problem Statement:**

Dominion Energy has identified the need to rebuild approximately 12.0 miles of 115kV Line #29 and 230kV Line #252 between Aquia Harbour Switching Station to Possum Point and the approximately 1.7 miles of 115kV tap line to Quantico Substation based on the Company’s End of Life Criteria.

- Lines #29 and #252 were mostly constructed on double circuit CORTEN steel structures in 1978. The 115 kV tap line to Quantico Substation was constructed on wood structures in 1978.
- A recent field inspection indicated continued degradation of structures where steel members are delaminating and cracking, and wood structures are showing woodpecker damages.
- Industry guidelines indicate equipment life for wood structures is 35-55 years, conductor and connectors are 40-60 years, and porcelain insulators are 50 years. A 50-year cycle for CORTEN steel structures is often cited.
- Line #29 is the only feed to the customers at Quantico Substation.



# Dominion Transmission Zone: Supplemental Line #29 and Line #252 EOL Rebuild

**Need Number:** DOM-2021-0058

**Process Stage:** Solutions Meeting 10/05/2021

**Proposed Solution:**

- Using current 230kV standards and a minimum summer emergency rating of 1047 MVA, wreck and rebuild approximately 12 miles of double circuit Lines #252 and #29 from Aquia Harbour Switching Station to Possum Point.
- At Possum Point, upgrade the wave trap on Line #252 to 3000A.
- At Aquia Substation, upgrade the Line #252 switches and leads to 3000A.
- At Aquia Harbour Switching Station, upgrade the Line #252 wave trap and a circuit breaker switch to 3000A.

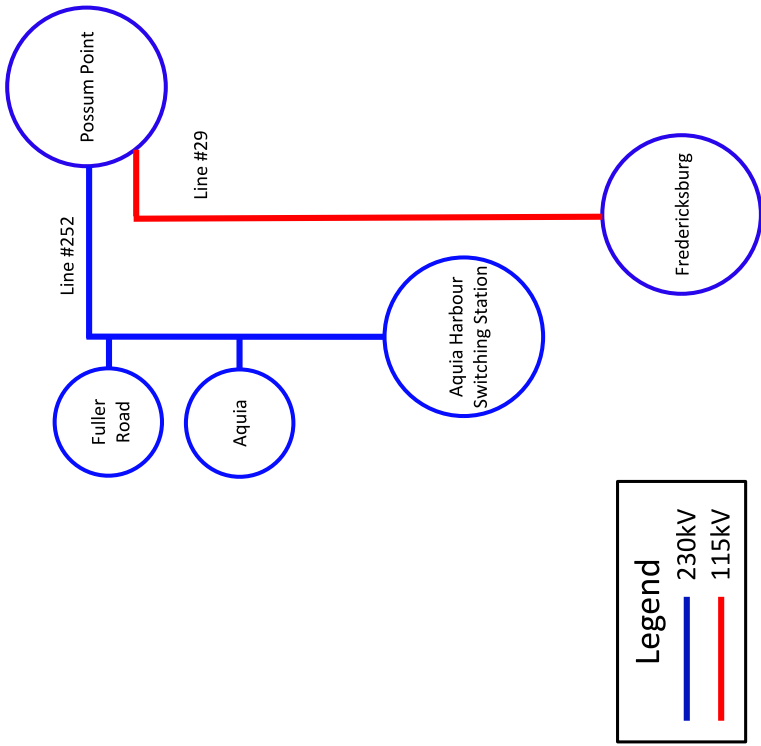
**Estimated Project Cost:** \$38.0 M

**Alternatives Considered:**  
No feasible alternatives

**Projected In-service Date:** 06/01/2026

**Project Status:** Engineering

**Model:** 2025 RTEP



Appendix





## High level M-3 Meeting Schedule

### Assumptions

Activity	Timing
Posting of TO Assumptions Meeting information	20 days before Assumptions Meeting
Stakeholder comments	10 days after Assumptions Meeting

### Needs

Activity	Timing
TOs and Stakeholders Post Needs Meeting slides	10 days before Needs Meeting
Stakeholder comments	10 days after Needs Meeting

### Solutions

Activity	Timing
TOs and Stakeholders Post Solutions Meeting slides	10 days before Solutions Meeting
Stakeholder comments	10 days after Solutions Meeting

### Submission of Supplemental Projects & Local Plan

Activity	Timing
Do No Harm (DNH) analysis for selected solution	Prior to posting selected solution
Post selected solution(s)	Following completion of DNH analysis
Stakeholder comments	10 days prior to Local Plan Submission for integration into RTEP
Local Plan submitted to PJM for integration into RTEP	Following review and consideration of comments received after posting of selected solutions

TEAC – Dominion Supplemental 10/05/2021

## Revision History

09/22/2021 – V1 – Original version posted to [pjm.com](http://pjm.com).  
10/4/2021 – V2 – Correction on slide 6.



# Reliability Analysis Update

Aaron Berner, Senior Manager

Transmission Expansion Advisory Committee  
Tuesday, November 2, 2021



# First Read

## Baseline Reliability Projects

# Dominion Transmission Zone: Baseline Fredericksburg/Carson/Hopewell Area

**Process Stage:** First Read

**Criteria:** Generator Deliverability, FERC Form 715 (C.2.1.3 Critical Stress Case) & N-1

**Assumption Reference:** 2026 RTEP assumption

**Model Used for Analysis:** 2026 RTEP cases

**Proposal Window Exclusion:** None

**Problem Statement:**

In the 2026 RTEP summer case:

Fredericksburg (Group 1: N2-SLD1, N2-SLD2, GD-S16, GD-S467, DOM-T5)

- 230kV Line #2104 Cranes Corner to Stafford is overloaded for a single and breaker contingency under Generator Deliverability and is also overloaded under Dominion stress case criteria.
- Load loss of 307 MW under N-1-1.

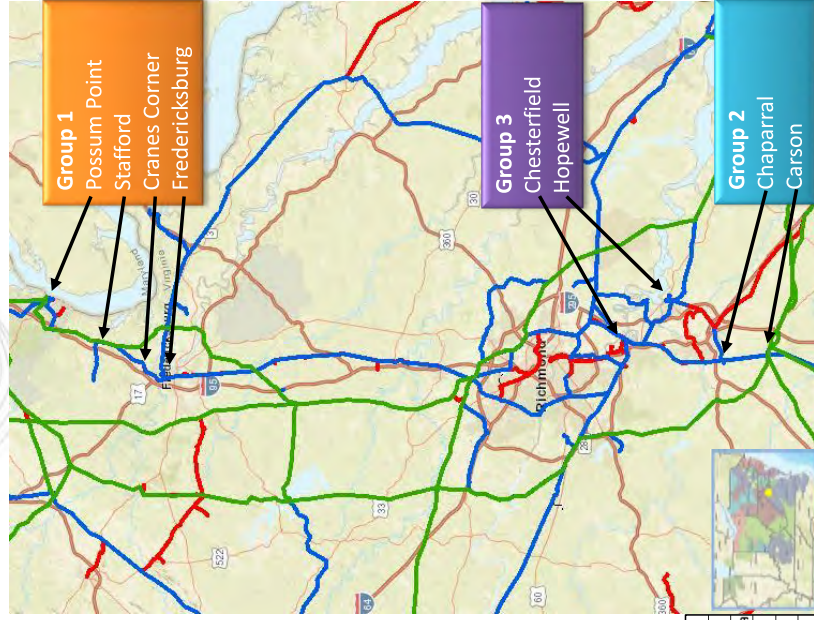
Carson (Group 2: GD-S465, GD-S39)

- Carson 500/230kV transformer #2 is overloaded for a breaker contingency under Generator Deliverability.
- 230kV Line #249 Carson to Chaparral is overloaded for a single contingency under Generator Deliverability.

Hopewell (Group 3: GD-S18, GD-S33, GD-S436)

- 230kV Line #211 is overloaded for a single contingency under Generator Deliverability.
- 230kV Line #228 is overloaded for a single and breaker contingency under Generator Deliverability.

Continued on next slide....





# Dominion Transmission Zone: Baseline Fredericksburg/Carson/Hopewell Area

## Existing Facility Rating:

Area	Branch	SN/SE/WN/WE (MVA)
Fredericksburg	6CRANES – 6STAFORD 230kV	722/722/914/914
Carson	8CARSON – 6CARSON 500kV	928.1/961.6/1192.8/1238.1
Carson	6CARSON – 6CHAPARRAL T 230kV	595/595/659/659
Carson	6LOCKS – 6CHAPARRAL T 230kV	595/595/659/659
Carson	6LOCKS – 3HARROWG 115kV	147/147/185/185
Hopewell	6HOPEWELL – 6CHESTF A 230kV	478/478/606/606
Hopewell	6HOPEWELL – 6CHESTF B 230kV	478/478/606/606

As part of the 2021 RTEP Window #1, the following project was proposed to address violations at Fredericksburg, Carson and Hopewell:

Proposal ID	Proposing Entity	Upgrade Description	Upgrade Cost (\$M)
224	Dominion	<b>Fredericksburg:</b> Convert 115kV Line #29 to 230 kV; Reconductor 230kV Line #2104 Cranes Corner to Aquia Harbor. Feed Quantico via Fuller Road Substation	93.412
		<b>Carson:</b> Energize Carson 500/230kV Tx#1; Reconductor 230kV Line #249 Carson to Locks; Partial Rebuild 115kV Line #100 Locks to Harrowgate	
		<b>Hopewell:</b> Partial rebuild 2.9 miles of double circuit 230kV Lines #211/228	

Continued on next slide....



# Dominion Transmission Zone: Baseline Fredericksburg/Carson/Hopewell Area

**Proposed Solution:** Proposal #2021\_1-224

## Fredericksburg

- Convert Line #29 Aquia Harbor to Possum Point to 230 kV (Extended Line #2104) and swap Line #2104 and converted Line #29 at Aquia Harbor backbone termination. Upgrade terminal equipment at Possum Point to terminate converted Line 29 (now extended Line #2104). (Line #29 from Fredericksburg to Aquia Harbor is being rebuilt under baseline b2981 to 230kV standards.) **Estimated cost: \$9.386M**
- Upgrade Aquia Harbor terminal equipment to not limit 230kV Line #9281 conductor rating. **Estimated cost: \$0.631M**
- Upgrade Fredericksburg terminal equipment by rearranging 230 kV bus configuration to terminate converted Line 29 (now becoming 9281). The project will add a new breaker at the 230kV bay and reconfigure line termination of 230kV Lines #2157, #2090, and #2083. **Estimated cost: \$2.725M**
- Reconductor/rebuild approximately 7.6 miles of 230kV Line #2104 Cranes Corner – Stafford to achieve a summer rating of 1047 MVA<sup>(1)</sup>. Reconductor/rebuild approximately 0.34 miles of 230kV Line #2104 Stafford – Aquia Harbor to achieve a summer rating of 1047 MVA. Upgrade terminal equipment at Cranes Corner to not limit the new conductor rating. **Estimated cost: \$19.596M**
- Upgrade wave trap and line leads at 230kV Line #2090 Ladysmith CT terminal to achieve 4000A rating. **Estimated cost: \$0.152M**
- Upgrade Fuller Road substation to feed Quantico substation via 115 kV radial line. Install four breaker ring and break 230kV Line #252 into two new lines: 1) #252 between Aquia Harbor to Fuller Road and 2) #9282 between Fuller Road and Possum Point. Install a 230/115 kV transformer which will serve Quantico substation. **Estimated cost: \$24.159M**

<sup>(1)</sup> This portion of the project will be addressed by baseline b3321 as it overlaps the violation associated with the deactivation of Morgantown 1 and 2 presented at the 8/31 TEAC.

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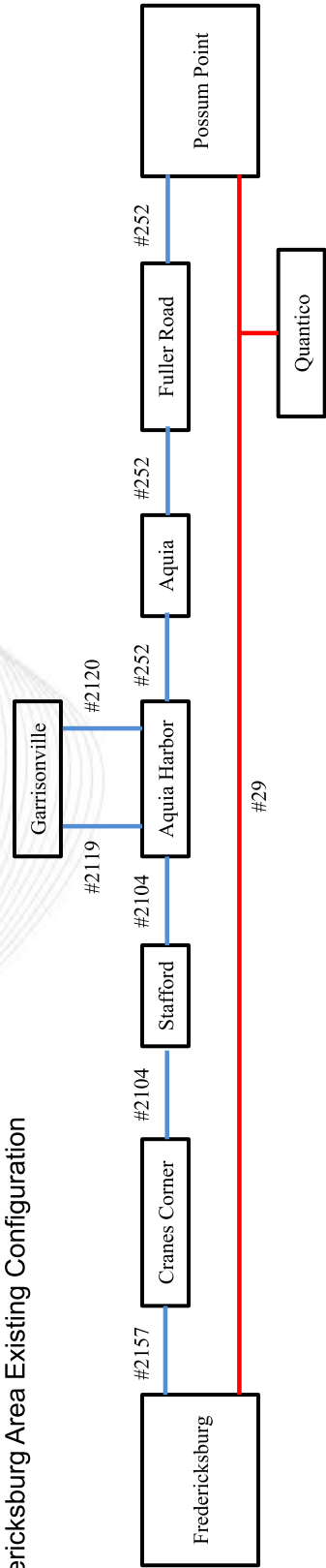




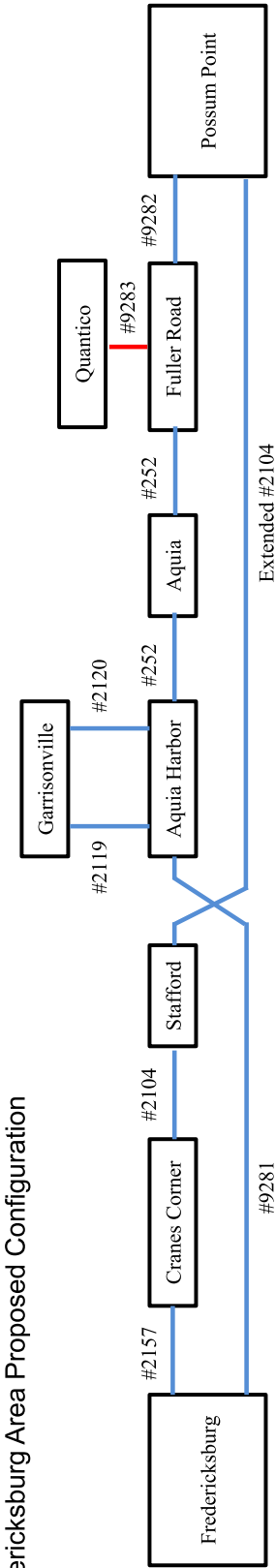
# Dominion Transmission Zone: Baseline

## Fredericksburg/Carson/Hopewell Area

Fredericksburg Area Existing Configuration



Fredericksburg Area Proposed Configuration



Continued on next slide....



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**Reliability Analysis Update**



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## Revision History

Version No.	Date	Description
1	10/28/2021	<ul style="list-style-type: none"><li>Original slides posted</li></ul>
2	10/29/2021	<ul style="list-style-type: none"><li>Added slides 7, 8, 9, and 10, plus made a date correction on slide #6</li></ul>
3	11/1/2021	<ul style="list-style-type: none"><li>Corrected slide 13 header information</li></ul>
4	11/4/2021	<ul style="list-style-type: none"><li>Corrected transformer # on slide 8 (Lawrence 230/69 kV 220-4)</li></ul>
5	11/9/2021	<ul style="list-style-type: none"><li>Corrected FG#s on slide 58</li></ul>
6	11/15/2021	<ul style="list-style-type: none"><li>Corrected preliminary facility ratings on slide 42</li></ul>
7	12/13/2021	<ul style="list-style-type: none"><li>Slide #16, changed the 2nd "Required IS date" to "Projected IS date"</li></ul>



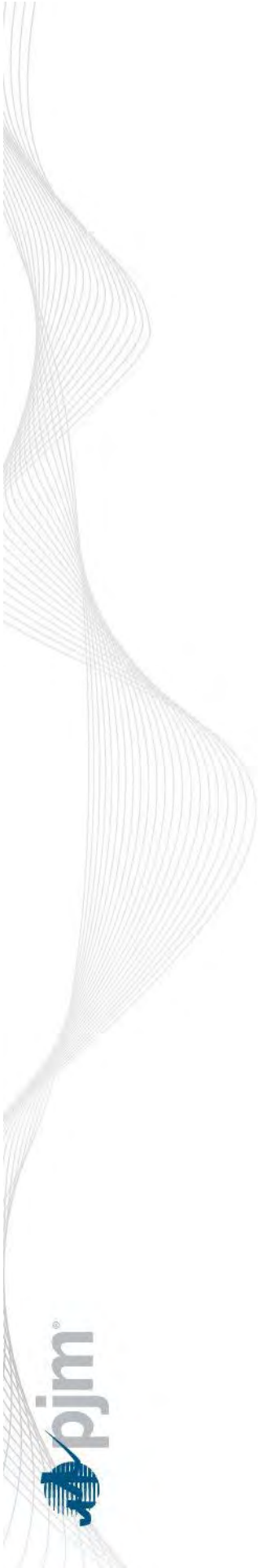
# Reliability Analysis Update

Aaron Berner, Senior Manager

Transmission Expansion Advisory Committee  
Tuesday, November 30, 2021



## 2021 RTEP Proposal Window



## Second Review

### Baseline Reliability Projects



# Dominion Transmission Zone: Baseline Fredericksburg/Carson/Hopewell Area

**Process Stage:** Second Review

**Criteria:** Generator Deliverability, FERC Form 715 (C.2.1.3 Critical Stress Case) & N-1

**Assumption Reference:** 2026 RTEP assumption

**Model Used for Analysis:** 2026 RTEP cases

**Proposal Window Exclusion:** None

**Problem Statement:**

In the 2026 RTEP summer case:

Fredericksburg (Group 1: N2-SLD1, N2-SLD2, GD-S16, GD-S467, DOM-T5)

- 230kV Line #2104 Cranes Corner to Stafford is overloaded for a single and breaker contingency under Generator Deliverability and is also overloaded under Dominion stress case criteria.
- Load loss of 307 MW under N-1-1.

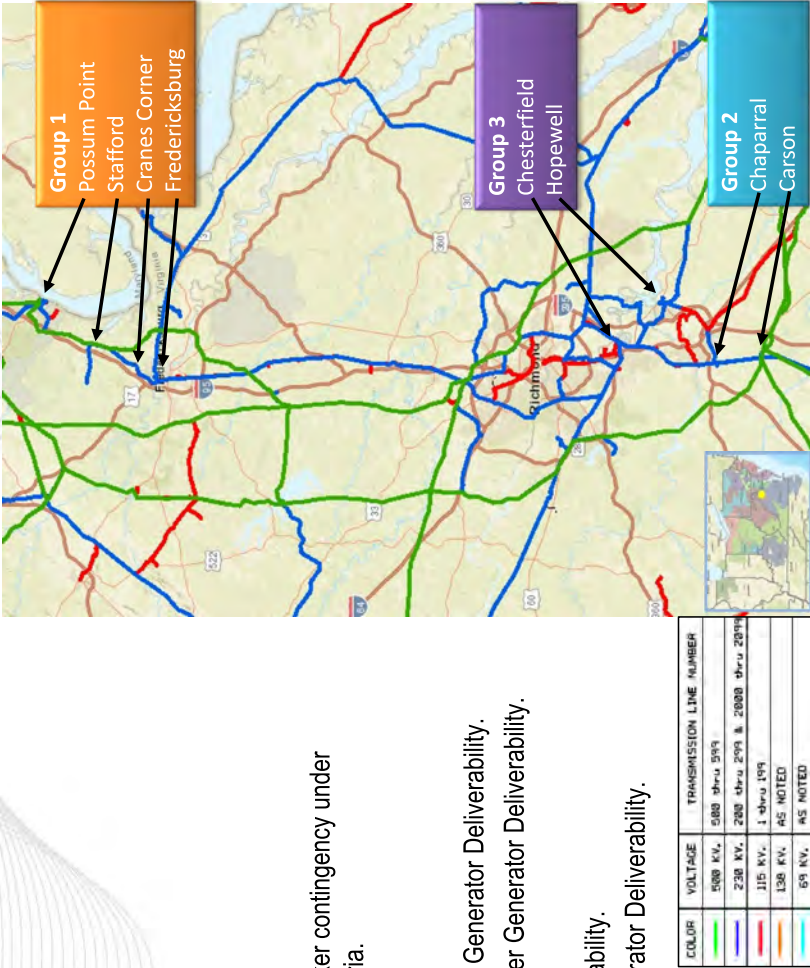
Carson (Group 2: GD-S465, GD-S39)

- Carson 500/230kV transformer #2 is overloaded for a breaker contingency under Generator Deliverability.
- 230kV Line #249 Carson to Chaparral is overloaded for a single contingency under Generator Deliverability.

Hopewell (Group 3: GD-S18, GD-S33, GD-S436)

- 230kV Line #211 is overloaded for a single contingency under Generator Deliverability.
- 230kV Line #228 is overloaded for a single and breaker contingency under Generator Deliverability.

Continued on next slide....





## Dominion Transmission Zone: Baseline Fredericksburg/Carson/Hopewell Area

### Existing Facility Rating:

Area	Branch	SN/SE/WN/WE (MVA)
Fredericksburg	6CRANES – 6STAFORD 230kV	722/722/914/914
Carson	8CARSON – 6CARSON 500/230kV #2	928.1/961.6/1192.8/1238.1
Carson	6CARSON – 6CHAPARRAL T 230kV	595/595/659/659
Carson	6LOCKS – 6CHAPARRAL T 230kV	595/595/659/659
Carson	6LOCKS – 3HARROWG 115kV	147/147/185/185
Hopewell	6HOPEWELL – 6CHESTF A 230kV	478/478/606/606
Hopewell	6HOPEWELL – 6CHESTF B 230kV	478/478/606/606

As part of the 2021 RTEP Window #1, the following project was proposed to address violations at Fredericksburg, Carson and Hopewell:

Proposal ID	Proposing Entity	Upgrade Description	Upgrade Cost (\$M)
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		<b>Carson:</b> Energize Carson 500/230kV Tx#1; Reconductor 230kV Line #249 Carson to Locks; Partial Rebuild 115kV Line #100 Locks to Harrowgate	
		<b>Hopewell:</b> Partial rebuild 2.9 miles of double circuit 230kV Lines #211/228	

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## Dominion Transmission Zone: Baseline Fredericksburg/Carson/Hopewell Area

**Recommended Solution:** Proposal #2021\_1-224

### Fredericksburg

- Convert Line #29 Aquia Harbor to Possum Point to 230 kV (Extended Line #2104) and swap Line #2104 and converted Line #29 at Aquia Harbor backbone termination. Upgrade terminal equipment at Possum Point to terminate converted Line 29 (now extended Line #2104). (Line #29 from Fredericksburg to Aquia Harbor is being rebuilt under baseline b2981 to 230kV standards.) **Estimated cost: \$9.386M (b3694.1)**
- Upgrade Aquia Harbor terminal equipment to not limit 230kV Line #9281 conductor rating. **Estimated cost: \$0.631M (b3694.2)**
- Upgrade Fredericksburg terminal equipment by rearranging 230 kV bus configuration to terminate converted Line 29 (now becoming 9281). The project will add a new breaker at the 230kV bay and reconfigure line termination of 230kV Lines #2157, #2090, and #2083. **Estimated cost: \$2.725M (b3694.3)**
- Reconductor/rebuild approximately 7.6 miles of 230kV Line #2104 Cranes Corner – Stafford to achieve a summer rating of 1047 MVA<sup>(1)</sup>. Reconductor/rebuild approximately 0.34 miles of 230kV Line #2104 Stafford – Aquia Harbor to achieve a summer rating of 1047 MVA. Upgrade terminal equipment at Cranes Corner to not limit the new conductor rating. **Estimated cost: \$19.596M (b3694.4)**
- Upgrade wave trap and line leads at 230kV Line #2090 Ladysmith CT terminal to achieve 4000A rating. **Estimated cost: \$0.152M (b3694.5)**
- Upgrade Fuller Road substation to feed Quantico substation via 115 kV radial line. Install four breaker ring and break 230kV Line #252 into two new lines: 1) #252 between Aquia Harbor to Fuller Road and 2) #9282 between Fuller Road and Possum Point. Install a 230/115 kV transformer which will serve Quantico substation. **Estimated cost: \$24.159M (b3694.6)**

<sup>(1)</sup> This portion of the project will be addressed by baseline b3321 as it overlaps the violation associated with the deactivation of Morgantown 1 and 2 presented at the 8/31 TEAC.

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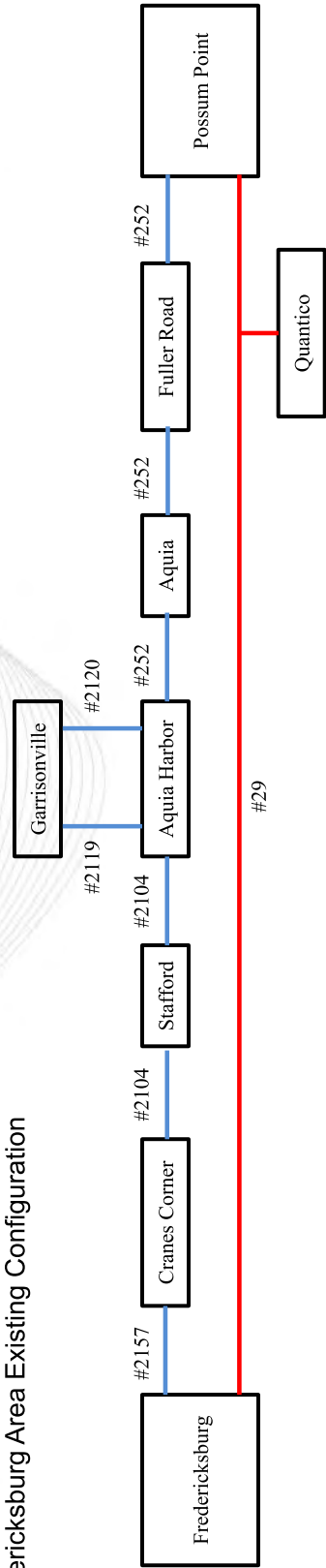




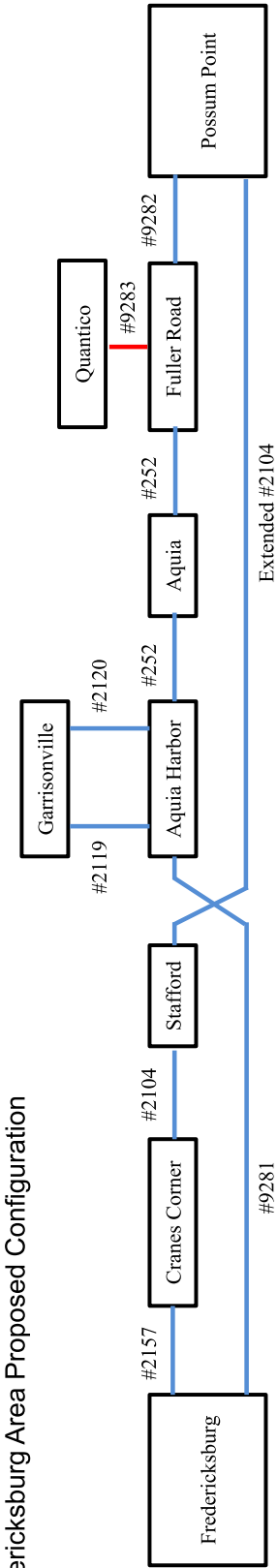
# Dominion Transmission Zone: Baseline

## Fredericksburg/Carson/Hopewell Area

Fredericksburg Area Existing Configuration



Fredericksburg Area Proposed Configuration



Continued on next slide....

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**Reliability Analysis Update**



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Version No.	Date	Description
1	11/23/2021	<ul style="list-style-type: none"> <li>Original slides posted</li> </ul>
2	12/13/2021	<ul style="list-style-type: none"> <li>Slide #6, Changed the 2<sup>nd</sup> “Required IS date” to “Projected IS date”</li> </ul>
3	4/27/2022	<ul style="list-style-type: none"> <li>Slide #29, Changed “Reconductor” to “Rebuild” for the 211/228 updates in the Hopewell area.</li> </ul>



# Transmission Expansion Advisory Committee (TEAC) Recommendations to the PJM Board

PJM Staff White Paper

PJM Interconnection  
February 2022

For Public Use

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## I. Executive Summary

On December 8, 2021, the PJM Board of Managers approved changes to the Regional Transmission Expansion Plan (RTEP), totaling a net increase of \$95.65 million for baseline projects, to resolve baseline reliability criteria violations and address changes to existing projects. The PJM Board of Managers also approved a net increase of \$39.14 million for network upgrades to address new projects with signed ISAs, project scope changes and project cancellations.

Since then, PJM has identified additional baseline reliability criteria violations, and the transmission system enhancements needed to solve them, at an estimated cost of \$519.37 million. Scope/cost changes to an existing project will result in a net increase of \$3.54 million, and cancellation to an existing project will result in a net decrease of \$7.5 million. This yields an overall RTEP net increase of \$515.41 million, for which PJM recommended Board approval. With these changes, RTEP projects will total approximately \$39,448.9 million since the first Board approvals in 2000.

PJM sought Reliability and Security Committee consideration and full Board approval of the RTEP baseline projects summarized in this white paper. On February 16, 2022, the Board approved the addition of RTEP baseline projects as well as other changes to the RTEP as summarized in this paper.

## II. Baseline Project Recommendations

A key dimension of PJM's RTEP process is baseline reliability evaluation, which is necessary before subsequent interconnection requests can be analyzed. Baseline analysis identifies system violations to reliability criteria and standards, determines the potential to improve the market efficiency and operational performance of the system, and incorporates any public policy requirements. PJM then develops transmission system enhancements to solve identified violations and reviews them with stakeholders through the Transmission Expansion Advisory Committee (TEAC) and Subregional RTEP committees prior to submitting its recommendation to the Board. Baseline reliability transmission enhancement costs are allocated to PJM responsible customers.

## III. Baseline Reliability Projects Summary

A summary of baseline projects with estimated costs equal to or greater than \$10 million, as well as one operational performance driven project, is provided below. A complete listing of all recommended projects and their associated cost allocations is included in Attachment A (allocations to a single zone) and Attachment B (allocations to multiple zones). Projects with estimated costs less than \$10 million typically include, by way of example, transformer replacements, line reconductoring, breaker replacements and upgrades to terminal equipment, including relay and wave trap replacements.

### A. AEP Transmission Zone

- Baseline project b3353 – Allen 46 kV Station Rebuild Baseline Conversion: \$16 million
- Baseline project b3348 – Dehue Area Improvements: \$65.8 million
- Baseline project b3361 – Prestonsburg-Thelma 46 kV Rebuild: \$33.01 million



***B. APS Transmission Zone***

- Baseline project b3683 – Messick Road-Ridgeley 138 kV Upgrades: \$11.2 million

***C. ComEd Transmission Zone***

- Baseline project b3677 – LaSalle-Mazon 138 kV Rebuild: \$42.06 million

***D. Dominion Transmission Zone***

- Baseline project b3686 – Bremo-Columbia D.P. 115 kV Switching Station: \$16 million
- Baseline project b3687 – Bristers-Minnieville D.P. 115 kV Rebuild: \$30 million
- Baseline project b3684 – Earleys-Kelford 115 kV Rebuild: \$18.75 million
- Baseline project b3692 – Elmont-Chickahominy 500 kV Rebuild: \$58.16 million
- Baseline project b3694 – Fredericksburg/Carson/Hopewell Area Improvements: \$93.41 million
- Baseline project b3689 – Remington CT-Gainesville 230 kV Reconnector: \$30.68 million

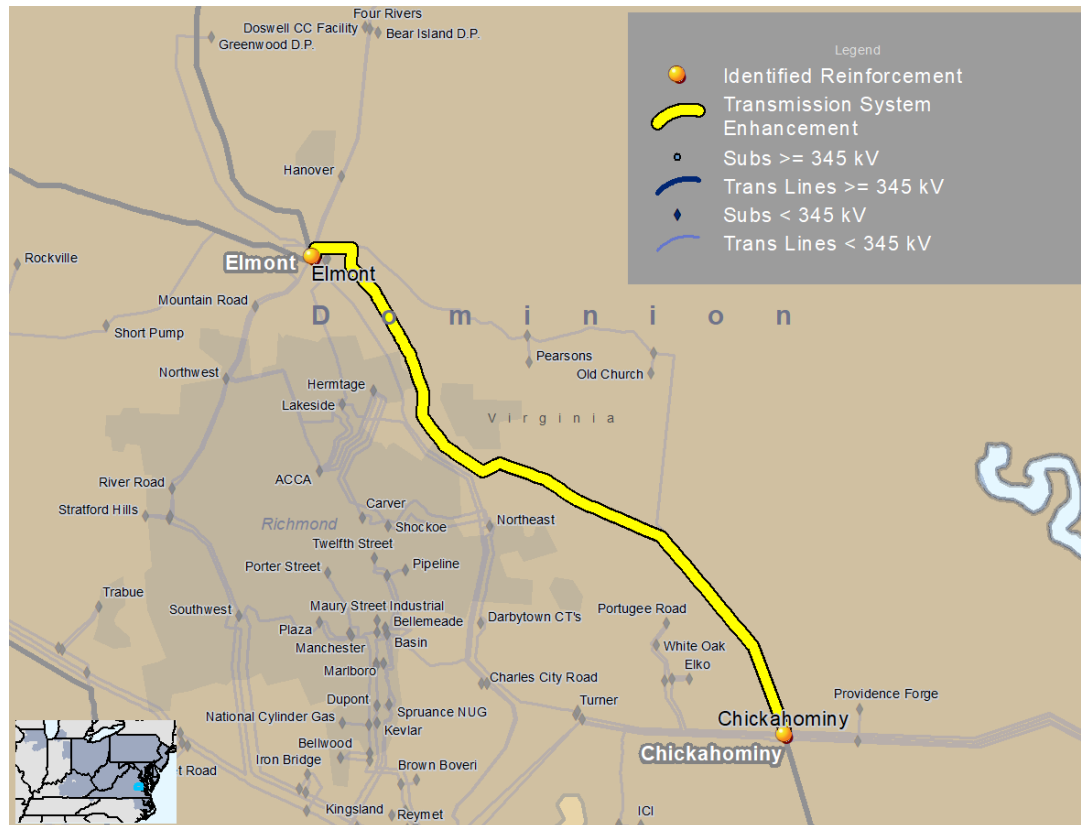
PJM also recommended projects totaling \$79.53 million, which include a 115 kV and multiple 69 kV line rebuilds, 230 kV line reconductoring, a 345/138 kV transformer installation, 138/69/46 kV and 138/69 kV transformer replacements, capacitor bank installations, a reactor installation, circuit breaker and disconnect switch installations/replacements, and other substation and terminal equipment upgrades/replacements, whose individual cost estimates are less than \$10 million.

A more detailed description of the larger-scope projects that PJM recommended to the Board is provided below.

***E. Baseline Reliability Project Details*****Baseline Project b3353: Allen 46 kV Station Rebuild Baseline Conversion****AEP Transmission Zone**

In the 2026 RTEP winter case, the Stanville-Allen 46 kV line section is overloaded for multiple N-1 outage combination.

**Map 9. b3692: Elmont-Chickahominy 500 kV**



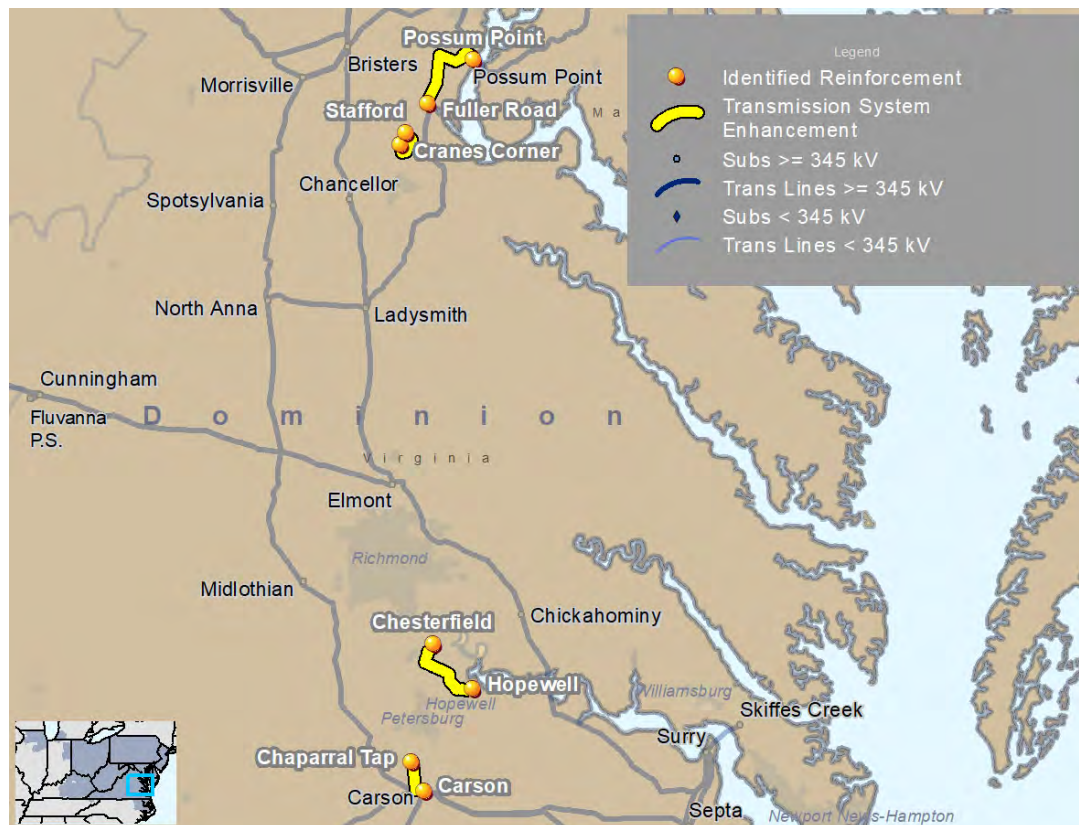
The recommended solution, solicited through the 2021 Window 1 competitive proposal process, is to rebuild approximately 27.7 miles of 500 kV transmission line from Elmont to Chickahominy with current 500 kV standards construction practices to achieve a summer rating of 4330 MVA. The estimated cost for this project is \$58.16 million, with a required and projected in-service date of June 2026. The local transmission owner, Dominion, will be designated to complete this work.

## Baseline Project b3694: Fredericksburg/Carson/Hopewell Area Improvements

### Dominion Transmission Zone

In the 2026 RTEP summer case, in the Fredericksburg area, the Cranes Corner-Stafford 230 kV line (No. 2104) is overloaded for an N-1 and N-2 outage as well as under Dominion stress case criteria, and there is load loss of 307 MW for N-1 outage combinations. In the Carson area, the Carson 500/230 kV transformer No. 2 is overloaded for an N-2 outage, and the Carson-Chaparral 230 kV line (No. 249) is overloaded for an N-1 outage. In the Hopewell area, the Chesterfield-Hopewell 230 kV line (No. 211) is overloaded for an N-1 outage, and the Chesterfield-Hopewell 230 kV line (No. 228) is overloaded for an N-1 and N-2 outage.

**Map 10. b3694: Fredericksburg/Carson/Hopewell Area Improvements**



The recommended solution, solicited through the 2021 Window 1 competitive proposal process, is a comprehensive project that addresses all three areas.

In the Fredericksburg area, the project will convert 115 kV line No. 29 (Aquia Harbor-Possum Point) to 230 kV (extended line No. 2104) and swap line No. 2104 (Cranes Corner-Stafford 230 kV) and converted line No. 29 at Aquia Harbor backbone termination. The project will also upgrade terminal equipment at Possum Point, Aquia Harbor and Fredericksburg 230 kV. The project will add a new breaker at the Fredericksburg 230 kV bay and reconfigure 230 kV line terminations. Approximately 7.6 miles of 230 kV line No. 2104 (Cranes Corner-Stafford) and approximately 0.34 miles of 230 kV line No. 2104 (Stafford-Aquia Harbor) will be reconducted/rebuilt to achieve a summer rating of 1047 MVA (terminal equipment at Cranes Corner will be upgraded to not limit the new conductor rating). The project will upgrade the wave trap and line leads at 230 kV line No. 2090 Ladysmith CT terminal to achieve 4000 A rating. The Fuller Road substation will be upgraded to feed the Quantico substation via a 115 kV radial line, and a four-breaker ring will be installed to break 230 kV line No. 252 into two new lines: 1) No. 252 between Aquia Harbor to Fuller Road, and 2) No. 9282 between Fuller Road and Possum Point. A 230/115 kV transformer will also be installed, which will serve Quantico substation.

In the Carson area, the project will energize the in-service spare 500/230 kV Carson No. 1 transformer, and partially wreck and rebuild 10.34 miles of 230 kV line No. 249 (Carson-Locks) to achieve a minimum summer emergency rating of 1047 MVA (terminal equipment at Carson and Locks will be upgraded to not limit the new conductor rating). The project includes the wreck and rebuild of 5.4 miles of 115 kV line No. 100 (Locks-Harrowgate) to achieve a

### **AMPT Project in ATSI Transmission Zone**

- Baseline project b3153 (Amherst area improvements, including construction of a greenfield 0.3 mile 138 kV double circuit line tapping the Beaver-Black River 138 kV line) is no longer needed because the single-point radial exposure criteria has been removed from the AMPT's FERC 715 Planning Criteria. Instead, the project is being resubmitted as a supplemental project. The project had an estimated cost of \$7.5 million.

This change yields a net RTEP decrease of \$7.5 million.

### ***B. Scope/Cost Changes***

The following scope/cost modification was recommended:

#### **Dominion Transmission Zone**

- Baseline project b2443.6 (installation of second Possum Point 500/230 kV transformer) has undergone a scope change and cost increase. The b2443.6 project was initially slated to be cancelled in 2021, as it was determined that the deficiencies were no longer present in the updated summer 2023 & 2025 RTEP cases. However, the cancellation was placed on hold due to an issue identified in the 2021 RTEP and potential for the project to be brought back if the proposal was provided to mitigate the violation. Based on what was previously submitted for b2443.6 back in 2019, there was a modest change in scope to include a wreck and rebuild of an existing line that connects the 500 kV and 230 kV Possum Point substations. Double circuit structures will be installed to carry both the new and old lines, and there is some rearrangement work in the 230 kV substation. The total cost of the project has increased from \$21 million to \$24.54 million, yielding an RTEP increase of \$3.54 million.

This change yields a net RTEP increase of \$3.54 million.

## **VIII. Review by the Transmission Expansion Advisory Committee (TEAC)**

Project needs and recommended solutions as discussed in this report were reviewed with stakeholders during 2021 and 2022, most recently at the January 2022 TEAC meeting. Written comments were requested to be submitted to PJM to communicate any concerns with project recommendations. No comments have been received as of this white paper publication date.

## **IX. Cost Allocation**

Cost allocations for recommended projects are shown in Attachment A (for allocation to a single zone) and Attachment B (for allocation to multiple zones).

Cost allocations are calculated in accordance with Schedule 12 of the Open Access Transmission Tariff (OATT). Baseline reliability project allocations are calculated using a distribution factor methodology that allocates cost to the load zones that contribute to the loading on the new facility. The allocations will be filed at FERC 30 days following approval by the Board.

## **X. Board Approval**

The PJM Reliability and Security Committee is requested to endorse the changes to the RTEP proposed in this white paper, and recommended to the full Board for approval the changes to existing RTEP projects as detailed in this white paper to be included in PJM's RTEP. On February 16, 2022, the Board approved the addition of RTEP baseline projects as well as other changes to the RTEP as summarized in this paper. The RTEP is published annually on PJM's website.

## Attachment A – Reliability Project Single-Zone Allocations

Upgrade ID	Description	Cost Estimate (\$M)	Transmission Owner	Cost Responsibility	Required In-Service Date
<b>b3346.1</b>	Rebuild approximately 3.5 miles of overloaded 69 kV line between North Delphos-East Delphos-Elida Road switch. This includes approximately 1.1 miles of double circuit line that makes up a portion of the North Delphos-South Delphos 69 kV line and the North Delphos-East Delphos 69 kV line. Approximately 2.4 miles of single circuit line will also be rebuilt between the double circuit portion to East Delphos station and from East Delphos to Elida Road Switch.	\$8.43	AEP	AEP	6/1/2026
<b>b3346.2</b>	Replace the line entrance spans at South Delphos to eliminate the overloaded 4/0 Copper and 4/0 ACSR conductor.	\$0.44	AEP	AEP	6/1/2026
<b>b3348.1</b>	Construct a 138 kV single bus station (Tin Branch) consisting of a 138 kV box bay with a distribution transformer and 12 kV distribution bay. Two 138 kV lines will feed this station (from Logan and Sprigg stations), and distribution will have one 12 kV feed. Install two 138 kV circuit breakers on the line exits. Install 138 kV circuit switcher for the new transformer.	\$5.58	AEP	AEP	11/1/2026
<b>b3348.2</b>	Construct a new 138/46/12 kV Argyle station to replace Dehue station. Install a 138 kV ring bus using a breaker-and-a-half configuration, with an autotransformer with a 46 kV feed and a distribution transformer with a 12 kV distribution bay. Two 138 kV lines will feed this station (from Logan and Wyoming stations). There will also be a 46 kV feed from this station to Becco station. Distribution will have two 12 kV feeds. Retire Dehue station in its entirety.	\$10.00	AEP	AEP	11/1/2026
<b>b3348.3</b>	Bring the Logan-Sprigg #2 138 kV circuit in and out of Tin Branch station by constructing approximately 1.75 miles of new overhead double circuit 138 kV line. Double circuit T3 series lattice towers will be used along with 795,000 cm ACSR 26/7 conductor. One shield wire will be conventional 7 #8 ALUMOWELD, and one shield wire will be OPGW.	\$8.58	AEP	AEP	11/1/2026



Upgrade ID	Description	Cost Estimate (\$M)	Transmission Owner	Cost Responsibility	Required In-Service Date
<b>b3687</b>	Rebuild approximately 15.1-mile-long line segment between 115 kV line #183 Bristers and Minnieville D.P. with 2-768 ACSS and 4000 A supporting equipment from Bristers to Ox to allow for future 230 kV capability of 115 kV line #183. The continuous summer normal rating will be 523 MVA from Ox-Minnieville. The continuous summer normal rating will be 786 MVA from Minnieville-Bristers.	\$30.00	Dominion	Dominion	6/1/2026
<b>b3689.1</b>	Reconductor approximately 24.42 miles of 230 kV line #2114 Remington CT-Elk Run-Gainesville to achieve a summer rating of 1574 MVA by fully reconductoring the line and upgrading the wave trap and substation conductor at Remington CT and Gainesville.	\$28.99	Dominion	Dominion	6/1/2026
<b>b3689.2</b>	Replace 230 kV breakers SC102, H302, H402 and 218302 at Brambleton substation with 4000A 80 kA breakers and associated equipment including breaker leads as necessary to address breaker duty issues identified in short circuit analysis.	\$1.69	Dominion	Dominion	6/1/2026
<b>b3690</b>	Reconductor approximately 1.07 miles of 230 kV line #2008 segment from Cub Run-Walney to achieve a summer rating of 1574 MVA. Replace line switch 200826 with a 4000A switch.	\$1.93	Dominion	Dominion	6/1/2026
<b>b3691</b>	Reconductor approximately 1.4 miles of 230 kV line #2141 from Lakeview-Carolina to achieve a summer rating of 1047 MVA.	\$1.19	Dominion	Dominion	6/1/2026
<b>b3694.1</b>	Convert line #29 Aquia Harbor to Possum Point to 230 kV (Extended line #2104) and swap line #2104 and converted line #29 at Aquia Harbor backbone termination. Upgrade terminal equipment at Possum Point to terminate converted line 29 (now extended line #2104). (Line #29 from Fredericksburg to Aquia Harbor is being rebuilt under baseline b2981 to 230kV standards.)	\$9.39	Dominion	Dominion	6/1/2026
<b>b3694.10</b>	Reconductor approximately 2.9 miles of 230 kV line #211 Chesterfield-Hopewell to achieve a minimum summer emergency rating of 1046 MVA.	\$4.91	Dominion	Dominion	6/1/2026
<b>b3694.11</b>	Reconductor approximately 2.9 miles of 230 kV line #228 Chesterfield-Hopewell to achieve a minimum summer emergency rating of 1046 MVA.	\$4.91	Dominion	Dominion	6/1/2026
<b>b3694.12</b>	Upgrade equipment at Chesterfield substation to not limit ratings on lines 211 and 228.	\$0.76	Dominion	Dominion	6/1/2026

Upgrade ID	Description	Cost Estimate (\$M)	Transmission Owner	Cost Responsibility	Required In-Service Date
<b>b3694.13</b>	Upgrade equipment at Hopewell substation to not limit ratings on lines 211 and 228.	\$1.71	Dominion	Dominion	6/1/2026
<b>b3694.2</b>	Upgrade Aquia Harbor terminal equipment to not limit 230 kV line #9281 conductor rating.	\$0.63	Dominion	Dominion	6/1/2026
<b>b3694.3</b>	Upgrade Fredericksburg terminal equipment by rearranging 230 kV bus configuration to terminate converted line 29 (now becoming 9281). The project will add a new breaker at the 230 kV bay and reconfigure line termination of 230 kV lines #2157, #2090 and #2083.	\$2.73	Dominion	Dominion	6/1/2026
<b>b3694.4</b>	Reconductor/rebuild approximately 7.6 miles of 230 kV line #2104 Cranes Corner-Stafford to achieve a summer rating of 1047 MVA(1). Reconductor/rebuild approximately 0.34 miles of 230 kV line #2104 Stafford-Aquia Harbor to achieve a summer rating of 1047 MVA. Upgrade terminal equipment at Cranes Corner to not limit the new conductor rating.	\$19.60	Dominion	Dominion	6/1/2026
<b>b3694.5</b>	Upgrade wave trap and line leads at 230 kV line #2090 Ladysmith CT terminal to achieve 4000A rating.	\$0.15	Dominion	Dominion	6/1/2026
<b>b3694.6</b>	Upgrade Fuller Road substation to feed Quantico substation via 115 kV radial line. Install four-breaker ring and break 230 kV line #252 into two new lines: 1) #252 between Aquia Harbor to Fuller Road and 2) #9282 between Fuller Road and Possum Point. Install a 230/115 kV transformer which will serve Quantico substation.	\$24.16	Dominion	Dominion	6/1/2026
<b>b3694.7</b>	Energize in-service spare 500/230 kV Carson Tx#1.	\$0.00	Dominion	Dominion	6/1/2026
<b>b3694.8</b>	Partial wreck and rebuild 10.34 miles of 230 kV line #249 Carson-Locks to achieve a minimum summer emergency rating of 1047 MVA. Upgrade terminal equipment at Carson and Locks to not limit the new conductor rating.	\$15.37	Dominion	Dominion	6/1/2026
<b>b3694.9</b>	Wreck and rebuild 5.4 miles of 115 kV line #100 Locks-Harrowgate to achieve a minimum summer emergency rating of 393 MVA. Upgrade terminal equipment at Locks and Harrowgate to not limit the new conductor rating and perform line #100 Chesterfield terminal relay work.	\$9.10	Dominion	Dominion	6/1/2026
<b>b3697</b>	Replace station conductor and metering inside Whipain and Plymouth substations to increase the ratings of the 220-13/220-14 Whipain-Plymouth 230 kV line facilities.	\$0.62	PECO	PECO	6/1/2025



# Dominion Supplemental Projects

Transmission Expansion Advisory  
Committee  
April 30, 2024



## Needs

Stakeholders must submit any comments within 10 days of this meeting in order to provide time necessary to consider these comments prior to the next phase of the M-3 process

# Dominion Transmission Zone: Supplemental Operational Flexibility and Efficiency

**Need Number:** DOM-2024-0035  
**Process Stage:** Need Meeting 04/30/2024  
**Project Driver:** Operational Flexibility and Efficiency

**Specific Assumption References:**

See details on Operational Flexibility and Efficiency in Dominion’s Planning Assumptions presented in December 2023.

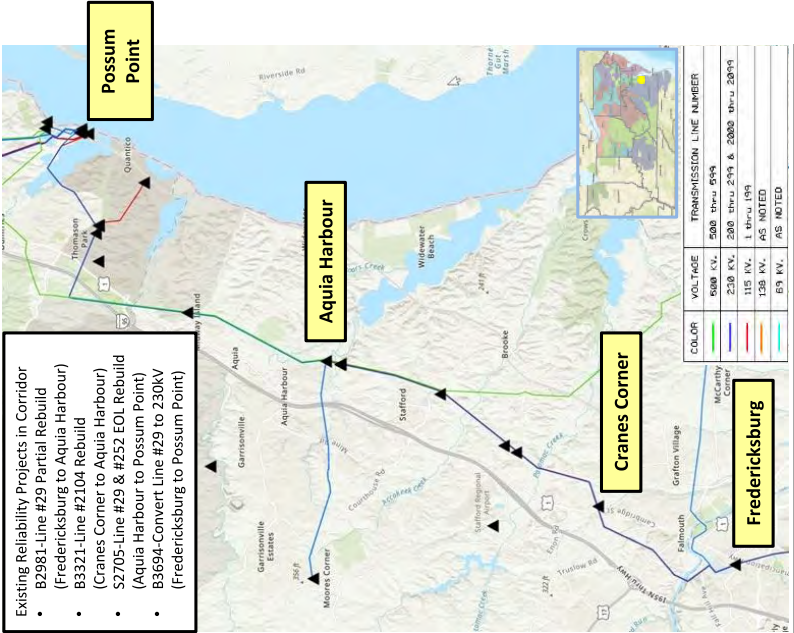
**Problem Statement (page 1 of 2):**

Multiple projects have been developed to address reliability violations in the Fredericksburg to Possum Point corridor, resulting in a majority of the corridor being rebuilt over the next 3–4 years so that two, 230kV transmission lines will be available to support existing network flows and to interconnect new customer load. These include baseline projects b2981, b3321, b3694 and supplemental project s2705. There is a need to reevaluate options to maximize use of the existing ROW and the planned upgrades while minimizing chances of wreck and rebuild work in the near future.

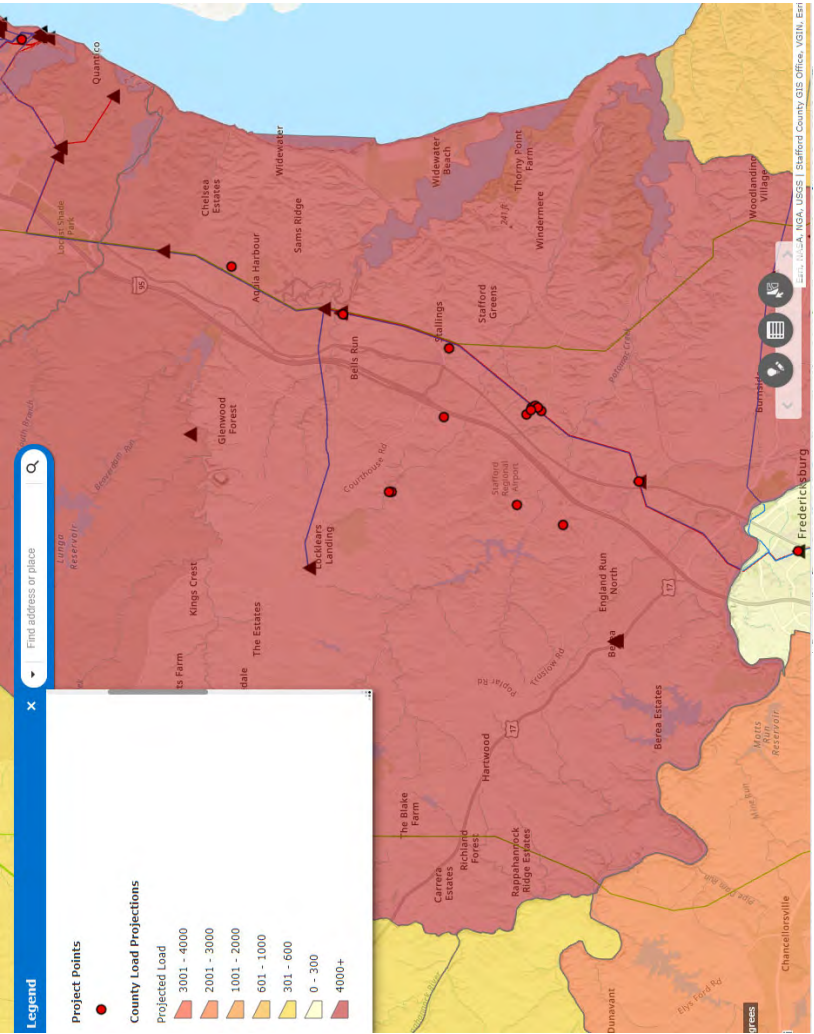
Delivery Point (DP) Requests for thirteen new substations to serve data center load in the corridor have been submitted by DEV Distribution and are in various stages of evaluation/development. Load projections for the DP’s currently indicate over 1700 MW of new load by year 2029, growing to over 3000 MW by year 2032.

Additionally, in the corridor south of Fredericksburg Substation, DP Requests for fourteen new substations have been received with projected loads exceeding 2000 MW by year 2029 and 3000 MW by year 2032.

Without diverse transmission sources to serve the new substations, it is anticipated that initial facility interconnections with the two, 230kV transmission lines will have to be reworked as additional transmission lines are required in the corridor to address new reliability violations. This is expected to result in customer interconnection delays, increased outage durations, and increased overall cost.



Dominion Transmission Zone: Supplemental Operational Flexibility and Efficiency



**Need Number:** DOM-2024-0035  
**Process Stage:** Need Meeting 04/30/2024  
**Project Driver:** Operational Flexibility and Efficiency

**Specific Assumption References:**  
See details on Operational Flexibility and Efficiency in Dominion's Planning Assumptions presented in December 2023.

**Problem Statement (page 2 of 2):**

	A	B	E	G	R	X
5	Need Presented 04/30/2024 TEAC					
6	Need Previously Presented					
	DOM#	Project Name	Connect	Type	2029	2032
8	2023-18	Spartan Sub	5/2/2025	DP	110	110
9	2023-35	Caboose Sub	6/1/2026	DP	84	140
10	n/a	Widewater Sub	1/1/2027	EO	0	77
11	2024-28	Shady Hill	4/4/2027	DP	175	175
12	2024-05	Centreport Sub	7/1/2027	DP	136	136
13	2023-56	Alto Sub	7/1/2027	DP	213	213
14	2024-06	Woodcutters Sub	1/1/2028	DP	250	1000
15	2024-07	Surveyors	1/1/2028	DP	300	300
16	2024-29	Soprano Sub	4/1/2028	DP	116	255
17	2023-34	Freight Sub	8/5/2028	DP	40	140
18	2024-08	Baritone Sub	10/1/2028	DP	32	183
19	2024-34	Opera Sub	10/1/2029	DP	0	242
20	n/a	Classical Sub	7/1/2030	EO	0	155
21	2023-24	Locomotive Sub	11/4/2031	DP	116	255
22	n/a	Tenor Sub	7/1/2032	EO	0	6
23	2024-30	Mountain View Sub	4/1/2026	DP	181	181
24						
25				TOTAL	1753	3568

Appendix



# High level M-3 Meeting Schedule

## Assumptions

Activity	Timing
Posting of TO Assumptions Meeting information	20 days before Assumptions Meeting
Stakeholder comments	10 days after Assumptions Meeting

## Needs

Activity	Timing
TOs and Stakeholders Post Needs Meeting slides	10 days before Needs Meeting
Stakeholder comments	10 days after Needs Meeting

## Solutions

Activity	Timing
TOs and Stakeholders Post Solutions Meeting slides	10 days before Solutions Meeting
Stakeholder comments	10 days after Solutions Meeting

## Submission of Supplemental Projects & Local Plan

Activity	Timing
Do No Harm (DNH) analysis for selected solution	Prior to posting selected solution
Post selected solution(s)	Following completion of DNH analysis
Stakeholder comments	10 days prior to Local Plan Submission for integration into RTEP
Local Plan submitted to PJM for integration into RTEP	Following review and consideration of comments received after posting of selected solutions



Revision History

04/19/2024– V1 – Original version posted to pjm.com  
04/30/2024– V2 – Corrected date in footer.



# Dominion Supplemental Projects

Transmission Expansion Advisory  
Committee  
August 6, 2024





## Solutions

Stakeholders must submit any comments within 10 days of this meeting in order to provide time necessary to consider these comments prior to the next phase of the M-3 process

# Dominion Transmission Zone: Supplemental Operational Flexibility and Efficiency

**Need Number:** DOM-2024-0035  
**Process Stage:** Solution Meeting 08/06/2024  
**Previously Presented:** Need Meeting 04/30/2024  
**Project Driver:** Operational Flexibility and Efficiency

**Specific Assumption References:**

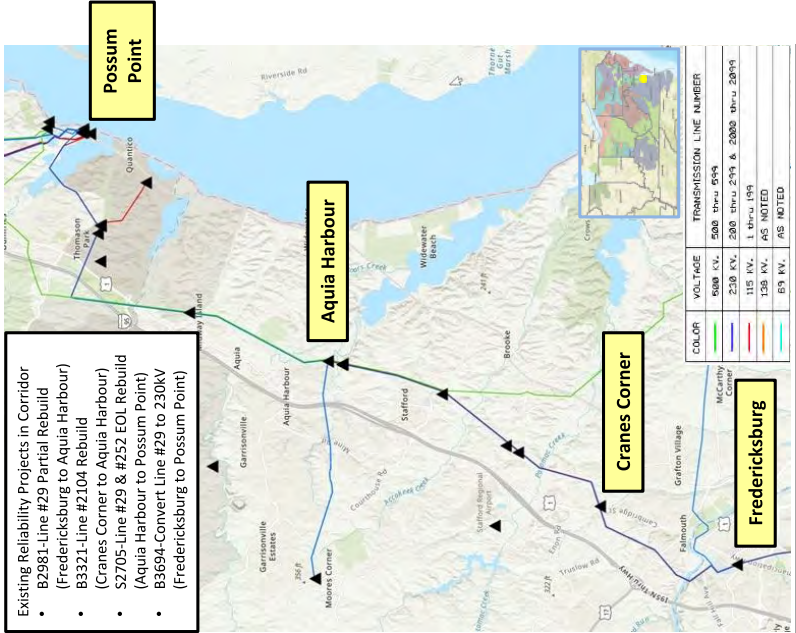
See details on Operational Flexibility and Efficiency in Dominion’s Planning Assumptions presented in December 2023.

**Problem Statement:**

Multiple projects have been developed to address reliability violations in the Fredericksburg to Possum Point corridor, resulting in a majority of the corridor being rebuilt over the next 3-4 years so that two, 230kV transmission lines will be available to support existing network flows and to interconnect new customer load.

Delivery Point (DP) Requests for thirteen new substations to serve data center load in the corridor have been submitted by DEV Distribution and are in various stages of evaluation/development. Load projections for the DP’s currently indicate over 1700 MW of new load by year 2029, growing to over 3000 MW by year 2032.

Additionally, in the corridor south of Fredericksburg Substation, DP Requests for fourteen new substations have been received with projected loads exceeding 2000 MW by year 2029 and 3000 MW by year 2032. Without diverse transmission sources to serve the new substations, it is anticipated that initial facility interconnections with the two, 230kV transmission lines will have to be reworked as additional transmission lines are required in the corridor to address new reliability violations. This is expected to result in customer interconnection delays, increased outage durations, and increased overall cost.



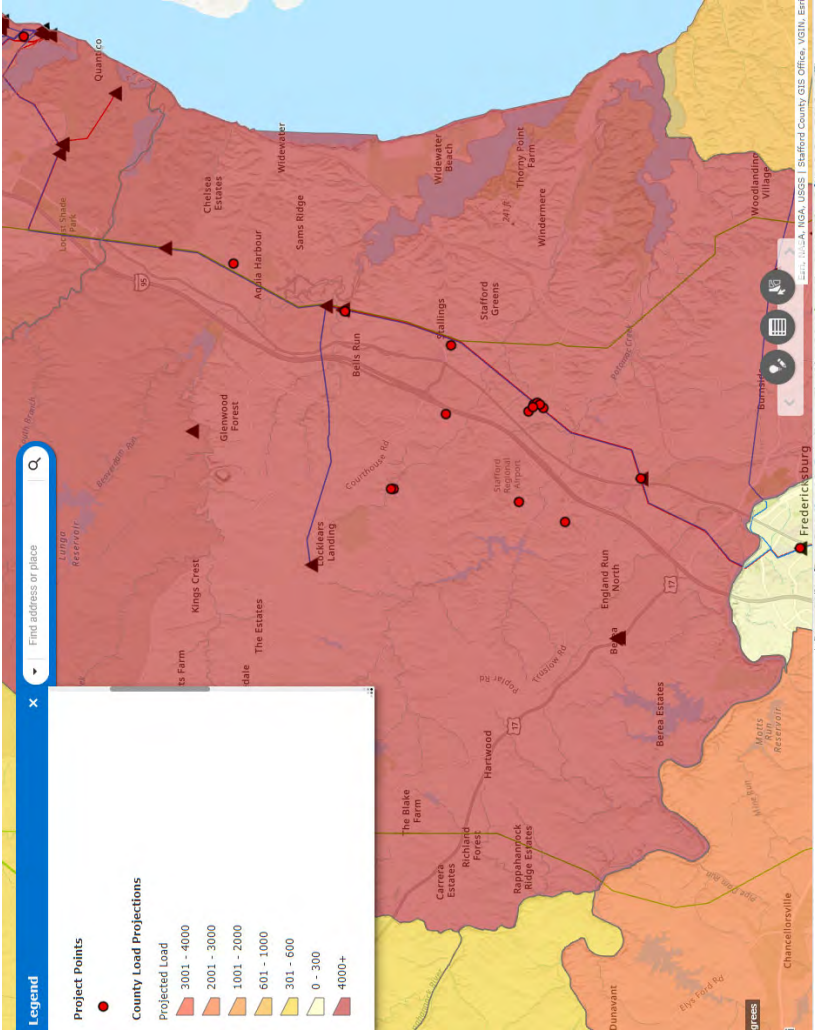
# Dominion Transmission Zone: Supplemental Operational Flexibility and Efficiency

**Need Number:** DOM-2024-0035  
**Process Stage:** Solution Meeting 08/06/2024  
**Previously Presented:** Need Meeting 04/30/2024  
**Project Driver:** Operational Flexibility and Efficiency

**Specific Assumption References:**  
See details on Operational Flexibility and Efficiency in Dominion's Planning Assumptions presented in December 2023.

**Problem Statement (continued):**

	A	B	E	G	R	X
5	Need Presented 04/30/2024 TEAC					
6	Need Previously Presented					
	DOM#	Project Name	Connect	Type	2029	2032
8	2023-18	Spartan Sub	5/2/2025	DP	110	110
9	2023-35	Caboose Sub	6/1/2026	DP	84	140
10	n/a	Widewater Sub	1/1/2027	EO	0	77
11	2024-28	Shady Hill	4/4/2027	DP	175	175
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22	n/a	Tenor Sub	7/1/2032	EO	0	6
23	2024-30	Mountain View Sub	4/1/2026	DP	181	181
24						
25				TOTAL	1753	3568



# Dominion Transmission Zone: Supplemental Fredericksburg to Possum Corridor – Add 3<sup>rd</sup> and 4<sup>th</sup> 230kV Lines

**Need Number:** DOM-2024-0035  
**Process Stage:** Solutions Meeting 08/06/2024

**Proposed Solution:**

- Construct Allman Switching Station north of existing Fredericksburg Substation, to accommodate ten, 230kV line terminals (six north, four south) in five strings of a breaker-and-a-half arrangement. GIS equipment will be utilized due to limited space.
- Rebuild Line #2157 approx. 4.5 miles, Allman to Cranes Corner, with double-circuit structures and a minimum summer conductor rating of 1573 MVA.
- Rebuild Line #2083 approx. 0.7 miles, Allman to Hospital Jct, with double-circuit structures and a minimum summer conductor rating of 1573 MVA.
- Expand Cranes Corner Sub to accommodate a new backbone for line re-alignment.
- Construct a 2<sup>nd</sup> 230kV double-circuit pole line approx. 12 miles, Aquia Harbour to Possum Point. Approximately 41 lattice structures (~7.1 miles) of adjacent 500kV Line #568 will be replaced with monopole structures to accommodate the new 230kV double-circuit structures in the corridor.
- Install two additional 230kV lines in the corridor, with a minimum summer rating of 1573 MVA, by utilizing the vacant arm positions on the double-circuit structures that will be created by rebuilding the existing single-circuit structures from Fredericksburg to Aquia Harbour and the new double-circuit structures from Aquia Harbour to Possum Point.
- Reconfigure the 230kV terminals at Possum Point to accommodate the two new line terminations.

**Estimated Project Cost:** \$180.0M (\$120.0M T-Line; \$60.0M Substation)

**Alternatives Considered:**

The intent of this project is to facilitate the orderly expansion of Dominion's transmission system by introducing new 230kV sources into the Fredericksburg to Possum Point corridor that will support the projected load growth and maximize the use of existing right-of-way. No alternatives outside of the existing corridor were developed.

**Projected In-service Date:** 06/01/2029

**Project Status:** Conceptual

**Model:** 2029 RTEP

Bubble Diagrams  
on Next Page





REBUILD CORRIDOR/ CONVERT LINE #29 TO 230kV  
(Submitted/Approved Projects - b2981, b3321, s2705, b3696)



Appendix



## High level M-3 Meeting Schedule

### Assumptions

Activity	Timing
Posting of TO Assumptions Meeting information	20 days before Assumptions Meeting
Stakeholder comments	10 days after Assumptions Meeting

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Activity	Timing
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Stakeholder comments	10 days after Needs Meeting

### Solutions

Activity	Timing
TOs and Stakeholders Post Solutions Meeting slides	10 days before Solutions Meeting
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### Submission of Supplemental Projects & Local Plan

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Do No Harm (DNH) analysis for selected solution	Prior to posting selected solution
Post selected solution(s)	Following completion of DNH analysis
Stakeholder comments	10 days prior to Local Plan Submission for integration into RTEP
Local Plan submitted to PJM for integration into RTEP	Following review and consideration of comments received after posting of selected solutions

# Revision History

07/26/2024– V1 – Original version posted to [pjm.com](https://pjm.com)





**I. NECESSITY FOR THE PROPOSED PROJECT**

- B. [1] Detail the engineering justifications for the proposed project (for example, provide narrative to support whether the proposed project is necessary to upgrade or replace an existing facility, to significantly increase system reliability, to connect a new generating station to the Applicant's system, etc.). [2] Describe any known future project(s), including but not limited to generation, transmission, delivery point or retail customer projects, that require the proposed project to be constructed. [3] Verify that the planning studies used to justify the need for the proposed project considered all other generation and transmission facilities impacting the affected load area, including generation and transmission facilities that have not yet been placed into service. [4] Provide a list of those facilities that are not yet in service.**

Response: [1] Engineering Justification for the Project

For a detailed description of the engineering justification of the proposed Rebuild Project, see Section I.A.

[2] Known Future Projects

Significant future load growth is expected in the service area. The F2PPC has been experiencing increased interest from data center developers since approximately 2022 and Dom LSE has submitted ten DP requests to either begin or study interconnection for projects with a projected load of close to 600 MW by 2028 and 3,000 MW by 2032. Dom LSE also received customer load requests for (i) 13 new substations in the corridor south of Fredericksburg Substation and (ii) three new substations east of the F2PPC, with a combined projected load of over 2,700 MW by 2028 and over 5,200 MW by 2032.

Future projects dependent on this project are listed in Attachments I.A.8 and I.A.9.

[3] Planning Studies

The reliability studies conducted for this Rebuild Project and the study results are described in Section I.A.

[4] Facilities List

All approved PJM RTEP projects and associated generators are included in the 2026 RTEP model as based on PJM RTEP Protocols.

## **I. NECESSITY FOR THE PROPOSED PROJECT**

- C. Describe the present system and detail how the proposed project will effectively satisfy present and projected future electrical load demand requirements. Provide pertinent load growth data (at least five years of historical summer and winter peak demands and ten years of projected summer and winter peak loads where applicable). Provide all assumptions inherent within the projected data and describe why the existing system cannot adequately serve the needs of the Applicant (if that is the case). Indicate the date by which the existing system is projected to be inadequate.**

Response: As described in Section I.A, the F2PPC Load Area is generally defined as containing one 230 kV source, which consists of three sequential 230 kV lines, and one 115 kV source, feeding the various substations between the Fredericksburg and Possum Point terminals. The area served by the substations in the F2PPC is defined, generally, as the area in Stafford County paralleling Interstate 95, north of the Rappahannock River, east to the Potomac River and west along Route 17 to Hartwood Road. It also includes the areas, both north and south, around Stafford Regional Airport, as well as the area around Garrisonville Substation, north to MCBQ in Stafford County and the Town of Quantico and MCBQ in Prince William County. Attachment I.G.1 shows the portion of the Company's transmission system in the area of the Rebuild Project. The full F2PPC area is described in detail below; however, the scope of the Rebuild Project is only between Aquia Harbour Station and Possum Point Station.

### **Fredericksburg to Possum Point Corridor ("F2PPC")**

#### **Fredericksburg to Cranes Corner**

The existing electric transmission corridor between the Company's Fredericksburg Substation and Possum Point Station switchyard is approximately 24.5 miles long. For approximately 0.7 mile heading roughly north from Fredericksburg Substation, the corridor contains two 230 kV lines on double circuit, weathering steel monopole structures – Line #2157 (Fredericksburg-Cranes Corner) and Line #2083 (Fredericksburg-Birchwood NUG). The corridor also contains one 115 kV line on single circuit, two-pole wooden H-frame structures – Line #29 (Fredericksburg-Possum Point). Up to the point where the corridor reaches Hospital Junction, Line #2157 is on the west side of the corridor, Line #2083 is in the middle, and Line #29 is on the east side of the corridor. Just after crossing Mary Washington Boulevard, Line #29 crosses under Lines #2083 and #2157 as the corridor splits and Line #2083 heads roughly east toward Birchwood NUG while Line #2157 and Line #29 continue roughly north, each on single circuit, two-pole wooden H-frame structures for approximately 3.8 miles to Cranes Corner Substation, with Line #2157 on the east side of the corridor and Line #29 on the west side. (Note: approximately 0.8 mile north of Hospital Junction, the transmission corridor crosses the Rappahannock River, leaving the City of Fredericksburg and crossing into Stafford County)

At Cranes Corner Substation, Line #29 continues past the substation while Line #2157 terminates into a 230 kV breaker and leaves the substation as Line #2104 (Cranes Corner-Aquia Harbour). There are two 230-34.5 kV distribution transformers, 45 MVA Transformer #1 and 75 MVA Transformer #2, that feed a total of approximately 15,983 customers from six 34.5 kV distribution circuits.

Approximately 0.7 mile roughly northeast of Cranes Corner Substation, the corridor makes a more northerly turn at which point Line #29 crosses under Line #2104 (“Cranes Crossing”) and the lines switch positions as they continue to travel north, with Line #29 on the east side of the corridor and Line #2104 on the west. Also, approximately 0.3 mile north of Cranes Crossing on the west side of the right-of-way is the Dogwood Air Park, an aviation-oriented residential community surrounding a 4000-foot runway, bounded by the transmission corridor to the east and Route 1 to the west.

#### *Cranes Corner to Aquia Harbor*

Approximately 2.1 miles further north in the corridor from Cranes Crossing is the future Stafford Technology Park (“STP”) data center development which will be developed on both sides of the Line #2104/Line #29 corridor and is discussed further in the Future Projects section.

Continuing north approximately 2.3 miles from the STP development is another data center development, Spartan, which is located on the west side of the Line #2104/Line #29 corridor and was discussed in Section I.B above.

On the east side of the corridor at the Spartan development, 500 kV Line #568 (Ladysmith-Possum) enters the right-of-way on single circuit lattice towers and continues north on the east side of the corridor with Line #2104 on the west side and Line #29 in the middle.

Approximately 2.6 miles north of where Line #568 enters the corridor at the Spartan development, Stafford Substation is tapped from Line #2104, on the west side of the right-of-way. Stafford Substation consists of two 230-34.5 kV distribution transformers, 84 MVA Transformer #1 and 75 MVA Transformer #2, that feed a total of approximately 18,924 customers from six 34.5 kV distribution circuits.

Continuing approximately 0.3 mile north of Stafford Substation to Aquia Harbour Station, Line #568 bypasses Aquia Harbour Station on the east side of the corridor while Line #29 passes through Aquia Harbour Station by utilizing the upper position of the double circuit backbone within the station. Line #2104 terminates in the lower position of the double circuit backbone at Aquia Harbour Station where it drops into a line terminal created by “normally closed” tie-breaker 2104T2119 and “normally open” tie-breaker 252T2104. On the other side of the double circuit backbone at Aquia Harbour Station, Line #252 (Aquia Harbour-Possum Point)

terminates into the double circuit backbone where it drops into a line terminal created by “normally closed” tie-breaker 252T2120 and the previously mentioned “normally open” tie-breaker 252T2104.

Lines #2119 and #2120 are both underground 230 kV lines that loop in-and-out approximately 5.8 miles from Aquia Harbour Station to Garrisonville Substation.

At Garrisonville Substation, Lines #2119 and #2120 terminate in a 230kV four-breaker ring bus that is the source for two 230 kV 50-100 MVAR variable shunt reactors, as well as two 230-34.5 kV distribution transformers, 84 MVA Transformer #1 and 84 MVA Transformer #2, that feed a total of approximately 7,457 customers from four 34.5 kV distribution circuits.

Leaving Aquia Harbour Station to the north, Line #252 and Line #29 share double circuit lattice towers with Line #252 on the west side of the tower and Line #29 on the east side of the tower (but in the middle position within the corridor since Line #568 occupies the eastern side of the right-of-way).

Approximately 3.8 miles north of Aquia Harbour Station is Aquia Substation which is tapped from Line #252 and located within the MCBQ. There is a single 230 kV -34.5 kV, 33.6 MVA distribution transformer that feeds about 3,374 customers from a single 34.5 kV distribution circuit.

#### *Aquia Harbour to Possum Point/MCBQ*

Continuing north past Aquia Substation for approximately 1.4 miles, the corridor crosses Route 1 at the North Branch Chopawamsic Creek and enters Prince William County. The three lines (Lines #252, #29, and #568) continue in the corridor together for approximately 1.6 miles, traversing Locust Shade Park, Interstate 95, and the eastern edge of Quantico National Cemetery before Line #252 and Line #29 turn east by crossing under Line #568 between structures 568/38 and 568/39 (“Cemetery Junction”).

At Cemetery Junction, Line #568 continues north for approximately 0.8 miles before turning east and continuing for approximately 5.5 miles to the 500 kV switchyard at Possum Point Power Station. Line #252 and Line #29 continue east from Cemetery Junction (crossing back over I-95 and Rt. 1) on shared double circuit lattice towers for approximately 1.8 miles to Fuller Road Substation, with Line #252 on the north side of the tower and Line #29 on the south side of the tower.

At Fuller Road Substation, Line #252 is tapped as the source while Line #29 passes through the substation without touching any structures. There is a single 230 kV -34.5 kV, 33.6 MVA distribution transformer that feeds about 424 customers from two 34.5 kV distribution circuits.

Approximately 0.2 miles east of Fuller Road Substation, Lines #252 and #29 turn northeast at Structure #252/5568 (#29/1835) (“Quantico Tap”) and continue for approximately 2.7 miles to Structure #252/5583 (#29/1850) where they split, with Line #252 continuing approximately 0.5 miles on predominately single circuit, two-pole H-frame structures to the 230 kV switchyard at Possum Point Station, and Line #29 continuing approximately 0.7 miles on predominately single circuit, two-pole H-frame structures to the 115 kV switchyard at Possum Point Station.

At the Quantico Tap, Line #29 continues as a radial for approximately 1.7 miles on single circuit, two-pole wooden H-frame structures to Quantico Substation.

At Quantico Substation, there are two 115 kV-13.2 kV distribution transformers, 22.4 MVA Transformer #1 and 22.4 MVA Transformer #2, that feed approximately 450 customers, including MCBQ, from three 13.2 kV distribution circuits.

### Projected Load Growth

Attachment I.C.1 shows the five-year summer and winter historical peaks (coincident with the system peak) for the existing substations in the F2PPC, while Attachment I.C.2 and Attachment I.C.3 show the summer and winter projected loads, respectively.

Projected loads from the 16 additional DP requests discussed in Section 1.A are shown in Attachment I.C.4. The projections from the new DP requests are estimated to drive the F2PPC total direct-connected load to close to 600 MW by 2028 and 3,000 MW by 2032. Additionally, in the corridor south of Fredericksburg Substation, the Company received DP Requests for 13 new substations to serve the growing data center load. The projected new load is estimated to be over 2,600 MW by 2028 and over 4,700 MW by 2032. Further, east of the F2PPC, Dom LSE submitted DP requests for three new substations with projected loads over 100 MW by 2028 and over 500 MW by 2032. These 26 DP requests (ten in the F2PPC, 13 south, three east) represent additional load projections of over approximately 3,000 MW in 2028 and over approximately 7,800 MW in 2032. Due to volume of DP requests, the Company is still working to model the impacts of this unprecedented load growth; however, given the reliability upgrades that have already been identified in the F2PPC, the Company’s strategy to maximize the number of lines that can fit into the existing rights-of-way by rebuilding existing single circuit structures with double circuit structures, utilizing current 230 kV standards with a minimum normal summer rating of 1,573 MVA, is prudent utility practice.

Completing the Rebuild Project by rebuilding Lines #29, #252, #2083 and #568, including Lines #29, #252, #2083 on double circuit monopole structures, will enable the Company to maintain reliable service to accommodate the significant load growth anticipated in this area of the Company’s transmission system as discussed in Section I.A. In addition, existing Lines #29 and #252 cannot continue to adequately serve the needs of the Company and its customers because of the

aging infrastructure on both lines and overloading issues on Line #252, as discussed in Section I.A.

The Company has created a plan to address its end-of-life facilities, setting target completion dates for end-of-life projects based on the condition of the facilities, the Company's resources, and the need to schedule outages. The in-service date for the Rebuild Project is January 31, 2029, which reflects the need confirmed by industry guidelines and balanced against the timeline for permitting, construction, and obtaining necessary outages.

## Attachment I.C.1 - Historical Summer and Winter Loads in the F2PPC

SUMMER LOADS	Historical MW (Coincident with System Peak)				
Date	7/20/2019	7/20/2020	8/12/2021	8/9/2022	7/28/2023
Quantico TX#1	n/a	7.4	7.2	7.5	6.5
Quantico TX#2	n/a	7.4	7.2	7.5	6.5
Aquia TX#1	28.5	25.6	28.9	24.5	23.5
Cranes Corner TX#1	37.3	19.5	19.6	38.2	37.4
Cranes Corner TX#2	44.4	56.6	56.3	41.7	46.2
Garrisonville TX#1	43.1	48.1	46.6	47.4	44.8
Stafford TX#1	59.0	62.6	59.9	60.9	59.9
Stafford TX#2	46.9	52.6	48.1	48.6	49.2
Fuller Road TX#1	7.3	13.4	11.8	12.6	12.3
<b>TOTAL</b>	<b>266.5</b>	<b>293.2</b>	<b>285.6</b>	<b>288.9</b>	<b>286.3</b>
WINTER LOADS	Historical MW (Coincident with System Peak)				
Date	1/31/2019	1/21/2020	1/29/2021	1/27/2022	12/24/2022
Quantico TX#1	n/a	4.9	4.4	4.7	7.8
Quantico TX#2	n/a	4.9	4.4	4.7	0.2
Aquia TX#1	26.7	22.5	21.9	23.9	23.4
Cranes Corner TX#1	40.9	16.1	16.2	39.3	43.2
Cranes Corner TX#2	45.0	41.3	43.0	41.6	44.8
Garrisonville TX#1	56.4	44.1	44.1	54.0	56.9
Stafford TX#1	64.3	51.6	50.4	58.8	61.9
Stafford TX#2	57.2	42.1	41.5	50.6	56.4
Fuller Road TX#1	9.0	7.9	7.6	8.1	7.1
<b>TOTAL</b>	<b>299.5</b>	<b>235.4</b>	<b>233.5</b>	<b>285.7</b>	<b>301.7</b>

## Attachment I.C.2 - Projected Summer Loads in the F2PPC

SUMMER LOADS		Projected MW									
Year (August)	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	
EXISTING LOADS	Quantico TX#1	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	
	Quantico TX#2	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	
	Aquia TX#1	23.5	23.5	23.5	23.5	23.5	23.5	23.5	23.5	23.5	
	Cranes Corner TX#1	37.4	37.4	37.4	37.4	37.4	37.4	37.4	37.4	37.4	
	Cranes Corner TX#2	52.2	47.9	47.9	47.9	47.9	47.9	47.9	47.9	47.9	
	Garrisonville TX#1	44.8	44.8	44.8	44.8	44.8	44.8	44.8	44.8	44.8	
	Stafford TX#1	59.9	59.9	59.9	59.9	59.9	59.9	59.9	59.9	59.9	
	Stafford TX#2	49.2	49.2	49.2	49.2	49.2	49.2	49.2	49.2	49.2	
	Fuller Road TX#1	12.3	12.3	12.3	12.3	12.3	12.3	12.3	12.3	12.3	
	Spartan	18.1	28.9	71.5	71.5	71.5	71.5	71.5	71.5	71.5	
PROPOSED LOADS	Widewater*	0.0	0.0	0.0	0.0	0.0	0.0	22.0	66.0	121.0	
	Centreport	0.0	0.0	0.0	4.0	48.0	136.0	136.0	136.0	136.0	
	Alto	0.0	0.0	0.0	32.0	66.0	213.0	213.0	213.0	213.0	
	Woodcutters	0.0	0.0	0.0	0.0	100.0	250.0	350.0	800.0	1300.0	
	Baritone	0.0	0.0	0.0	0.0	0.0	32.0	111.0	183.0	183.0	
	Classical*	0.0	0.0	0.0	0.0	0.0	0.0	8.0	60.0	175.0	
	Opera	0.0	0.0	0.0	0.0	0.0	0.0	54.0	170.0	255.0	
	Tenor*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	66.0	
	Soprano	0.0	0.0	0.0	0.0	18.0	116.0	219.0	255.0	255.0	
	Total EXISTING	292.3	288.0	288.0	288.0	288.0	288.0	288.0	288.0	288.0	
Total PROPOSED	18.1	28.9	71.5	107.5	303.5	818.5	1162.5	1910.5	2627.5	2775.5	
	Total OVERALL	310.4	316.9	359.5	395.5	591.5	1106.5	1450.5	2198.5	3063.5	
* = "Engineering Only" DP Request											



## Attachment I.C.3 - Projected Winter Loads in the F2PPC

WINTER LOADS		Projected MW										
Year (February)	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033		
EXISTING LOADS	Quantico TX#1	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
	Quantico TX#2	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
	Aquia TX#1	23.4	23.4	23.4	23.4	23.4	23.4	23.4	23.4	23.4	23.4	
	Cranes Corner TX#1	43.2	43.2	43.2	43.2	43.2	43.2	43.2	43.2	43.2	43.2	
	Cranes Corner TX#2	44.8	50.8	44.6	44.6	44.6	44.6	44.6	44.6	44.6	44.6	
	Garrisonville TX#1	56.9	56.9	56.9	56.9	56.9	56.9	56.9	56.9	56.9	56.9	
	Stafford TX#1	61.9	61.9	61.9	61.9	61.9	61.9	61.9	61.9	61.9	61.9	
	Stafford TX#2	56.4	56.4	56.4	56.4	56.4	56.4	56.4	56.4	56.4	56.4	
	Fuller Road TX#1	7.1	7.1	7.1	7.1	7.1	7.1	7.1	7.1	7.1	7.1	
	Spartan	0.0	18.0	33.7	64.9	64.9	64.9	64.9	64.9	64.9	64.9	
PROPOSED LOADS	Widewater*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	22.0	66.0	
	Centreport	0.0	0.0	0.0	4.0	48.0	136.0	136.0	136.0	136.0	136.0	
	Alto	0.0	0.0	0.0	32.0	66.0	213.0	213.0	213.0	213.0	213.0	
	Woodcutters	0.0	0.0	0.0	0.0	100.0	250.0	350.0	800.0	1300.0	1300.0	
	Baritone	0.0	0.0	0.0	0.0	0.0	32.0	111.0	183.0	183.0	183.0	
	Classical*	0.0	0.0	0.0	0.0	0.0	0.0	8.0	60.0	155.0	175.0	
	Opera	0.0	0.0	0.0	0.0	0.0	0.0	54.0	170.0	242.0	255.0	
	Tenor*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.0	66.0	
	Soprano	0.0	0.0	0.0	0.0	18.0	116.0	219.0	255.0	255.0	255.0	
	Total EXISTING	301.7	307.7	301.5	301.5	301.5	301.5	301.5	301.5	301.5	301.5	
EXISTING LOADS	Total PROPOSED	0.0	18.0	33.7	100.9	296.9	811.9	1155.9	1881.9	2576.9	2713.9	
	Total OVERALL	301.7	325.7	335.2	402.4	598.4	1113.4	1457.4	2183.4	2878.4	3015.4	

\* = "Engineering Only," DP Request

\* = "Engineering Only" DP Request

## Attachment I.C.4 - Proposed New Loads East and South of the F2PPC

LOADS (East)		Projected MW									
Year		2024	2025	2026	2027	2028	2029	2030	2031	2032	2033
Caboose		0.0	0.0	6.0	30.0	84.0	84.0	84.0	12.0	140.0	180.0
Freight		0.0	0.0	0.0	0.0	2.0	40.0	90.0	120.0	140.0	160.0
Locomotive		0.0	0.0	0.0	0.0	18.0	116.0	219.0	255.0	255.0	255.0
Total PROPOSED		0.0	0.0	6.0	30.0	104.0	240.0	393.0	387.0	535.0	595.0
* = "Engineering Only" DP Request											
LOADS (South)		Projected MW									
Year		2024	2025	2026	2027	2028	2029	2030	2031	2032	2033
New Post		0.0	66.0	99.0	237.0	237.0	237.0	237.0	237.0	237.0	237.0
River View		0.0	7.0	47.0	108.0	108.0	108.0	108.0	108.0	108.0	108.0
Caroline County*		0.0	5.0	20.0	50.0	100.0	200.0	300.0	400.0	500.0	600.0
Hunters Ridge		0.0	55.0	171.0	400.0	600.0	600.0	800.0	800.0	800.0	800.0
Belvedere		0.0	0.0	92.0	210.0	285.0	285.0	285.0	285.0	285.0	285.0
Slayden Creek		0.0	0.0	5.0	92.0	210.0	210.0	210.0	210.0	210.0	210.0
Matta		0.0	0.0	33.0	83.0	149.0	210.0	281.0	352.0	462.0	572.0
Hickory Ridge*		0.0	0.0	146.0	146.0	290.0	290.0	290.0	290.0	290.0	290.0
Ruther Glen		0.0	0.0	170.0	170.0	338.0	338.0	338.0	548.0	548.0	548.0
Carmel Church		0.0	0.0	18.0	80.0	125.0	187.0	299.0	299.0	299.0	299.0
Falling Creek		0.0	0.0	0.0	0.0	5.0	92.0	210.0	210.0	210.0	210.0
Tidewater		0.0	0.0	0.0	0.0	0.0	92.0	210.0	285.0	285.0	285.0
Kettler Crossroads*		0.0	0.0	0.0	81.0	189.0	297.0	400.0	450.0	500.0	550.0
Total PROPOSED		0.0	133.0	801.0	1657.0	2636.0	3146.0	3968.0	4474.0	4734.0	4994.0
= "Engineering Only" DP Request											

**I. NECESSITY FOR THE PROPOSED PROJECT**

- D. If power flow modeling indicates that the existing system is, or will at some future time be, inadequate under certain contingency situations, provide a list of all these contingencies and the associated violations. Describe the critical contingencies including the affected elements and the year and season when the violation(s) is first noted in the planning studies. Provide the applicable computer screenshots of single-line diagrams from power flow simulations depicting the circuits and substations experiencing thermal overloads and voltage violations during the critical contingencies described above.**

Response: See Section I.A.

## I. NECESSITY FOR THE PROPOSED PROJECT

- E. Describe the feasible project alternatives, if any, considered for meeting the identified need including any associated studies conducted by the Applicant or analysis provided to the RTO. Explain why each alternative was rejected.

Response: Feasible Project Alternatives

The Company did not identify alternatives to PJM for the Rebuild Project because there is no alternative that can satisfy the Rebuild Project's three primary drivers, which are to: (a) maintain the structural integrity and reliability of the networked transmission system; (b) resolve identified violations of the mandatory NERC Reliability Standards; and (c) provide for future load growth in the area.<sup>13</sup>

### Analysis of Demand-Side Resources

Pursuant to the Commission's November 26, 2013, Order entered in Case No. PUE-2012-00029, and its November 1, 2018, Final Order entered in Case No. PUR-2018-00075 ("2018 Final Order"), the Company is required to provide an analysis of demand-side resources ("DSM") as incorporated into the Company's planning studies. DSM is the broad term that includes both energy efficiency ("EE") and demand response ("DR"). In this case, PJM and the Company have identified a need for the proposed Rebuild Project based on the need to maintain the overall long-term reliability of its transmission system and to comply with mandatory NERC Reliability Standards.<sup>14</sup> Notwithstanding, when performing an analysis based on PJM's 50/50 load forecast, there is no adjustment in load for DR programs because PJM only dispatches DR when the system is under stress (*i.e.*, a system emergency). Accordingly, while existing DSM is considered to the extent the load forecast accounts for it, DR that has been bid previously into PJM's capacity market is not a factor in this particular application because of the identified need for the Rebuild Project. Based on these considerations, the evaluation of the Rebuild Project demonstrated that despite accounting for DSM consistent with PJM's methods, the Rebuild Project is necessary.

Incremental DSM also will not eliminate the need for the Rebuild Project. As reflected in Attachments I.C.1–I.C.3, the highest annual projected peak load over the next 10 years in the F2PPC is projected to total approximately 3,000 MW (including future planned stations). By way of comparison, statewide, the Company achieved demand savings of 276.5 MW (net) / 350.0 MW (gross) from its DSM programs in 2023.

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<sup>13</sup> See Section I.A.

<sup>14</sup> While the PJM load forecast does not directly incorporate DR, its load forecast incorporates variables derived from Itron that reflect EE by modeling the stock of end-use equipment and its usages. Further, because PJM's load forecast considers the historical non-coincident peak ("NCP") for each load serving entity ("LSE") within PJM, it reflects the actual load reductions achieved by DSM programs to the extent an LSE has used DSM to reduce its NCPs.

## **I. NECESSITY FOR THE PROPOSED PROJECT**

### **F. Describe any lines or facilities that will be removed, replaced, or taken out of service upon completion of the proposed project, including the number of circuits and normal and emergency ratings of the facilities.**

Response: The approximately 0.6 mile segment of Line #29 from Structure #252/5583 (#29/1850) to the Possum Point Station 115 kV switchyard will be removed when Line #29 is converted to 230 kV operation.

Between Aquia Harbour Station and Possum Point Station, a total of 65 double circuit lattice steel tower structures will be removed from Lines #29 and Line #252. These lines are currently supported on and share the same double circuit latticed steel tower structures. Additionally, one single circuit 3-pole guyed wood structure, four single circuit H-frame wood structures, and two single circuit latticed steel frame structures will be removed from Line #29 only. Furthermore, two single circuit 3-pole guyed wood structures and three single circuit H-frame wood structures will be removed from Line #252 only.

The Company will replace these structures with 101 230 kV tubular pole structures consisting of 74 double circuit V-String suspension structures and 24 double circuit double dead-end (“DDE”) structures, three single circuit pole DDE structures, all constructed of weathering steel. Furthermore, the Company is also adding a total of 101 230 kV tubular pole structures parallel to the rebuilt Line #29 and Line #252 in the same corridor to add two future circuits. These structures are comprised of 26 double circuit DDE structures and 75 double circuit V-String suspension structures.

Between Aquia Harbour Station and Cemetery Junction, 39 single circuit 500 kV steel lattice towers will be removed from Line #568. The Company will replace these structures with 40 500 kV single circuit steel pole structures, comprised of ten single circuit DDE structures and 30 single circuit V-String suspension structures.

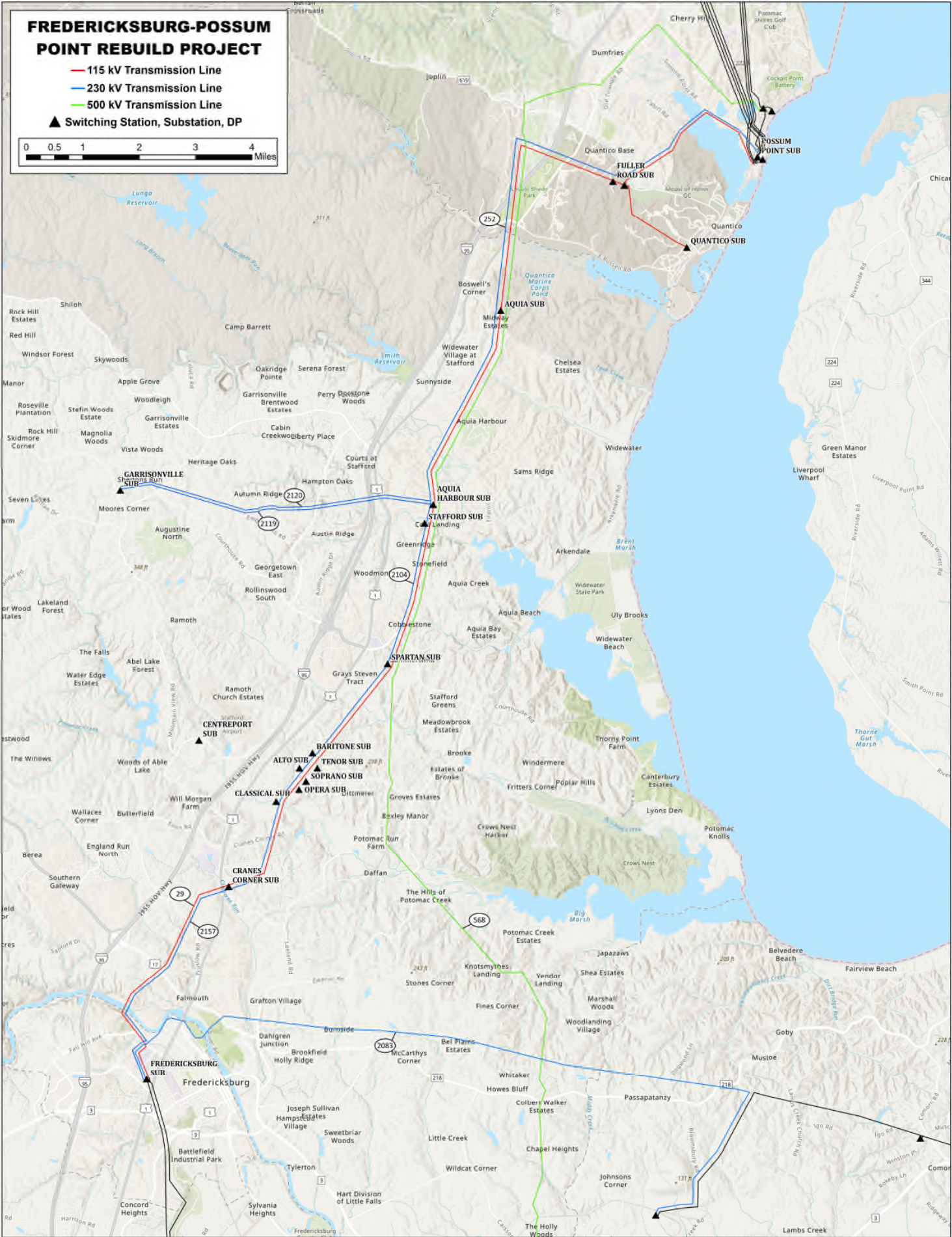
The new construction will optimize the number of lines that can fit in the right-of-way to serve the significant load growth anticipated in the area.

**I. NECESSITY FOR THE PROPOSED PROJECT**

- G. Provide a system map, in color and of suitable scale, showing the location and voltage of the Applicant's transmission lines, substations, generating facilities, etc., that would affect or be affected by the new transmission line and are relevant to the necessity for the proposed line. Clearly label on this map all points referenced in the necessity statement.**

Response: See Attachment I.G.1.





## **I. NECESSITY FOR THE PROPOSED PROJECT**

### **H. Provide the desired in-service date of the proposed project and the estimated construction time.**

Response: The desired in-service target date for the Rebuild Project is January 31, 2029. The Company estimates it will take approximately 46 months after a final order from the Commission for detailed engineering, materials procurement, permitting, real estate, and construction of the Rebuild Project. Accordingly, to support this estimated construction timeline and construction plan, the Company respectfully requests a final order by February 28, 2025. Should the Commission issue a final order by February 28, 2025, the Company estimates that construction should begin in March 2026 with the Rebuild Project to be completed by the in-service target date of January 31, 2029. This schedule is contingent upon obtaining the necessary permits and careful coordination of outages, the latter of which may be particularly challenging due to the amount of new load growth, rebuilds, and new builds scheduled to occur in this load area. Dates may need to be adjusted based on permitting delays or design modifications to comply with additional agency requirements identified during the permitting application process, as well as the ability to schedule outages, and unpredictable delays due labor shortages or materials/supply issues. Based on the Rebuild Project's complexity, there may be delays with procurement of materials.

Any adjustments to the Rebuild Project schedule resulting from these or similar challenges could necessitate a minimum of a six- to twelve-month delay in the targeted in-service date. Accordingly, for purposes of judicial economy, the Company requests that the Commission issue a final order approving both a desired in-service target date (*i.e.*, January 31, 2029) and an authorization sunset date (*i.e.*, January 31, 2030) for energization of the Project.

In addition, the Company is actively monitoring regulatory changes and requirements associated with the Northern Long Eared Bat ("NLEB") and how it could potentially impact construction timing associated with time of year restrictions ("TOYRs"). The U.S. Fish and Wildlife Service ("USFWS") previously indicated that it planned to issue final NLEB guidance to replace the interim guidance by April 1, 2024; however, the interim guidance has been extended by USFWS until late summer 2024. In the meantime, the USFWS issued several draft guidance documents for public review and comment. The Company actively is tracking updates from the USFWS with respect to the final guidance. Once issued, the Company plans to review and follow the final guidance to the extent it applies to the Company's projects. Until the final guidance is issued, the Company will continue following the interim guidance. For projects that may require additional coordination, the Company will coordinate with the USFWS.

The Company is also continuing to track potential regulatory changes associated with the potential up-listing of the Tricolored bat ("TCB"). On September 14, 2022, the USFWS published the proposed rule to the Federal Register to list the



TCB as endangered under the Endangered Species Act (“ESA”). On April 1, 2024, the USFWS issued draft guidance for the NLEB and TCB for public review and comment. The USFWS also recently extended its Final Rule issuance target from September 2023 to September 2024. The Company is actively tracking this ruling and evaluating the effects of potential outcomes on Company projects’ permitting, construction, and in-service dates, including electric transmission projects.

**I. NECESSITY FOR THE PROPOSED PROJECT**

- I. Provide the estimated total cost of the project as well as total transmission-related costs and total substation-related costs. Provide the total estimated cost for each feasible alternative considered. Identify and describe the cost classification (e.g. “conceptual cost,” “detailed cost,” etc.) for each cost provided.**

Response: The estimated conceptual cost of the Rebuild Project is approximately \$205.5 million (in 2024 dollars).<sup>15</sup>

For the reasons discussed in Section I.A, the Company rejected the option to rebuild without the proposed double circuit structures on Lines #29, #252, and #2083.

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<sup>15</sup> The cost of the work associated with the work at the Fredericksburg, Cranes Corner, Fuller Road, Ladysmith, and Aquia Substations and Aquia Harbour and Possum Point Stations is approximately \$96.8 million (in 2024 dollars). The Company considers this work and the associated costs separate from the Rebuild Project.

## **I. NECESSITY FOR THE PROPOSED PROJECT**

- J. If the proposed project has been approved by the RTO, provide the line number, regional transmission expansion plan number, cost responsibility assignments, and cost allocation methodology. State whether the proposed project is considered to be a baseline or supplemental project.**

Response: The proposed need for the EOL rebuild of Lines #29 and #252 between Aquia Harbour Station and Possum Point Station was first presented to the PJM stakeholders at the TEAC Meeting on August 10, 2021. The proposed solution for the rebuild of these lines was presented at the October 5, 2021, TEAC Meeting. Attachments I.A.3 and I.A.4 contain the Need and Solution slides, respectively, which were presented at the TEAC Meetings. Subsequently, PJM assigned supplemental identification number “s2705” to the rebuild of Lines #29 and #252 between Aquia Harbour and Possum Point. Coupled with baseline upgrade project “b2981” (which proposes to rebuild Line #29 from Fredericksburg to Aquia Harbour and was approved by the PJM Board at its February 13, 2018, meeting as an EOL project (proposed in Company filing PUR-2024-00035)), Line #29 will be rebuilt to 230kV standards for the entirety between Fredericksburg Substation and Possum Point Station.

Additionally, to resolve a potential 300 MW load-loss violation of mandatory NERC reliability standards, the conversion of Line #29 to 230kV operation was approved by the PJM Board at its February 16, 2022, TEAC Meeting as a baseline upgrade, and assigned the identification number “b3694.” Attachments I.A.5, I.A.6, and I.A.7 contain the slides presented by PJM (first pass and second pass) and the Board Approval, respectively.

The Rebuild Project is presently 100% cost allocated to the DOM Zone.

**I. NECESSITY FOR THE PROPOSED PROJECT**

- K. If the need for the proposed project is due in part to reliability issues and the proposed project is a rebuild of an existing transmission line(s), provide five years of outage history for the line(s), including for each outage the cause, duration and number of customers affected. Include a summary of the average annual number and duration of outages. Provide the average annual number and duration of outages on all Applicant circuits of the same voltage, as well as the total number of such circuits. In addition to outage history, provide five years of maintenance history on the line(s) to be rebuilt including a description of the work performed as well as the cost to complete the maintenance. Describe any system work already undertaken to address this outage history.**

Response: Not applicable. The need for the Rebuild Project is not driven by outage history, but rather by the need to maintain reliable service for the load growth anticipated in the area, to replace transmission infrastructure nearing end of life, and to address projected overloading issues. See Sections I.A and I.C.

**I. NECESSITY FOR THE PROPOSED PROJECT**

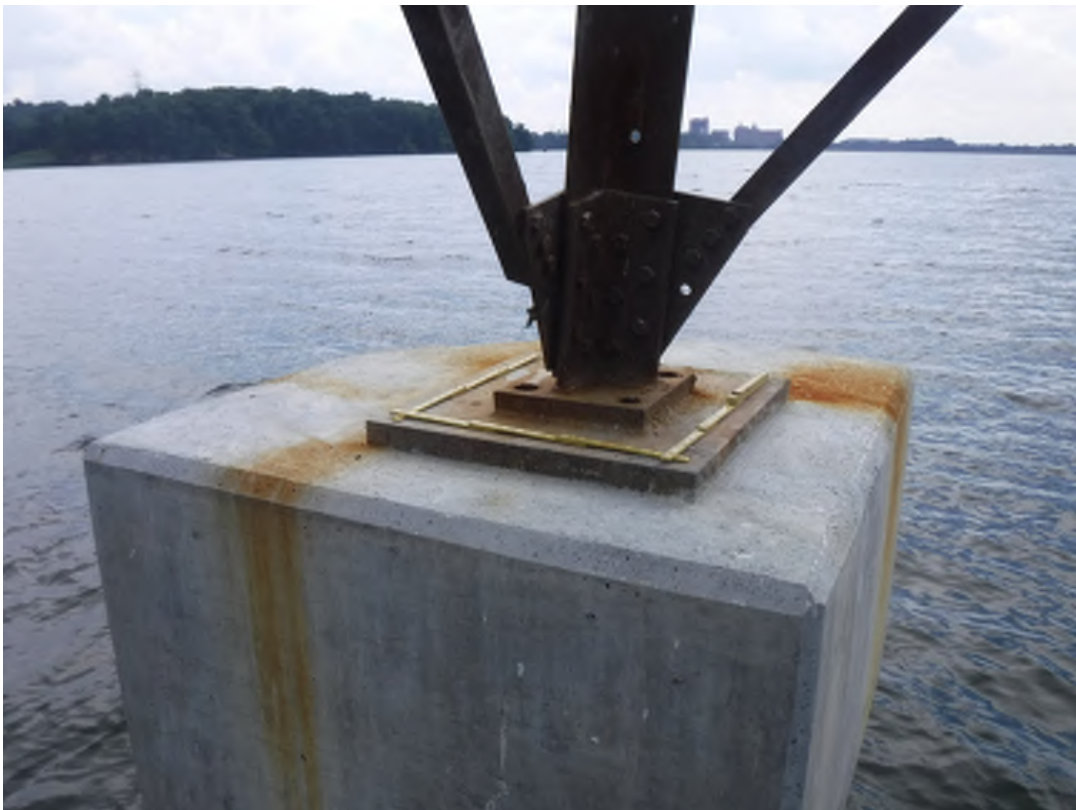
- L. If the need for the proposed project is due in part to deterioration of structures and associated equipment, provide representative photographs and inspection records detailing their condition.**

Response: See Attachment I.L.1 for photographs of the deterioration of structures on Lines #29 and #252. Section I.A provides further detail on the condition of these deteriorating structures. See Attachment I.L.2 for sample inspection records of Lines #29 and #252.

















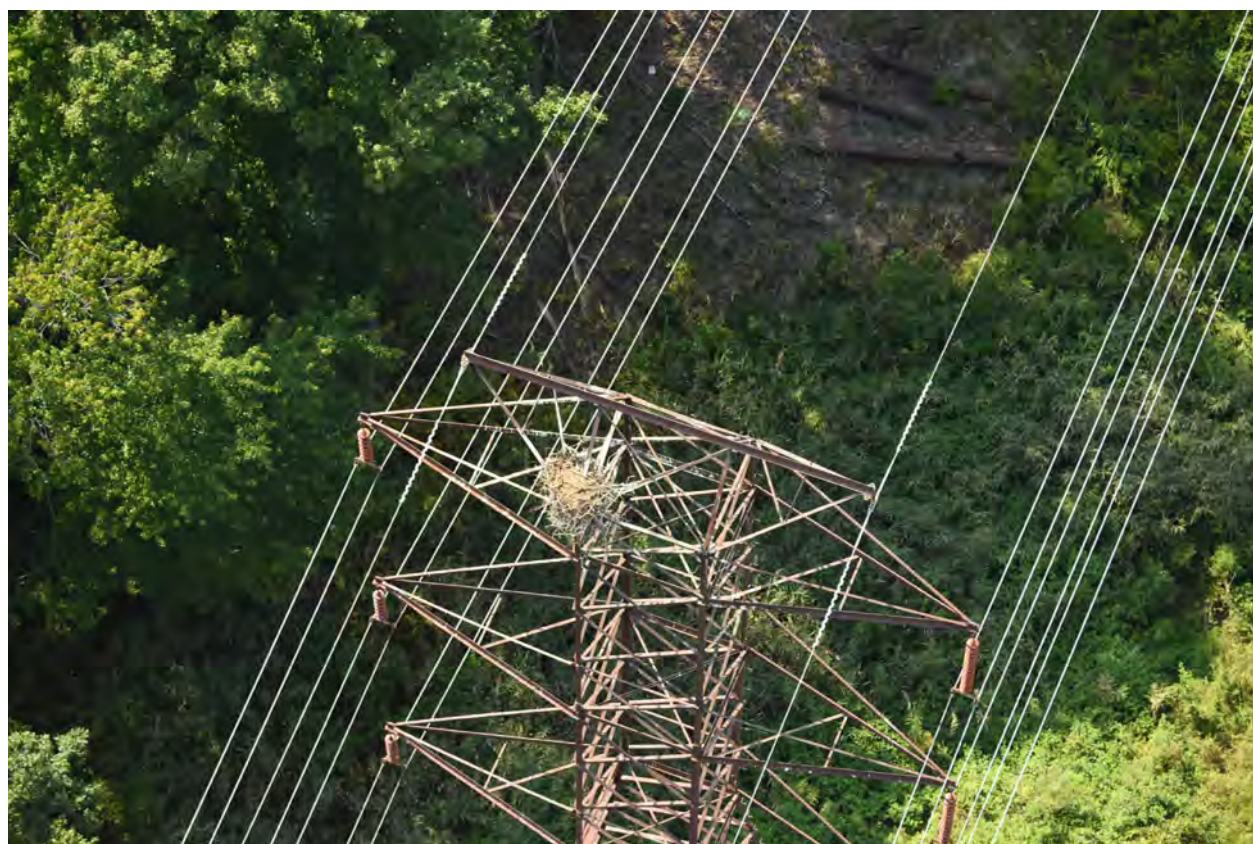








Line 29 and 252



OUTSTANDING NOTIFICATIONS - LINE 29 & 252							
NOTIFICATION	LINE/STR	CAUSE GROUP	CAUSE CODE	CAUSE TEXT	NOTIF. DATE	REPORTED BY	
-	25/519, 29/1786	Insulator Conductor	Wire Position L,M,A,T,B	M	10/26/2020	TIM0032	
-	25/519, 29/1786	Insulator Conductor	Broken- L-Leave, R-Replace	L	10/26/2020		
-	25/519, 29/1786	Insulator Conductor	Cond Insulator- Other=	Chipped bell	10/26/2020		
-	25/519, 29/1786	Insulator Conductor	(H) Hot End / (C) Cold End	C	10/26/2020		
-	25/519, 29/1805	Insulator Conductor	Wire Position L,M,A,T,B	C, R, T	10/28/2020	TIM0022	
-	25/519, 29/1805	Insulator Conductor	Broken- L-Leave, R-Replace	L	10/28/2020		
-	25/519, 29/1805	Insulator Conductor	Cond Insulator- Other=	Chipped bell	10/28/2020	TIM0032	
-	25/519, 29/1805	Insulator Conductor	(H) Hot End / (C) Cold End	C	10/28/2020		
-	25/519, 29/1805	Foundation	Foundation Other=	24 Fiberglass breakers need replaced	3/30/2017	JEREMY3	
-	25/519, 29/1805	Foundation	Foundation Other=	need 12 ladders	3/30/2017		
-	25/519, 29/1805	Guy	Guy Other=	Fuzzy breakers	10/28/2020	TIM0032	
-	25/519, 29/1840	Insulator Conductor	Wire Position L,M,A,T,B	1 #5, M #7, B #4	4/10/2017	TIM0032	
-	25/519, 29/1840	Insulator Conductor	(H) Hot End / (C) Cold End	C, R, T	4/10/2017		
-	25/519, 29/1840	Insulator Conductor	Broken- L-Leave, R-Replace	Replace #5, #7, #4	4/10/2017		
-	25/519, 29/1840	Insulator Conductor	(H) Hot End / (C) Cold End	H, #4	4/10/2017		
-	25/519, 29/1840	Insulator Conductor	Wire Position L,M,A,T,B	B,M	4/10/2017		
-	25/519, 29/1840	Insulator Conductor	Broken- L-Leave, R-Replace	L	4/10/2017		
-	25/519, 29/1840	Insulator Conductor	(H) Hot End / (C) Cold End	H/C	4/10/2017		
-	25/519, 29/1841	Insulator Conductor	Wire Position L,M,A,T,B	Bottom phase/left sub	10/20/2020	TIM0032	
-	25/519, 29/1841	Insulator Conductor	Cond Insulator- Other=	Chipped	10/20/2020		
-	25/519, 29/1841	Insulator Conductor	(H) Hot End / (C) Cold End	H	10/20/2020		
-	25/519, 29/1846	Conductor	Dampen(s) L-Loose, M-Missing	M	8/11/2020	BRAND58	
COMPLETED NOTIFICATIONS - LINE 29 & 252							
NOTIFICATION	LINE/STR	CAUSE GROUP	CAUSE CODE	CAUSE TEXT	NOTIF. DATE	REPORTED BY	
-	25/519, 29/1786	Conductor	Wire Position L,M,A,T,B	T, R	3/29/2017	TIM0032	
-	25/519, 29/1786	Conductor	Cotter Key-BO-Backed Out, M-M	BO @ shoe and plate	3/29/2017	TIM0032	
-	25/519, 29/1788	Equipment Needed for Repair	ATV	ATV	1/31/2007	GARY040	
-	25/519, 29/1788	Equipment Needed for Repair	Power Wagon	Power Wagon	1/31/2007	GARY040	
-	25/519, 29/1788	Work found during a routine PM	Work as a result of a PM Order	66667448	1/31/2007	GARY040	
-	25/519, 29/1788	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	Needs A120	1/31/2007	GARY040	
-	25/519, 29/1788	Grounds	Grounds - Broken	Grounds - Broken	1/31/2007		
-	25/519, 29/1789	Structure	DO NOT USE -17' Packout -3/4" Location=	DAMAGED	7/5/2012		
-	25/519, 29/1789	Structure	Str could not be inspected at this time	Structure-Str could not be inspected at	8/2/2023	JARE029	
-	25/519, 29/1789	Structure	Str could not be inspected at this time	couldn't climb active birds nest	8/2/2023	JARE029	
-	25/519, 29/1790	Structure	Environmental-Needs	Birds nest	8/2/2023	JARE029	
-	25/519, 29/1790	Structure	Str could not be inspected at this time	Structure-Str could not be inspected at	8/2/2023	JARE029	
-	25/519, 29/1790	Structure	Str could not be inspected at this time	couldn't climb active birds nest	8/2/2023	JARE029	
-	25/519, 29/1791	Work found during a routine PM	Work as a result of a PM Order	66798558	2/4/2008	RUSSELL	
-	25/519, 29/1791	Insulators - Static Insulators	Static Insulators - Broken	See text	2/4/2008	RUSSELL	
-	25/519, 29/1791	Structure	Ground Wire-M-Missing,CtCut	C	10/26/2020	TIM0032	
-	25/519, 29/1792	Work found during a routine PM	Work as a result of a PM Order	66667448	1/31/2007	RUSSELL	
-	25/519, 29/1792	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	Access Aqua Harbour	1/31/2007	RUSSELL	
-	25/519, 29/1793	Work found during a routine PM	Work as a result of a PM Order	66667448	1/31/2007	RUSSELL	
-	25/519, 29/1793	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	Access Aqua Harbour	1/31/2007	RUSSELL	
-	25/519, 29/1793	Structure - Steel	Steel - Missing/Faded Bolts	Steel - Missing/Faded Bolts	1/31/2007	RUSSELL	
-	25/519, 29/1794	Work found during a routine PM	Work as a result of a PM Order	66667448	1/31/2007	RUSSELL	
-	25/519, 29/1794	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	Access Aqua Harbour	1/31/2007	RUSSELL	
-	25/519, 29/1794	Miscellaneous	Miscellaneous - Other	Graffiti; Ref IMG0451	1/30/2009	CBH	
-	25/519, 29/1795	Work found during a routine PM	Work as a result of a PM Order	66798558	2/4/2008	RUSSELL	
-	25/519, 29/1795	Grounds	Grounds - Broken	Repair 1 4" solid ground	2/4/2008	RUSSELL	
-	25/519, 29/1795	Structure	Cotter Key-BO-Backed Out, M-Missing	Backed out key middle phase yoke play on	3/13/2023	JEREMY3	
-	25/519, 29/1796	Structure - Numbers	Numbers - Missing	Numbers - Missing	6/26/2004		
-	25/519, 29/1796	Work found during a routine PM	Work as a result of a PM Order	66667448	1/31/2007	RUSSELL	
-	25/519, 29/1796	Structure - Numbers	Numbers - Missing	Access Aqua Harbour	1/31/2007	RUSSELL	
-	25/519, 29/1797	Structure - Numbers	Numbers - Missing	Numbers - Missing	6/30/2004		
-	25/519, 29/1797	Structure	Ground Wire-M-Missing,CtCut	C	10/26/2020	TIM0032	
-	25/519, 29/1798	Miscellaneous	Need Anti Climb Sign	Need Anti Climb Sign	2/21/2000		
-	25/519, 29/1798	Insulator Conductor	Cotter Key-BO-Backed Out, M-M	BO	2/28/2017		
-	25/519, 29/1798	Insulator Conductor	(H) Hot End / (C) Cold End	H	2/28/2017		
-	25/519, 29/1799	Grounds	Grounds - Broken	Grounds - Broken	2/21/2000	RUSSELL	
-	25/519, 29/1799	Grounds	Grounds - Broken	Grounds - Broken	1/31/2001	RUSSELL	
-	25/519, 29/1799	Work found during a routine PM	Work as a result of a PM Order	66798558	2/4/2008	RUSSELL	
-	25/519, 29/1799	Grounds	Grounds - Broken	See text	2/4/2008	RUSSELL	
-	25/519, 29/1800	Grounds	Grounds - Broken	Grounds - Broken	2/21/2000		
-	25/519, 29/1800	Grounds	Grounds - Broken	Grounds - Broken	1/31/2001		
-	25/519, 29/1800	Structure	Leg Numbers 1,2,3,or4	F, A	6/3/2010	MASTEC	
-	25/519, 29/1800	Structure - Base Shoe	Base Shoe - Corroded Thin / Necking	Base Shoe - Corroded Thin / Necking	6/3/2010	MASTEC	
-	25/519, 29/1801	Miscellaneous	Need Anti Climb Sign	Need Anti Climb Sign	2/21/2000		
-	25/519, 29/1801	Structure - Steel	Steel - Excess Packout	Halfway up tower	6/3/2010	MASTEC	
-	25/519, 29/1801	Structure	Base Shoe - Corroded Thin / Necking	Completed 10.16.15 per K. Geis	6/3/2010	MASTEC	
-	25/519, 29/1801	Structure	Leg Numbers 1,2,3,or4	F	6/3/2010	MASTEC	
-	25/519, 29/1802	Miscellaneous	Need Anti Climb Sign	Need Anti Climb Sign	2/21/2000		
-	25/519, 29/1802	Structure - Base Shoe	Base Shoe - Corroded Thin / Necking	Base Shoe - Corroded Thin / Necking	6/3/2010	MASTEC	
-	25/519, 29/1802	Structure - Steel	Steel - Missing/Faded Bolts	Steel - Missing/Faded Bolts	6/3/2010	MASTEC	
-	25/519, 29/1802	Structure	Leg Numbers 1,2,3,or4	M	6/3/2010	MASTEC	
-	25/519, 29/1802	Grounds	Grounds - Broken	Grounds - Broken	6/3/2010	MASTEC	
-	25/519, 29/1803	Miscellaneous	Need Anti Climb Sign	Need Anti Climb Sign	2/21/2000		
-	25/519, 29/1803	Structure - Base Shoe	Base Shoe - Corroded Thin / Necking	Base Shoe - Corroded Thin / Necking	6/3/2010	MASTEC	
-	25/519, 29/1803	Braces - Knee Brace	Knee Brace Bolt Failure	Knee Brace Bolt Failure	6/3/2010	MASTEC	
-	25/519, 29/1803	Braces - Knee Brace	Defective Knee Brace	Bent Brace on bottom	6/3/2010	MASTEC	
-	25/519, 29/1804	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	Base Shoe -Needs Anti-Corrosive Treatmnt	1/31/2007	RUSSELL	
-	25/519, 29/1804	Work found during a routine PM	Work as a result of a PM Order	66667448	1/31/2007	RUSSELL	
-	25/519, 29/1804	Equipment Needed for Repair	ATV	Rt 611 - Rd Xing	2/5/2007	RUSSELL	
-	25/519, 29/1804	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	A120	2/5/2007	RUSSELL	
-	25/519, 29/1804	Work found during a routine PM	Work as a result of a PM Order	66667448	2/5/2007	RUSSELL	
-	25/519, 29/1804	Equipment Needed for Repair	ATV	Rt 611 - Rd Xing	2/5/2007	RUSSELL	
-	25/519, 29/1804	Grounds	Grounds - Broken	Grounds - Broken	2/5/2007	RUSSELL	
-	25/519, 29/1805	Work found during a routine PM	Work as a result of a PM Order	66667448	2/5/2007	RUSSELL	
-	25/519, 29/1805	Equipment Needed for Repair	ATV	Rt 611	2/5/2007	RUSSELL	
-	25/519, 29/1805	Structure - Numbers	Numbers - Faded	Install new #s on both sides - see TEXT	2/5/2007	RUSSELL	
-	25/519, 29/1805	Structure	Ground Wire-M-Missing,CtCut	Broken	2/8/2023	JARE029	
-	25/519, 29/1807	Structure - Numbers	Aerial Number Faded	Aerial Number Faded	6/30/2004		
-	25/519, 29/1808	Structure - Steel	Steel - Excess Packout	Steel - Excess Packout	5/7/2010	MASTEC	
-	25/519, 29/1808	Structure	Leg Numbers 1,2,3,or4	Completed 11.17.15 per K. Geis	5/7/2010	MASTEC	
-	25/519, 29/1808	Structure	Leg Numbers 1,2,3,or4	F	5/7/2010	MASTEC	
-	25/519, 29/1808	Static Wire	Static Wire Twisted	Static Wire Twisted	5/7/2010	MASTEC	
-	25/519, 29/1808	Insulator Conductor	Cotter Key-BO-Backed Out, M-M	M	5/7/2010	MASTEC	
-	25/519, 29/1808	Hardware	Hardware - Cotter Key Backed Out	Hardware - Cotter Key Backed Out	5/7/2010	MASTEC	
-	25/519, 29/1808	Hardware	Hardware - Cotter Key Missing	Hardware - Cotter Key Missing	5/7/2010	MASTEC	
-	25/519, 29/1809	Work found during a routine PM	Work as a result of a PM Order	66667448	2/5/2007	RUSSELL	
-	25/519, 29/1809	Equipment Needed for Repair	ATV	Rt 660	2/5/2007	RUSSELL	
-	25/519, 29/1809	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	A120	2/5/2007	RUSSELL	
-	25/519, 29/1809	Structure - Bolts on Shelf Gain	Bolts on Shelf Gain - Bent	Bolts on Shelf Gain - Bent	5/7/2010	MASTEC	
-	25/519, 29/1809	Grounds	Grounds - Broken	All legs	5/7/2010	TIM0032	
-	25/519, 29/1809	Structure	Ground Wire-M-Missing,CtCut	C	10/28/2020	TIM0032	
-	25/519, 29/1810	Grounds	Grounds - Broken	Grounds - Broken	2/21/2000		
-	25/519, 29/1810	Structure - Foundation	Foundation - Cot Vines / Underbrush	see Comments	1/31/2007		
-	25/519, 29/1810	Structure - Numbers	Numbers - Missing	Vines	7/28/2006	CBH	
-	25/519, 29/1810	Work found during a routine PM	Work as a result of a PM Order	66667448	2/5/2007	RUSSELL	
-	25/519, 29/1810	Work found during a routine PM	Work as a result of a PM Order	66667448	2/5/2007	RUSSELL	
-	25/519, 29/1810	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	66667448	2/5/2007	RUSSELL	
-	25/519, 29/1810	Work found during a routine PM	Work as a result of a PM Order	66667448	2/5/2007	RUSSELL	
-	25/519, 29/1810	Grounds	Grounds - Broken	Grounds - Broken	2/5/2007	RUSSELL	
-	25/519, 29/1810	Structure - Steel	Steel - Excess Packout	Steel - Excess Packout	5/7/2010	MASTEC	
-	25/519, 29/1810	Structure	Leg Numbers 1,2,3,or4	Completed 10.16.15 per K. Geis	5/7/2010	MASTEC	
-	25/519, 29/1811	Miscellaneous	Brace Other=	Brace Other=	5/7/2010	MASTEC	
-	25/519, 29/1811	Work found during a routine PM	Work as a result of a PM Order	66667448	2/5/2007	RUSSELL	
-	25/519, 29/1811	Equipment Needed for Repair	ATV	Rt 660 - Rd Xing	2/5/2007	RUSSELL	
-	25/519, 29/1811	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	A120	2/5/2007	RUSSELL	
-	25/519, 29/1811	Structure - Steel	Steel - Excess Packout	Steel - Excess Packout	5/7/2010	MASTEC	
-	25/519, 29/1811	Structure	Leg Numbers 1,2,3,or4	Completed 9.28.15 per K. Geis	5/7/2010	MASTEC	
-	25/519, 29/1811	Structure	Structure Other=	Piece of concrete	9/18/2018		
-	25/519, 29/1811	Structure	Member -C-Corroded S-Split,CtCut-Chipped	Structure-Member -C-Corroded S-Split,CtCut-C	10/28/2020	TIM0032	
-	25/519, 29/1812	Structure	Ground Wire-M-Missing,CtCut	C	10/28/2020	TIM0032	
-	25/519, 29/1812	Structure - Numbers	Aerial Number Faded	Aerial Number Faded	6/30/2004		
-	25/519, 29/1812	Work found during a routine PM	Work as a result of a PM Order	66667448	2/5/2007	RUSSELL	
-	25/519, 29/1812	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	"See Text"	2/5/2007	RUSSELL	
-	25/519, 29/1812	Equipment Needed for Repair	ATV	ATV	2/5/2007	RUSSELL	
-	25/519, 29/1812	Structure	Missing Alum-Location=	Missing Alum-Location=	12/11/2012		
-	25/519, 29/1814	Grounds	Grounds - Broken	Grounds - Broken	2/21/2000		
-	25/519, 29/1814	Grounds	Grounds - Broken	see Comments	1/30/2001		
-	25/519, 29/1814	Work found during a routine PM	Work as a result of a PM Order	66667448	2/5/2007	RUSSELL	
-	25/519, 29/1814	Equipment Needed for Repair	ATV	Access Rt. 1	2/5/2007	RUSSELL	
-	25/519, 29/1814	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	A120	2/5/2007	RUSSELL	
-	25/519, 29/1814	Work found during a routine PM	Work as a result of a PM Order	66667448	2/5/2007	RUSSELL	
-	25/519, 29/1814	Equipment Needed for Repair	ATV	Access Rt. 1	2/5/2007	RUSSELL	
-	25/519, 29/1814	Grounds	Grounds - Broken	2 broken	2/5/2007	RUSSELL	
-	25/519, 29/1814	Static Wire / Warning Spheres	Static Wire - Warning Spheres Defective	Has fallen on ground, REF IMG0452	1/20/2009	CBH	
-	25/519, 29/1814	Insulator Conductor	Pins -BO-Backed Out, D-Damaged	BO	2/28/2017		
-	25/519, 29/1814	Insulator Conductor	(H) Hot End / (C) Cold End	H	2/28/2017		
-	25/519, 29/1816	Structure	Ground Wire-M-Missing,CtCut	Broken	2/8/2023	JARE029	
-	25/519, 29/1816	Insulator Conductor	Cotter Key-BO-Backed Out, M-M	BO at yoke plate	8/1/2011	CBH	
-	25/519, 29/1817	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	Base Shoe -Needs Anti-Corrosive Treatmnt	2/21/2000		
-	25/519, 29/1817	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	Base Shoe -Needs Anti-Corrosive Treatmnt	1/30/2007		
-	25/519, 29/1817	Work found during a routine PM	Work as a result of a PM Order	66667448	2/5/2007	RUSSELL	
-	25/519, 29/1817	Equipment Needed for Repair	ATV	Access Russell Rd - QMB	2/5/2007	RUSSELL	
-	25/519, 29/1817	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	shovel off 1 footer & apply A120	2/5/2007	RUSSELL	
-	25/519, 29/1817	Structure	Bolt B-Broke NM-Not Met B-M-Bolt Miss	Missing	2/8/2023	JARE029	
-	25/519, 29/1817	Structure	Brace Other=	Steel needs both	2/8/2023	JARE029	
-	25/519, 29/1819	Conductor	Cotter Key-BO-Backed Out, M-M	Bo @ yoke plate	3/30/2017	JEREMY3	
-	25/519, 29/181						

-	252/5554, 29/1821	Structure - Wood or Concrete	Structure - Major Woodpecker Hole / Hole		1/29/2001	RACHE06	
-	252/5554, 29/1821	Conductor	Wire Position L,M,R,T,B	M, outside shoe	3/30/2017	JEREMY3	
-	252/5554, 29/1821	Conductor	Cotter Key-BO=Backed Out, M=Mi	BO	3/30/2017	JEREMY3	
-	252/5554, 29/1821	Conductor	Cotter Key-BO=Backed Out, M=Mi	Bo @ yoke plate	3/30/2017	JEREMY3	
-	252/5554, 29/1821	Conductor	Wire Position L,M,R,T,B	B	3/30/2017	JEREMY3	
-	252/5555, 29/1822	Work found during a routine PM	Work as a result of a PM Order	66667749	2/5/2007	RUSSEL8	
-	252/5555, 29/1822	Equipment Needed for Repair	ATV	Quantic Cemetery	2/5/2007	RUSSEL8	
-	252/5555, 29/1822	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	A120	2/5/2007	RUSSEL8	
-	252/5556	Guys	Guys - Damaged Fiber Glass Breaker		4/15/1999		
-	252/5556	Work found during a routine PM	Work as a result of a PM Order	66667749	2/5/2007	RUSSEL8	
-	252/5556	Guys	Guys - Damaged Fiber Glass Breaker		2/5/2007	RUSSEL8	
-	252/5556	Guys	Guys - Needs Guard	see TEXT	2/5/2007	RUSSEL8	
-	252/5556	Guys	Guy Buried		2/5/2007	RUSSEL8	
-	252/5556	Pole Position	2nd Pole From Left	dig out 1 middle pole	2/5/2007	RUSSEL8	
-	252/5556	Guys	Guys - Other	key backed out	11/17/2020	MEL055	
-	252/5558, 29/1825	Structure - Steel	Steel - Missing/Failed Bolt(s)		2/22/2000		
-	252/5558, 29/1825	Structure - Steel	Steel - Missing/Failed Bolt(s)	see Comments	1/29/2001		
-	252/5558, 29/1825	Insulator Conductor	Cotter Key-BO=Backed Out, M=Mi	Non standard installation	2/28/2017		
-	252/5558, 29/1825	Insulator Conductor	(H) Hot End / (C) Cold End	H	2/28/2017		
-	252/5559, 29/1826	Insulators - Static Insulators	Static Insulators - Broken		2/22/2000		
-	252/5559, 29/1826	Insulators - Static Insulators	Static Insulators - Broken	see Comments	1/29/2001		
-	252/5560, 29/1827	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	A120 - Rt. 1	2/5/2007	RUSSEL8	
-	252/5560, 29/1827	Work found during a routine PM	Work as a result of a PM Order	66667749	2/5/2007	RUSSEL8	
-	252/5561, 29/1828	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt		2/22/2000		
-	252/5561, 29/1828	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	see Comments	1/29/2001		
-	252/5561, 29/1828	Structure - Foundation	Foundation - Cut Vines / Underbrush	Vines	7/26/2006	CBH	
-	252/5561, 29/1828	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	A120 - Rt. 1	2/5/2007	RUSSEL8	
-	252/5561, 29/1828	Work found during a routine PM	Work as a result of a PM Order	66667749	2/5/2007	RUSSEL8	
-	252/5562, 29/1829	Grounds	Grounds - Broken	see Comments	8/26/2004		
-	252/5562, 29/1829	Grounds	Grounds - Broken		2/22/2000		
-	252/5562, 29/1829	Grounds	Grounds - Broken		1/29/2001		
-	252/5562, 29/1829	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	A120, Dig out 1 footer (QMB school)	2/5/2007	RUSSEL8	
-	252/5562, 29/1829	Work found during a routine PM	Work as a result of a PM Order	66667749	2/5/2007	RUSSEL8	
-	252/5562, 29/1829	Insulator Static	Broken- L=Leave, R=Replace		2/28/2017		
-	252/5563, 29/1830	Grounds	Grounds - Broken	see Comments	8/26/2004		
-	252/5563, 29/1830	Grounds	Grounds - Broken		2/22/2000		
-	252/5563, 29/1830	Grounds	Grounds - Broken		1/29/2001		
-	252/5563, 29/1830	Static Wire / Warning Spheres	Static Wire - Other	Static line cradle out of plum	1/30/2009	CBH	
-	252/5563, 29/1830	Structure	Corrosion-Severe-Location=	BO	2/8/2011	RICKEY8	
-	252/5563, 29/1830	Structure	Cotter Key Location=	put ground rods for structure	7/16/2014		
-	252/5564, 29/1831	Grounds	Grounds - Broken	see Comments	8/26/2004		
-	252/5564, 29/1831	Grounds	Grounds - Broken		1/29/2001		
-	252/5564, 29/1831	Grounds	Grounds - Broken		2/22/2000		
-	252/5564, 29/1831	Structure - Steel	Missing Steel		2/22/2000	RACHE06	
-	252/5564, 29/1831	Structure	Cotter Key Location=	put ground rods for structure	7/16/2014		
-	252/5565, 29/1832	Structure	Cotter Key Location=	put ground rods for structure	7/16/2014		
-	252/5566, 29/1833	Structure	Cotter Key Location=	put ground rods for structure	7/16/2014		
-	252/5566A	Insulator Static	Cotter Key-BO=Backed Out, M=Mi	BO	4/10/2017	CHR1376	
-	252/5567, 29/1834	Structure	Cotter Key Location=	put ground rods for structure	7/16/2014		
-	252/5568, 29/1, 29/1835	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	Need A120 - Q.M.B.	2/5/2007	RUSSEL8	
-	252/5568, 29/1, 29/1835	Work found during a routine PM	Work as a result of a PM Order	66667749	2/5/2007	RUSSEL8	
-	252/5568, 29/1, 29/1835	Structure	Cotter Key Location=	put ground rods for structure	7/16/2014		
-	252/5568, 29/1, 29/1835	Conductor	Conductor Other =	Install fault indicator	7/18/2019		
-	252/5570, 29/1837	Work found during a routine PM	Work as a result of a PM Order	66667449	2/7/2007	RUSSEL8	
-	252/5570, 29/1837	Grounds	Grounds - Broken	Repair 2 broken grds. Fuller Heights Rd.	2/7/2007	RUSSEL8	
-	252/5570, 29/1837	Insulator Conductor	Cotter Key-BO=Backed Out, M=Mi		8/11/2011		
-	252/5570, 29/1837	Insulator Conductor	Wire Position L,M,R,T,B	Top left yoke plate	8/11/2011		
-	252/5571, 29/1838	Insulator Conductor	Cotter Key-BO=Backed Out, M=Mi	BO	2/8/2011	RICKEY8	
-	252/5571, 29/1838	Insulator Conductor	Wire Position L,M,R,T,B	M- at shoe on yoke	2/8/2011	RICKEY8	
-	252/5572, 29/1839			See text	12/22/2008	CBH	
-	252/5572, 29/1839	Environmental Concerns	Environmental - Osprey Nest	Birds nest on structure	12/22/2008	CBH	
-	252/5572, 29/1839	Insulator Conductor	Wire Position L,M,R,T,B	T	10/20/2020	TIM0032	
-	252/5572, 29/1839	Insulator Conductor	Cotter Key-BO=Backed Out, M=Mi	BO at 1st. Bell and "Y" socket	10/20/2020	TIM0032	
-	252/5572, 29/1839	Insulator Conductor	(H) Hot End / (C) Cold End	H	10/20/2020	TIM0032	
-	252/5573, 29/1840				9/12/1994		
-	252/5573, 29/1840	Grounds	Grounds - Broken		2/23/2000		
-	252/5573, 29/1840	Grounds	Grounds - Broken	see Comments	1/29/2001		
-	252/5573, 29/1840	Miscellaneous	Need Anti Climb Sign		1/29/2001	RACHE06	
-	252/5573, 29/1840				7/26/2006	CBH	
-	252/5573, 29/1840	Phase Position	Right		7/26/2006	CBH	
-	252/5573, 29/1840	Phase Position	Top and Bottom		7/26/2006	CBH	
-	252/5573, 29/1840	Phase Position	Middle	1 Broken Bell	2/7/2007	RUSSEL8	
-	252/5573, 29/1840	Phase Position	Top	2 Broken Bells	2/7/2007	RUSSEL8	
-	252/5573, 29/1840	Phase Position	Bottom	1Broken Bell	2/7/2007	RUSSEL8	
-	252/5573, 29/1840	Work found during a routine PM	Work as a result of a PM Order	66667449	2/7/2007	RUSSEL8	
-	252/5573, 29/1840			"See Text"	2/7/2007	RUSSEL8	
-	252/5573, 29/1840	Insulator Conductor	Broken- L=Leave, R=Replace		8/11/2011		
-	252/5573, 29/1840	Insulator Conductor	Wire Position L,M,R,T,B	1, 2 3&4 from cold end	8/11/2011		
-	252/5573, 29/1840	Insulator Conductor	Wire Position L,M,R,T,B	T #5, M #7, B #4	4/10/2017	TIM0032	
-	252/5573, 29/1840	Insulator Conductor	(H) Hot End / (C) Cold End	C, #, #7	4/10/2017	TIM0032	
-	252/5573, 29/1840	Insulator Conductor	Broken- L=Leave, R=Replace	Replace #5, #7, #4	4/10/2017	TIM0032	
-	252/5573, 29/1840	Insulator Conductor	(H) Hot End / (C) Cold End	H, #4	4/10/2017	TIM0032	
-	252/5573, 29/1840	Structure	Structure Other=	Needs climbed	2/7/2023	JARE029	
-	252/5574, 29/1841	Structure - Numbers	Numbers - Missing	see Comments	8/26/2004		
-	252/5574, 29/1841	Structure - Numbers	Numbers - Missing		1/29/2001		
-	252/5574, 29/1841	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt		1/29/2001	RACHE06	
-	252/5574, 29/1841	Grounds	Grounds - Broken		2/23/2000	RACHE06	
-	252/5575, 29/1842	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt		2/23/2000		
-	252/5575, 29/1842	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	see Comments	1/29/2001		
-	252/5575, 29/1842			See text	12/22/2008	CBH	
-	252/5576, 29/1843	Structure	Ground Wire-M=Missing,C=Cut	Structure-Ground Wire-M=Missing,C=Cut	2/7/2023	BRAND58	
-	252/5577, 29/1844	Work found during a routine PM	Work as a result of a PM Order	66667449	2/7/2007	RUSSEL8	
-	252/5577, 29/1844	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	Need A120, Access Cabin Rd.	2/7/2007	RUSSEL8	
-	252/5578, 29/1845	Work found during a routine PM	Work as a result of a PM Order	66667449	2/7/2007	RUSSEL8	
-	252/5578, 29/1845	Structure - Steel	Steel - Missing/Failed Bolt(s)	"See Text"	2/7/2007	RUSSEL8	
-	252/5578, 29/1845	Equipment Needed for Repair	Boat		2/7/2007	RUSSEL8	
-	252/5578, 29/1845	Foundation	Foundation Other=	additional inspection	8/24/2016		
-	252/5578, 29/1845	Foundation	Foundation Other=	rehab	12/20/2016		
-	252/5579, 29/1846	Foundation	Foundation Other=	additional inspection	8/24/2016		
-	252/5579, 29/1846	Foundation	Foundation Other=	rehab	12/20/2016		
-	252/5580, 29/1847	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	apply A120	2/8/2007	RUSSEL8	
-	252/5580, 29/1847	Work found during a routine PM	Work as a result of a PM Order	66667449	2/8/2007	RUSSEL8	
-	252/5580, 29/1847	Work found during a routine PM	Work as a result of a PM Order	66667449	2/8/2007	RUSSEL8	
-	252/5580, 29/1847	Structure - Foundation	Foundation - Cut Vines / Underbrush	"See Text"	2/8/2007	RUSSEL8	
-	252/5580, 29/1847	Conductor	Damaged	possible	7/1/2012		
-	252/5581, 29/1848	Conductor	Damaged	possible	7/1/2012		
-	252/5582, 29/1849	Structure - Base Shoe	Base Shoe - Corroded-Thin / Necking		2/8/2007	RUSSEL8	
-	252/5582, 29/1849	Work found during a routine PM	Work as a result of a PM Order	66667449	2/8/2007	RUSSEL8	
-	252/5582, 29/1849	Work found during a routine PM	Work as a result of a PM Order	66667449	2/8/2007	RUSSEL8	
-	252/5582, 29/1849	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	"See Text"	2/8/2007	RUSSEL8	
-	252/5582, 29/1849	Environmental Concerns	Environmental - Osprey Nest	Nest; See IMG 0460	1/30/2009	CBH	
-	252/5583, 29/1850	Environmental Concerns	Environmental - Osprey Nest		1/25/2001		
-	252/5583, 29/1850	Environmental Concerns	Environmental - Osprey Nest	Found 1/30/09; CBH Routine Patrol	1/25/2001		
-	252/5583, 29/1850	Miscellaneous	Miscellaneous - Other	See IMG 0459	1/25/2001		
-	252/5583, 29/1850	Environmental Concerns	Environmental - Osprey Nest	Found again 4/28/2009, by CBH	1/25/2001		
-	252/5583, 29/1850	Work found during a routine PM	Work as a result of a PM Order	66667449	2/8/2007	RUSSEL8	
-	252/5583, 29/1850	Structure - Base Shoe	Base Shoe -Needs Anti-Corrosive Treatmnt	apply A120	2/8/2007	RUSSEL8	
-	252/5583, 29/1850	Work found during a routine PM	Work as a result of a PM Order	66667449	2/8/2007	RUSSEL8	
-	252/5583, 29/1850	Grounds	Grounds - Broken	Repair 1 ground Possum Pt. Rd	2/8/2007	RUSSEL8	
-	252/5584	Steel Pole	Ground Wire-M=Missing,C=Cut	Steel Pole-Ground Wire-M=Missing,C=Cut	2/7/2023	BRAND58	
-	252/5585	Wood Pole	Ground Wire-M=Missing,C=Cut	Both grounds broken	3/24/2017	BRAND58	
-	252/5585	Wood Pole	Ground Wire-M=Missing,C=Cut	Both grounds cut	6/30/2020	JARE029	
-	10120245	29/1823	Structure - Numbers	Numbers - Missing	2/22/2000		
-	10120246	29/1823	Structure - Numbers	Numbers - Missing	1/29/2001		
-	10293013	29/1823	Hardware	Hardware - Other	Top of pole not grounded - no pole grd.	2/5/2007	RUSSEL8
-	10293013	29/1823	Work found during a routine PM	Work as a result of a PM Order	66667749	2/5/2007	RUSSEL8
-	10293013	29/1823	Equipment Needed for Repair	ATV	Quantic Cemetery	2/5/2007	RUSSEL8

**I. NECESSITY FOR THE PROPOSED PROJECT**

**M. In addition to the other information required by these guidelines, applications for approval to construct facilities and transmission lines interconnecting a Non-Utility Generator (“NUG”) and a utility shall include the following information:**

- 1. The full name of the NUG as it appears in its contract with the utility and the dates of initial contract and any amendments;**
- 2. A description of the arrangements for financing the facilities, including information on the allocation of costs between the utility and the NUG;**
- 3. a. For Qualifying Facilities (“QFs”) certificated by Federal Energy Regulatory Commission (“FERC”) order, provide the QF or docket number, the dates of all certification or recertification orders, and the citation to FERC Reports, if available;**  
**b. For self-certificated QFs, provide a copy of the notice filed with FERC;**
- 4. Provide the project number and project name used by FERC in licensing hydroelectric projects; also provide the dates of all orders and citations to FERC Reports, if available; and**
- 5. If the name provided in 1 above differs from the name provided in 3 above, give a full explanation.**

Response: Not applicable.



**I. NECESSITY FOR THE PROPOSED PROJECT**

- N. Describe the proposed and existing generating sources, distribution circuits or load centers planned to be served by all new substations, switching stations and other ground facilities associated with the proposed project.**

Response: Not applicable.

## **II. DESCRIPTION OF THE PROPOSED PROJECT**

### **A. Right-of-way (“ROW”)**

#### **1. Provide the length of the proposed corridor and viable alternatives.**

Response: The total length of the existing Rebuild Project transmission corridor is approximately 12.4 miles between Aquia Harbour Station and Possum Point Station; and approximately 0.7 miles between Fredericksburg Substation and Hospital Junction.

No alternative routes are proposed for the Rebuild Project. See Section II.A.9 of the Appendix for an explanation of the Company’s route selection process.

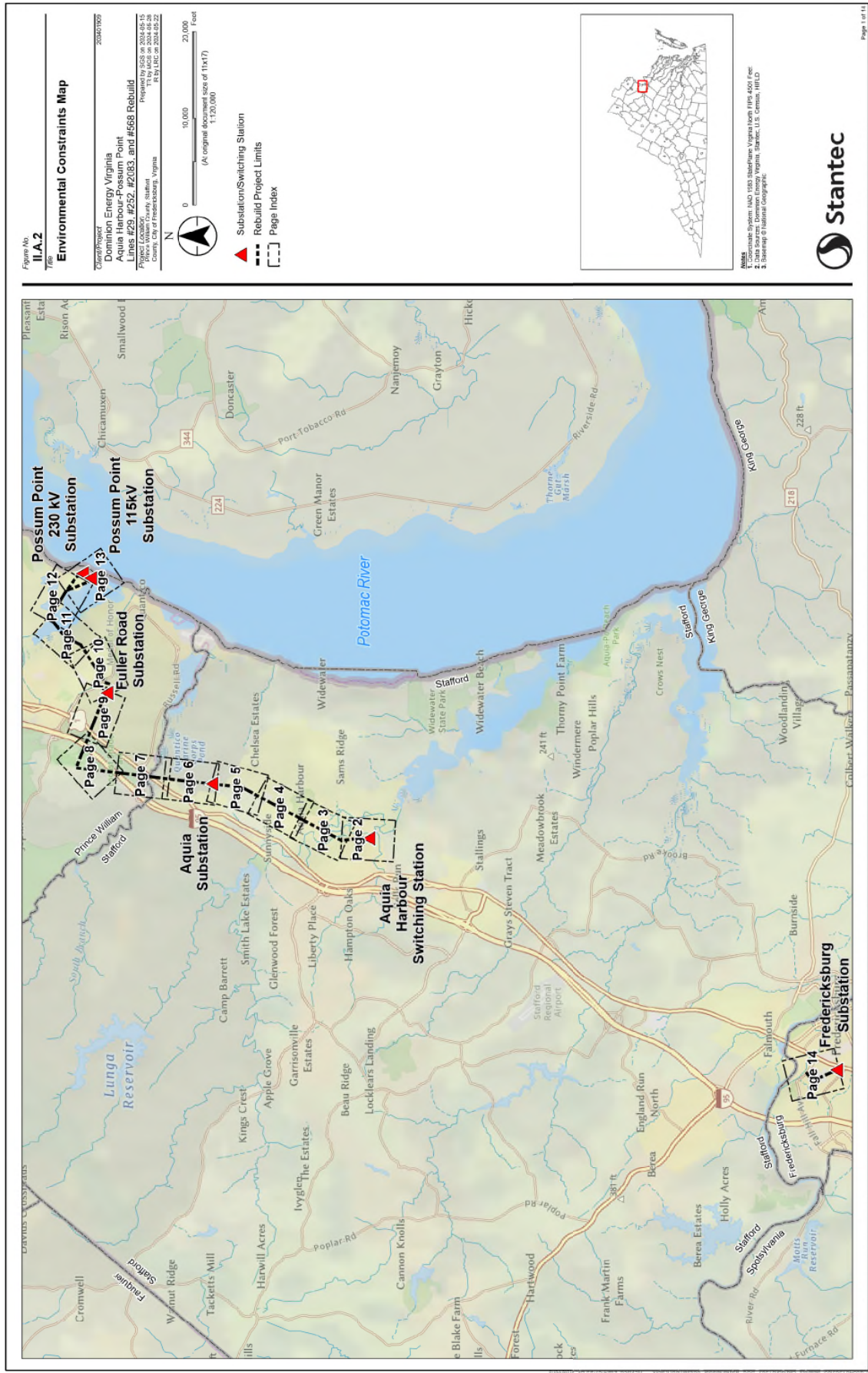
## **II. DESCRIPTION OF THE PROPOSED PROJECT**

### **A. Right-of-way (“ROW”)**

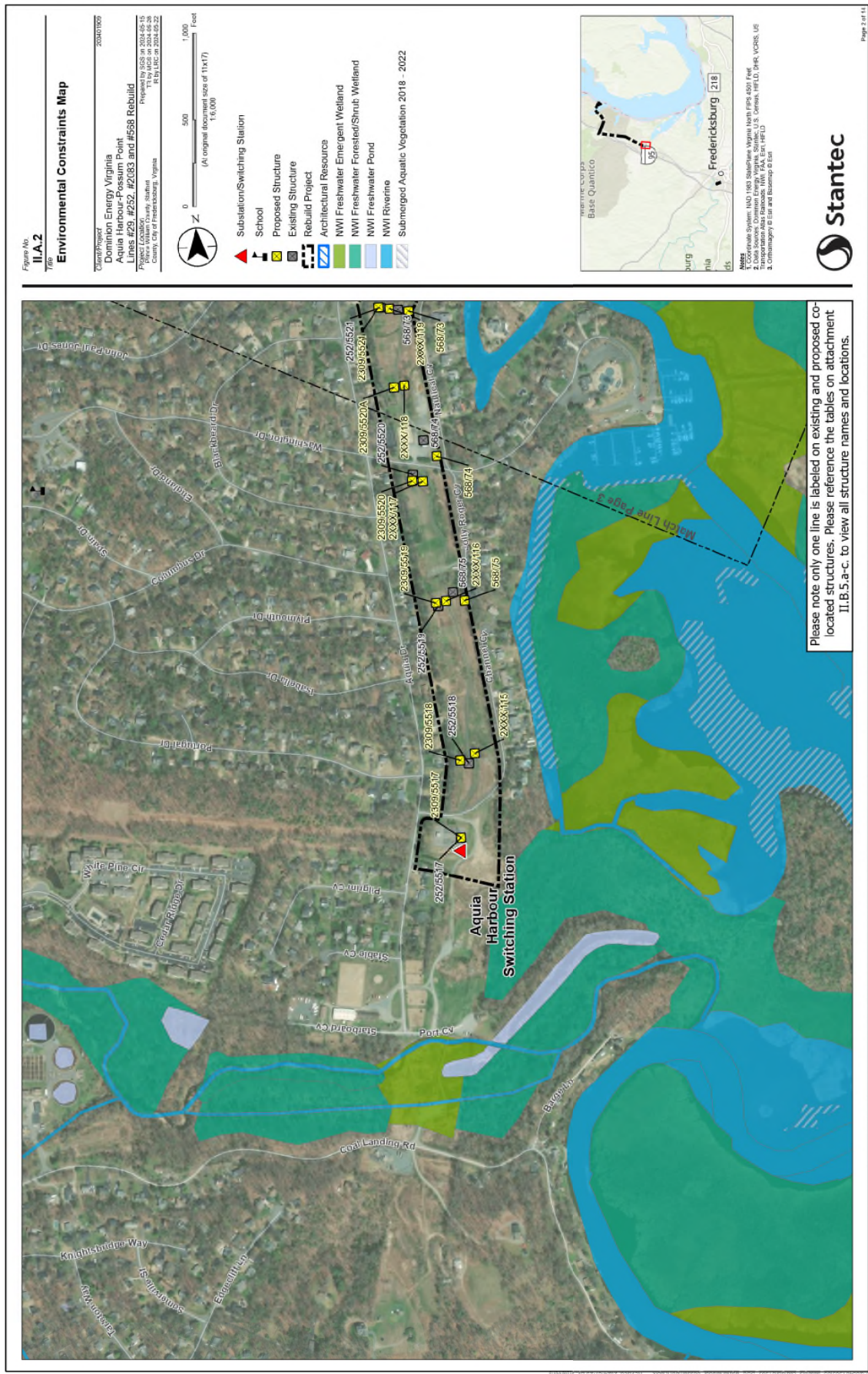
- 2. Provide color maps of suitable scale (including both general location mapping and more detailed GIS-based constraints mapping) showing the route of the proposed line and its relation to: the facilities of other public utilities that could influence the route selection, highways, streets, parks and recreational areas, scenic and historic areas, open space and conservation easements, schools, convalescent centers, churches, hospitals, burial grounds/cemeteries, airports and other notable structures close to the proposed project. Indicate the existing linear utility facilities that the line is proposed to parallel, such as electric transmission lines, natural gas transmission lines, pipelines, highways, and railroads. Indicate any existing transmission ROW sections that are to be quitclaimed or otherwise relinquished. Additionally, identify the manner in which the Applicant will make available to interested persons, including state and local governmental entities, the digital GIS shape file for the route of the proposed line.**

Response: See Attachment II.A.2, which includes existing linear utilities paralleled by the existing transmission line corridor. The Rebuild Project is entirely located within existing transmission line right-of-way or on Company-owned property with the exception of the 0.2 mile of additional 50 foot right-of-way required between existing Structure #252/5568 (#29/1835) and Fuller Road Substation; and the 0.1 mile of additional 67 foot right-of-way west of Fuller Road Substation.

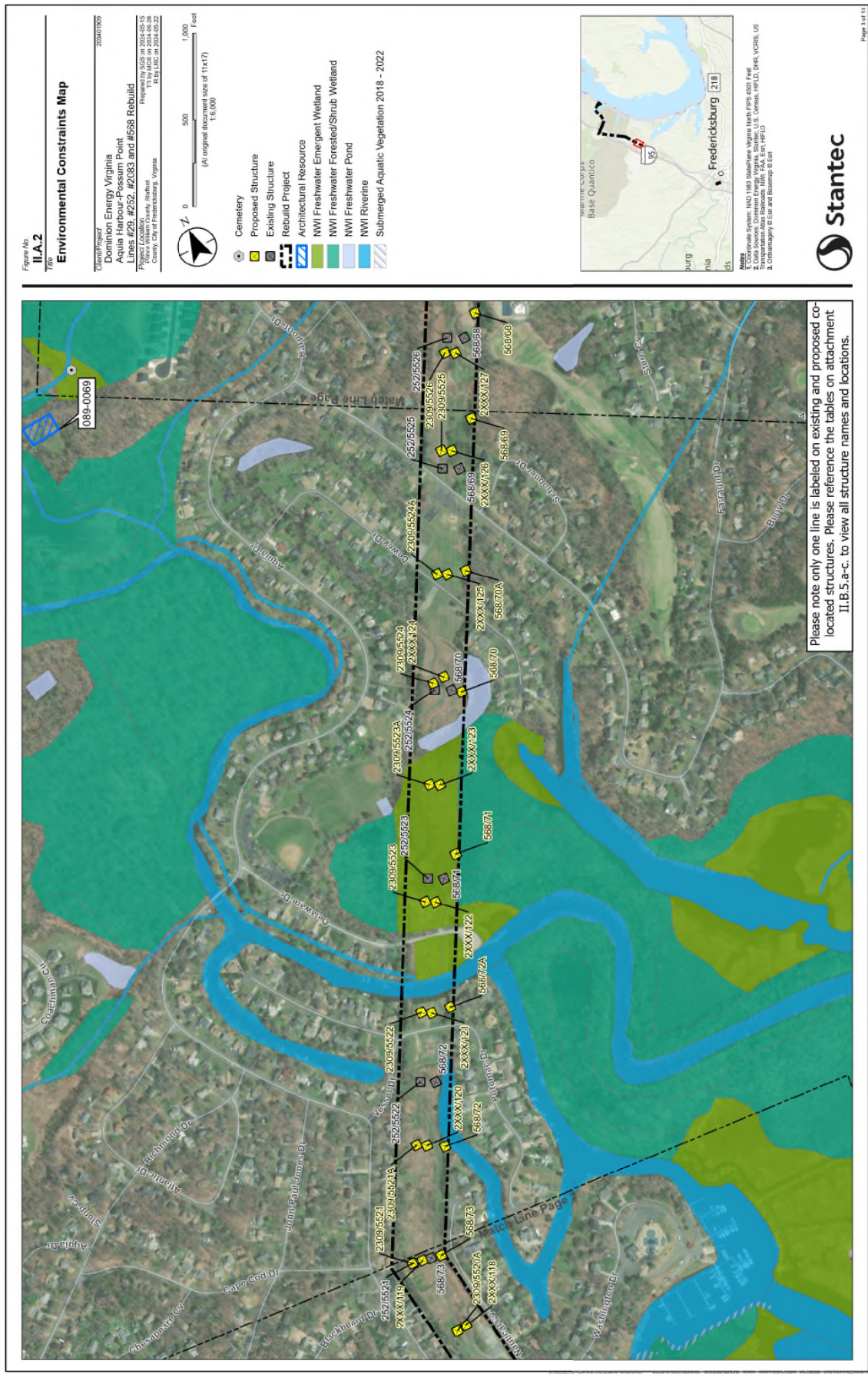
The Company will make the digital Geographic Information Systems (“GIS”) shape file available to interested persons upon request to counsel for the Company.



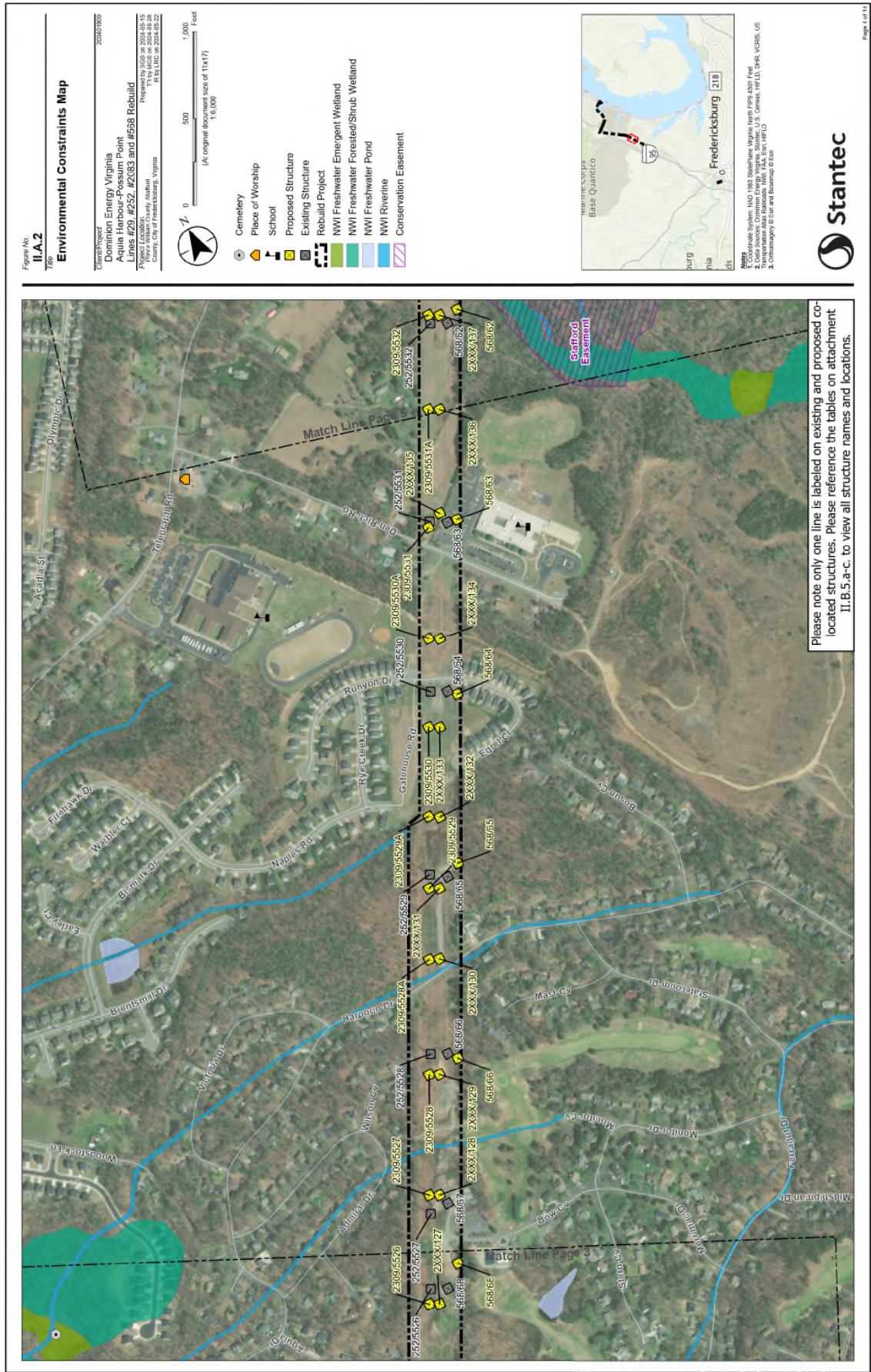




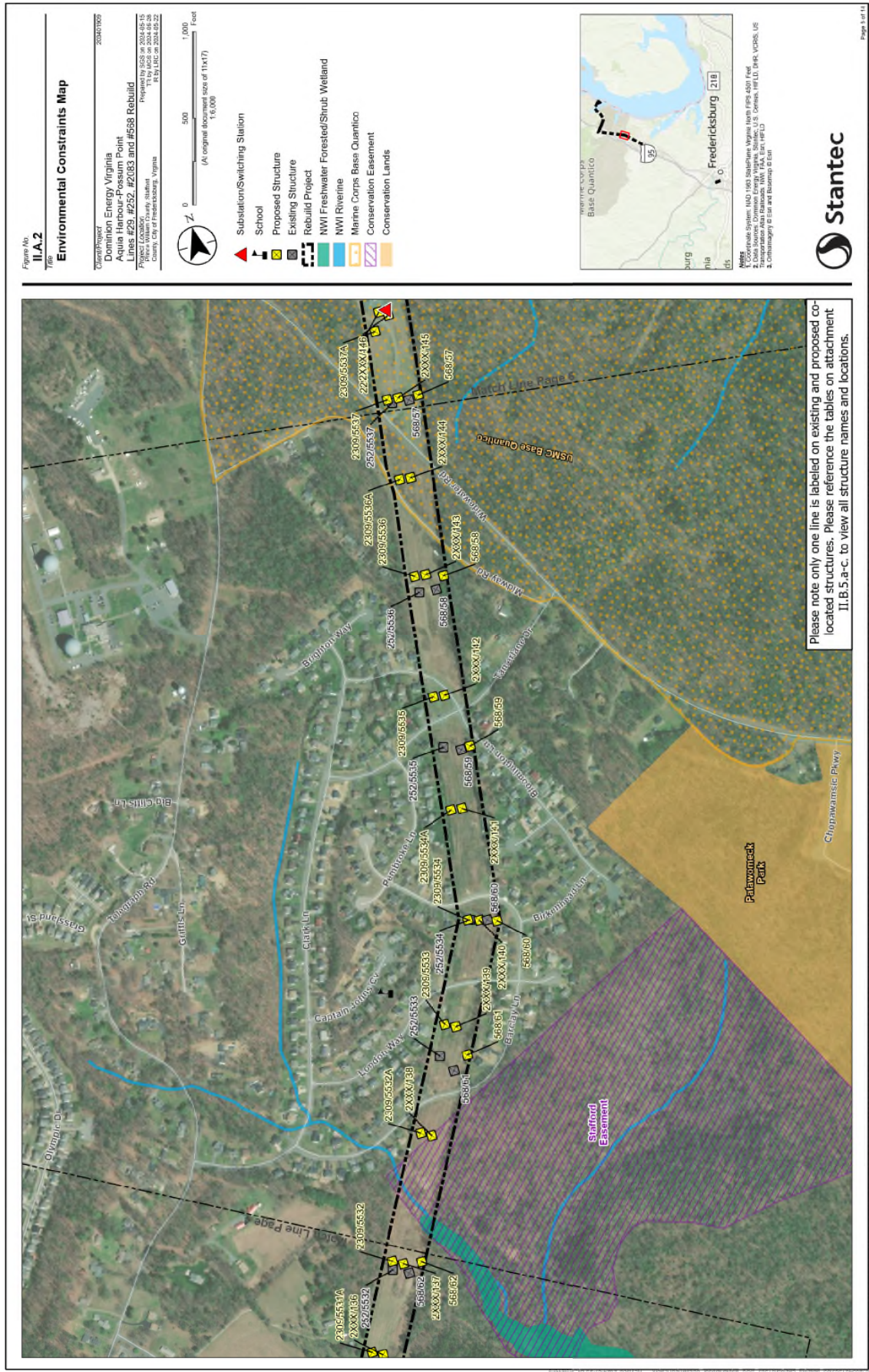








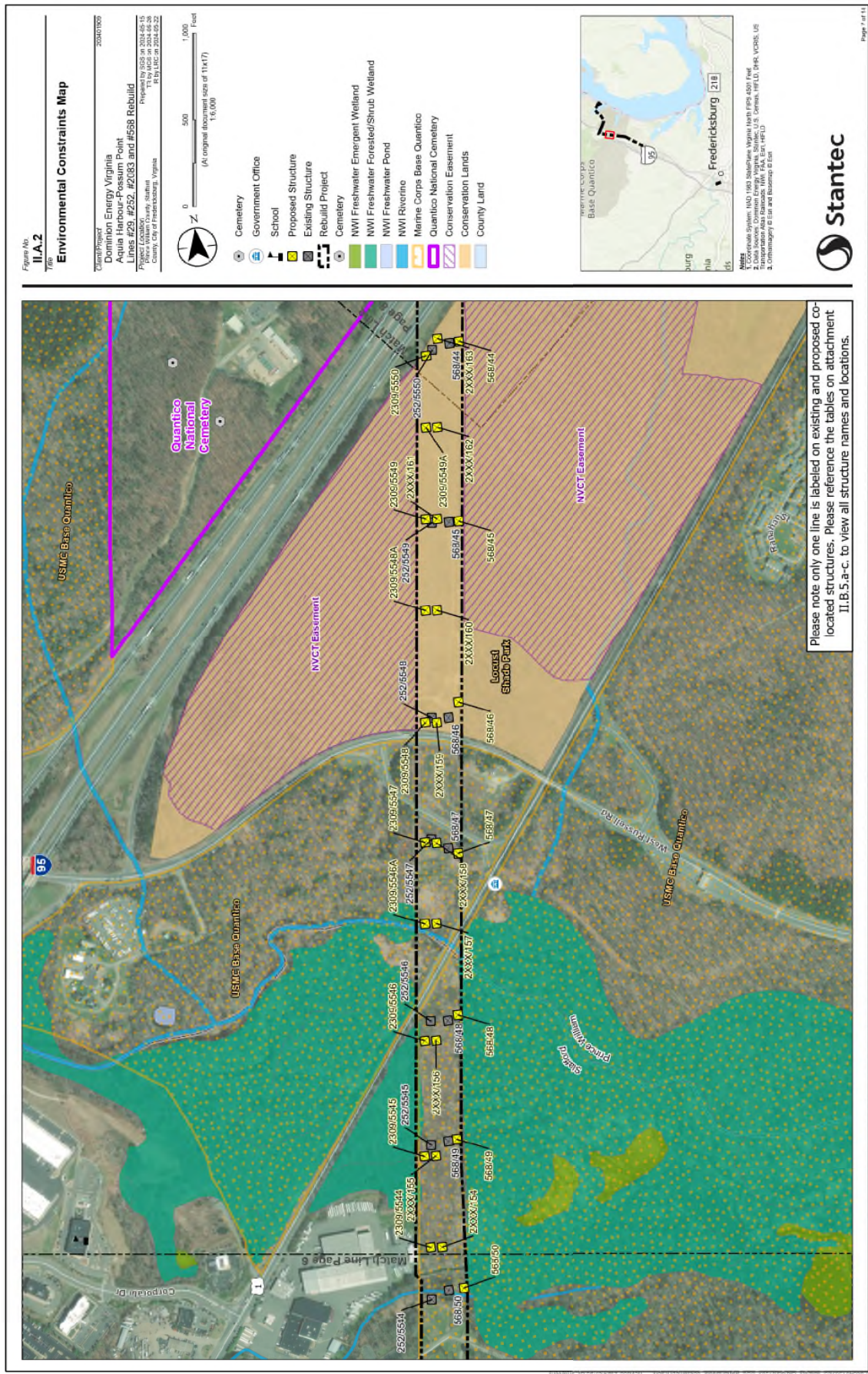




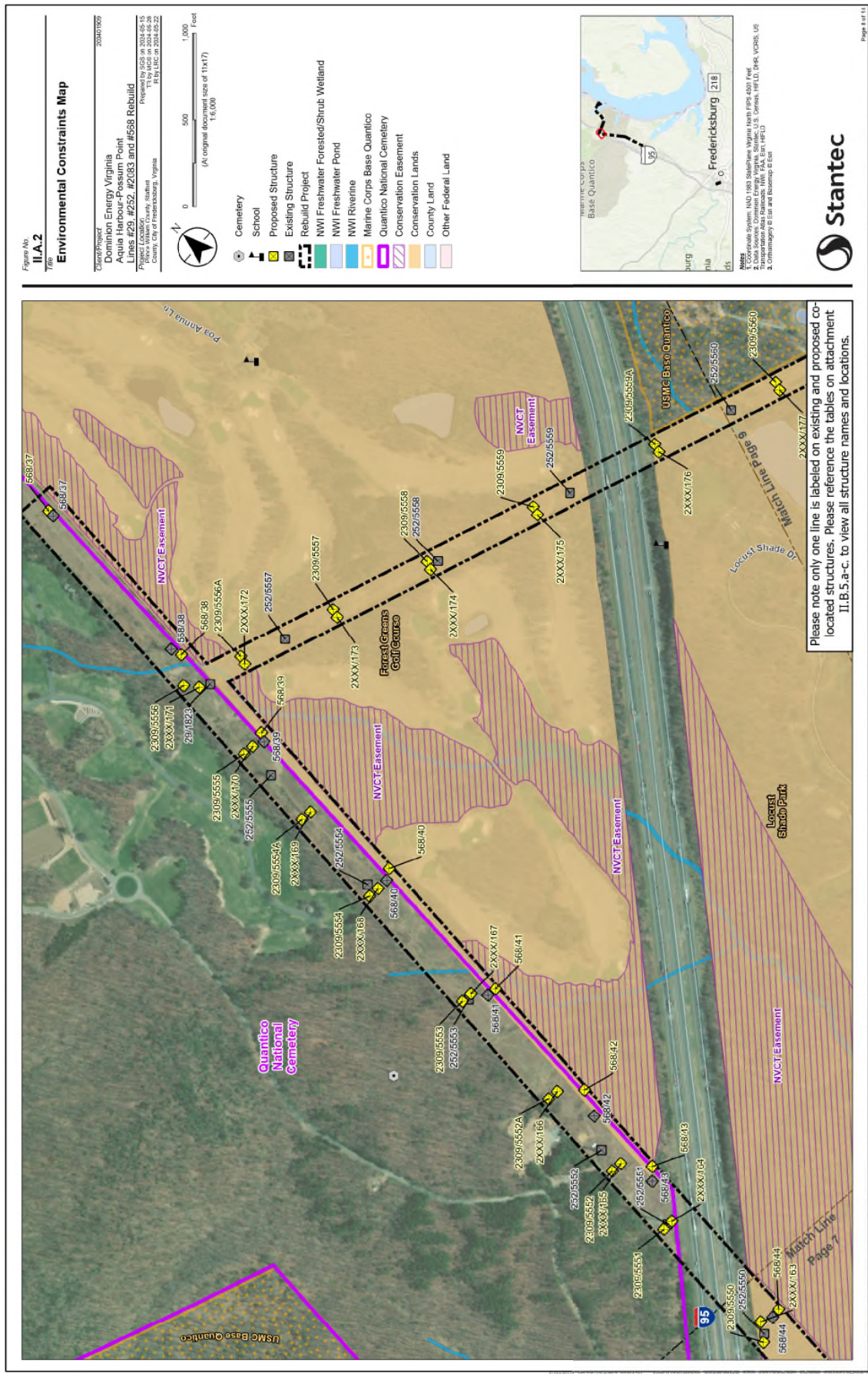




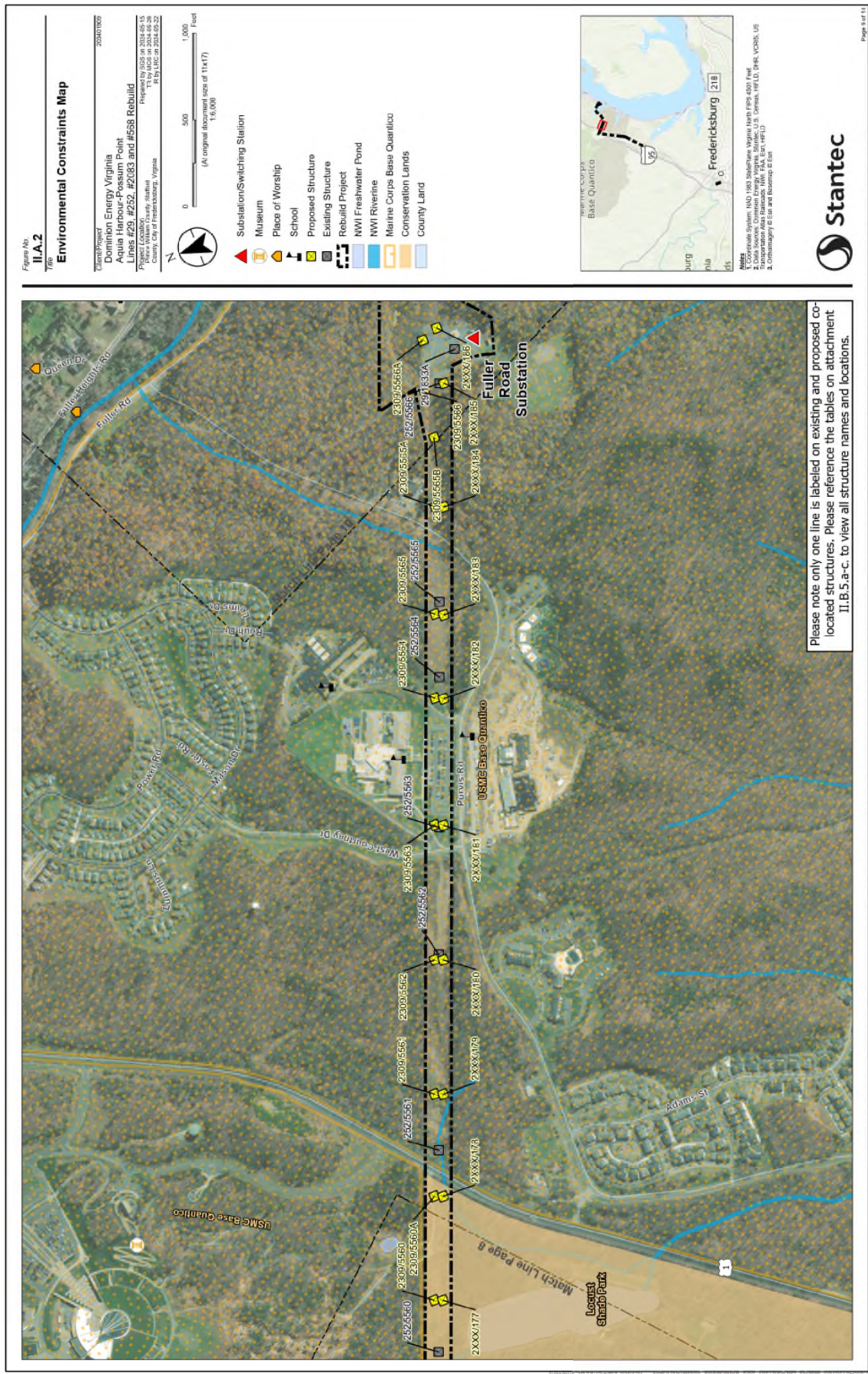




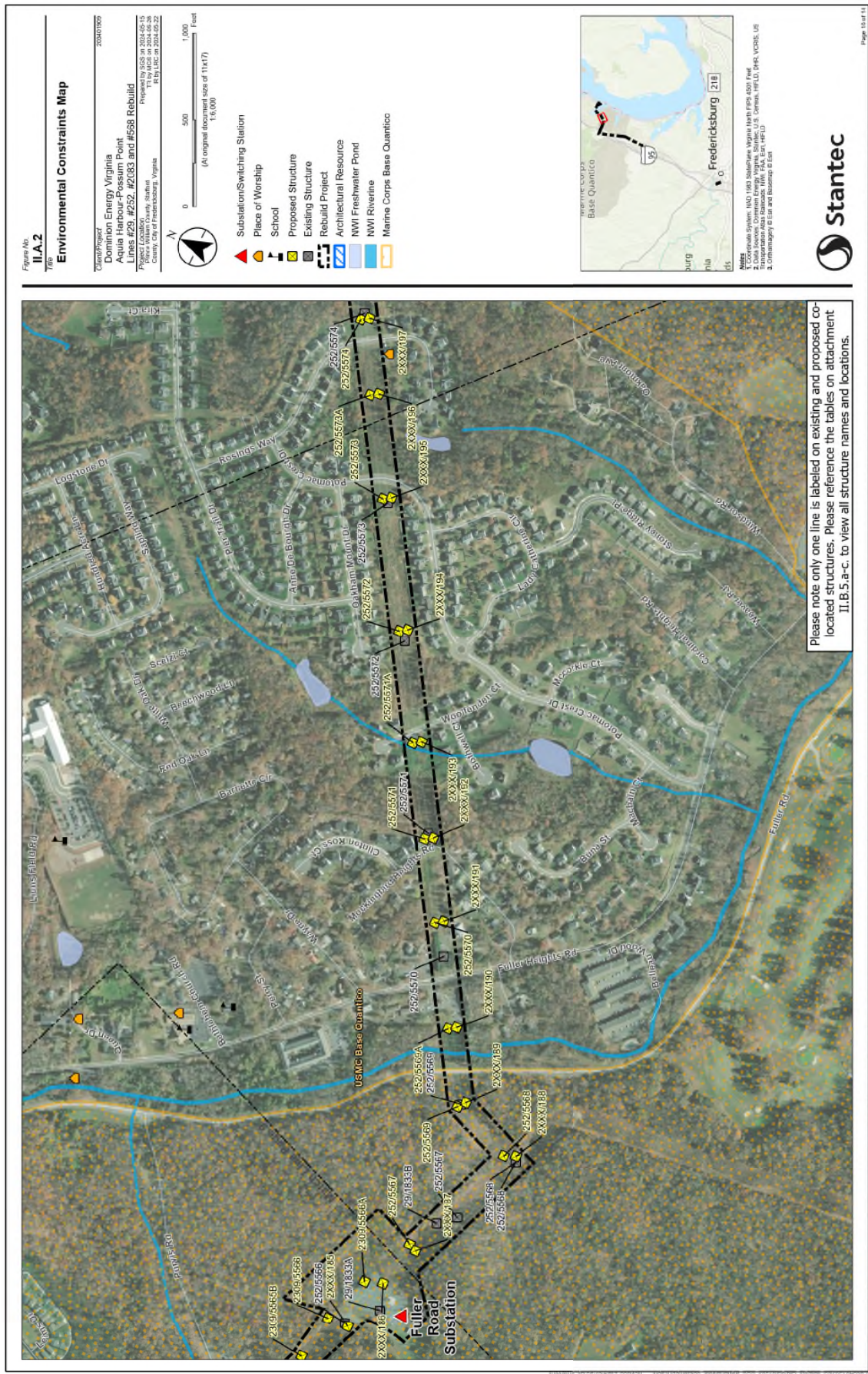












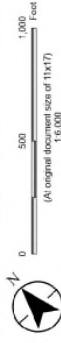


## Environmental Constraints Map

Client/Project  
 Dominion Energy Virginia  
 Aquia Harbour-Possum Point  
 Lines #29, #252, #2083 and #568 Rebuild  
 Project Location  
 Prince William County, Stafford  
 County, City of Fredericksburg, Virginia

Prepared by SGS on 2024-05-15  
 T1 by MCS on 2024-05-28  
 R1 by LRC on 2024-05-22

202401909



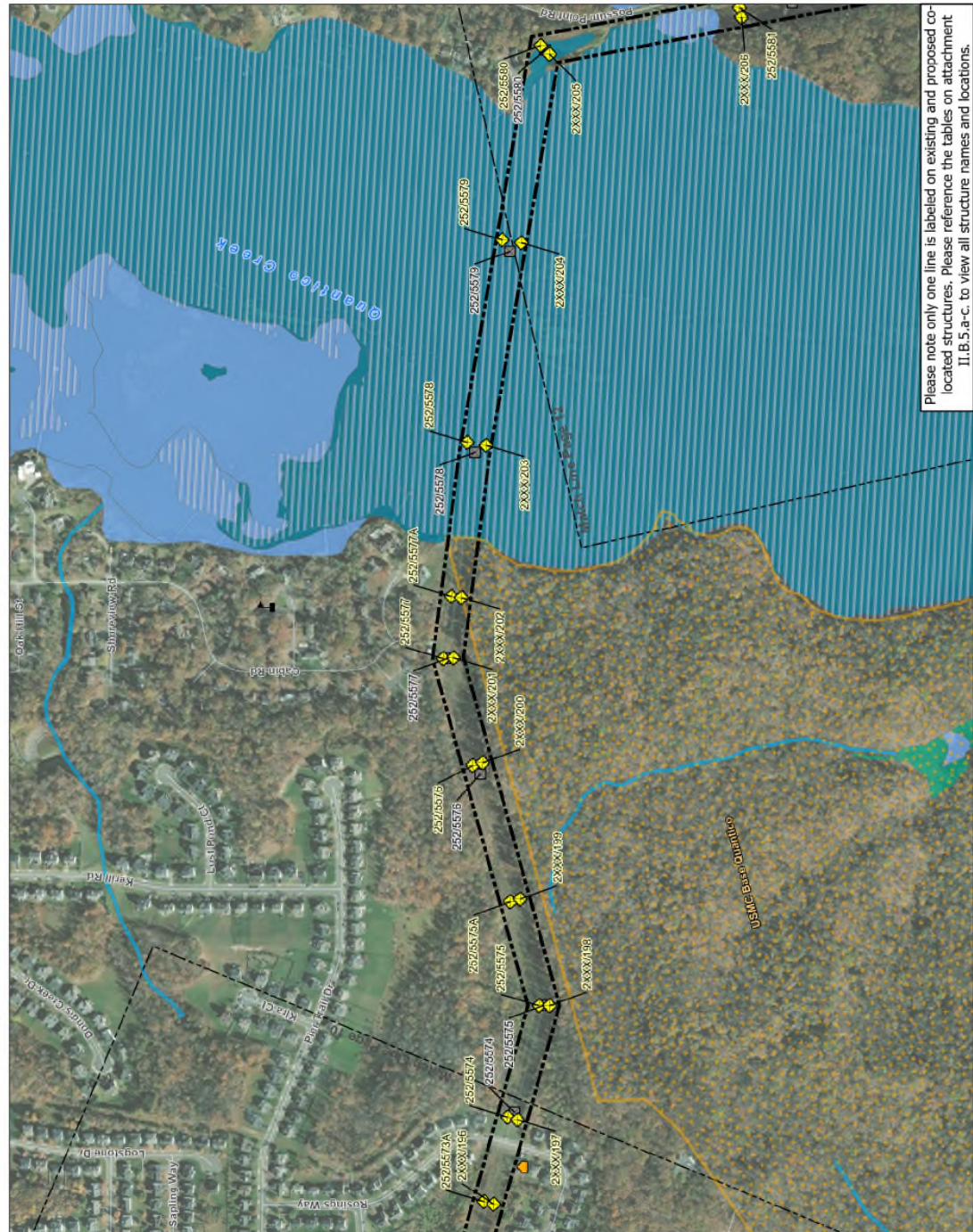
- Place of Worship  
School  
Proposed Structure  
Existing Structure  
Rebuild Project  
Architectural Resource  
NWI Estuarine and Marine Deepwater  
NWI Estuarine and Marine Wetland  
NWI Freshwater Forested/Shrub Wetland  
NWI Riverine  
Marine Corps Base Quantico  
Submerged Aquatic Vegetation 2018 - 2022



**Notes**  
1. Coordinate System: NAD 1983 StatePlane Virginia North FIPS 4501 Feet  
2. Data Sources: Dominion Energy Virginia, Slanlec, U.S. Census, HIFLD, DMR, VICRIS, US Transportation Atlas Railroads: NNI, FAA, ERI, HIFLD  
3. Orthorectification © Esri and BaseMap © Esri

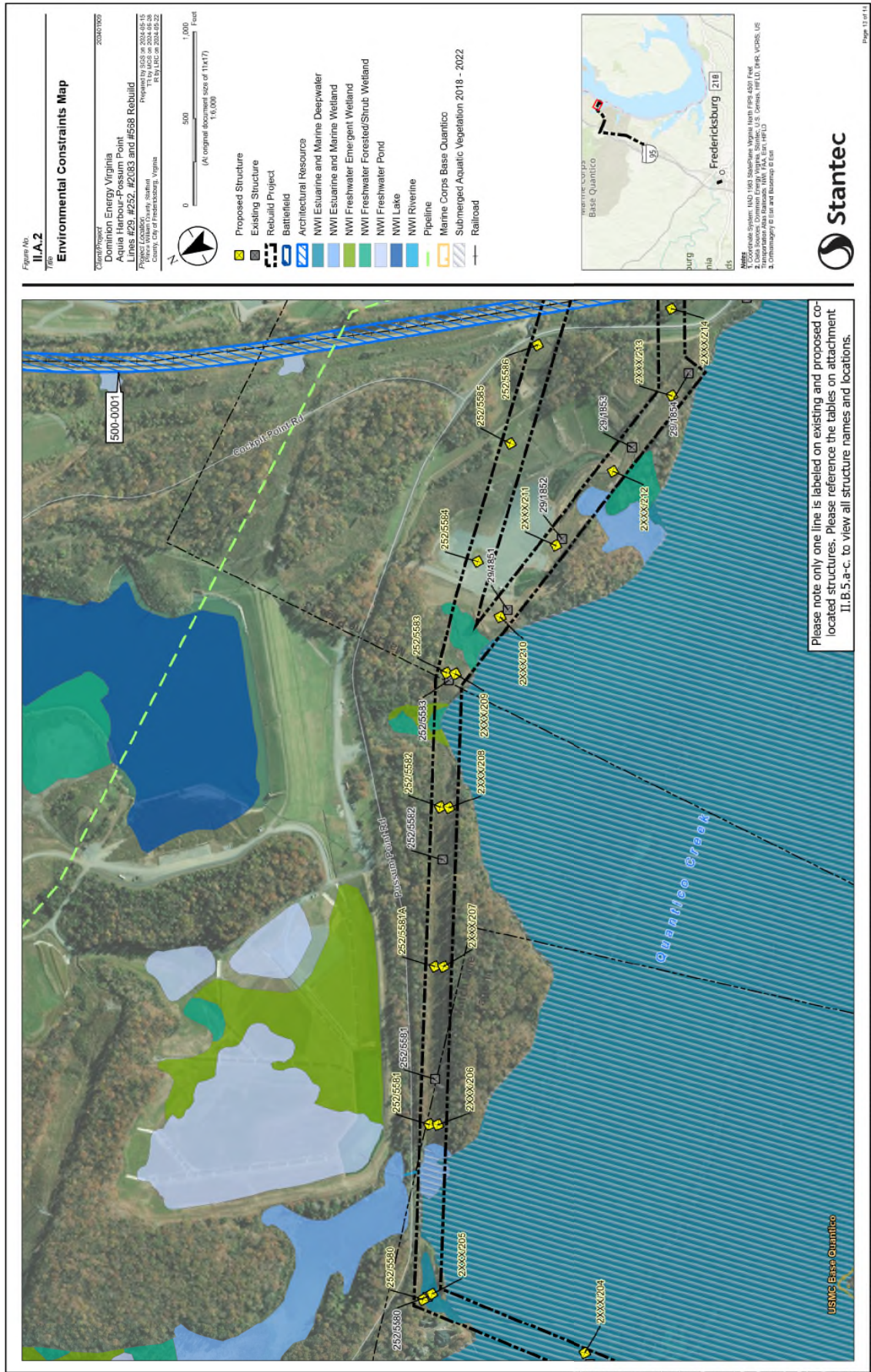


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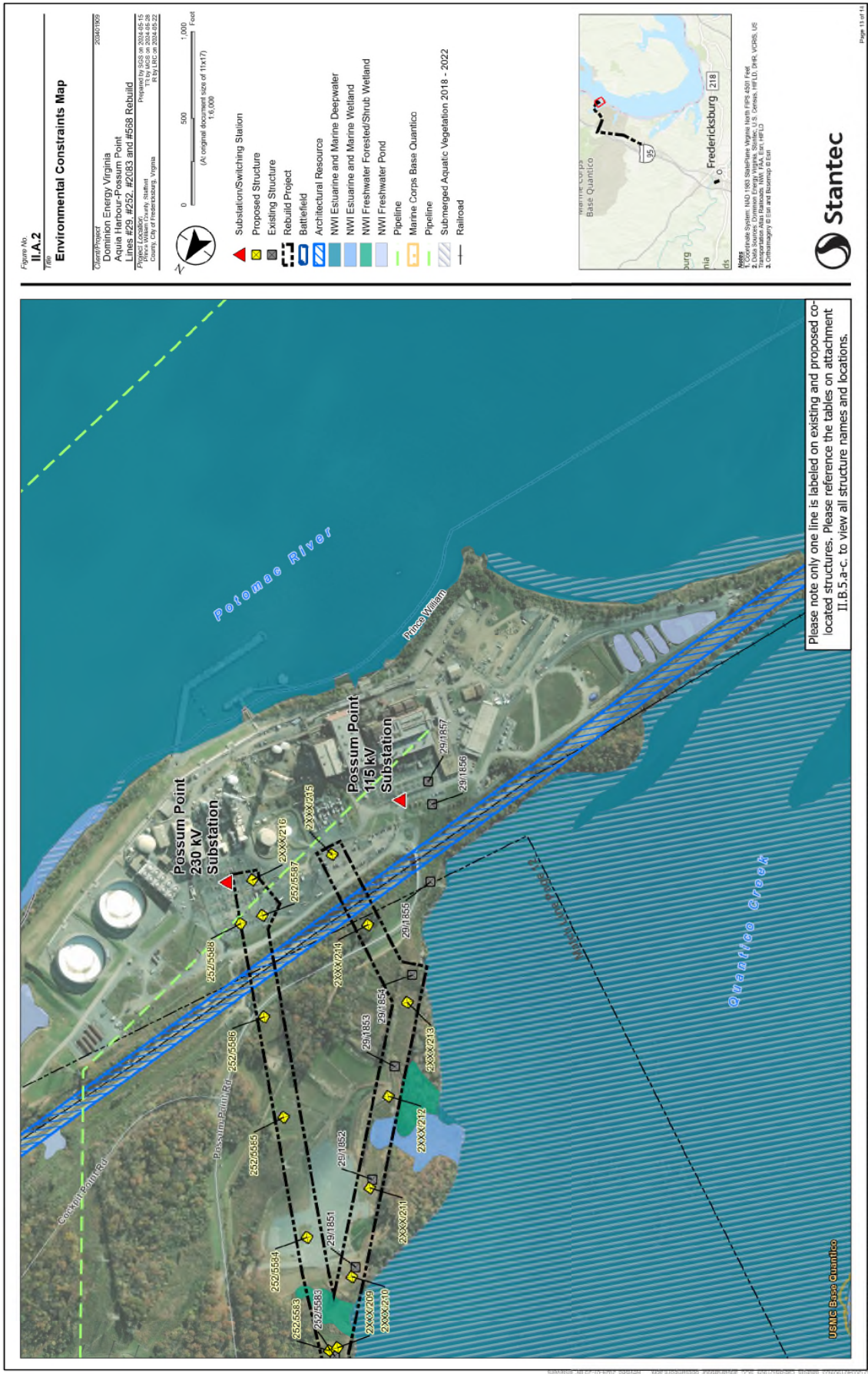


Disclaimer: This document has been prepared based on information provided by others as cited in the Index section. Statistic has not verified the accuracy and/or completeness of this information and shall not be responsible for any error or omission which may be incorporated herein as a result. Statistic assumes no responsibility for sole recipient in electronic format, and the recipient's full responsibility for verifying the accuracy and completeness of the data.

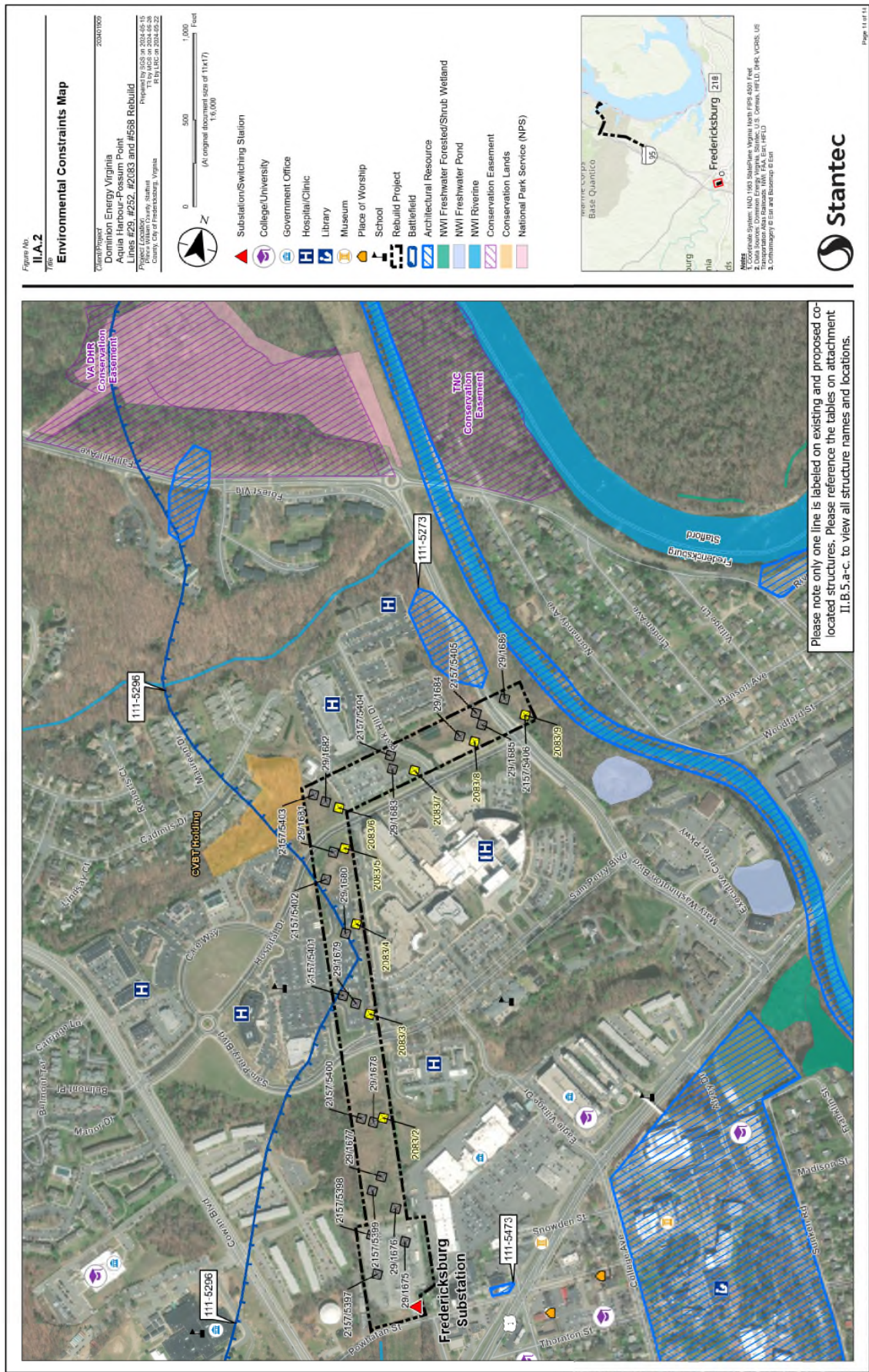












## **II. DESCRIPTION OF THE PROPOSED PROJECT**

### **A. Right-of-way (“ROW”)**

- 3. Provide a separate color map of a suitable scale showing all the Applicant’s transmission line ROWs, either existing or proposed, in the vicinity of the proposed project.**

Response: See Attachment I.G.1.

## II. DESCRIPTION OF THE PROPOSED PROJECT

### A. Right-of-way (“ROW”)

4. **To the extent the proposed route is not entirely within existing ROW, explain why existing ROW cannot adequately service the needs of the Applicant.**

Response: The Rebuild Project is located within existing rights-of-way or on Company-owned property with the exception of the 0.2 mile of 50 feet of additional right-of-way required between existing Structure #252/5568 (#29/1835) and Fuller Road Substation. The limited space in the corridor is due to existing underground and overhead distribution lines and fiber cables within the right-of-way corridor from Fuller Road Substation. To maintain adequate distance from these facilities, additional right-of-way is needed.

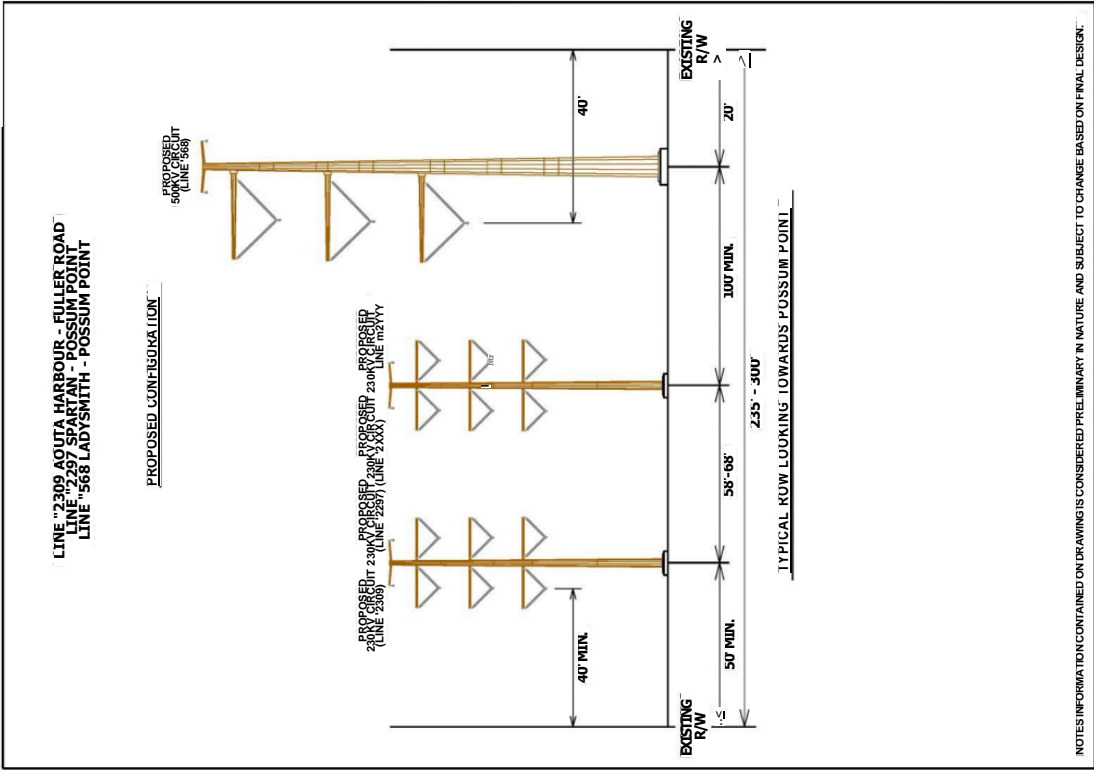
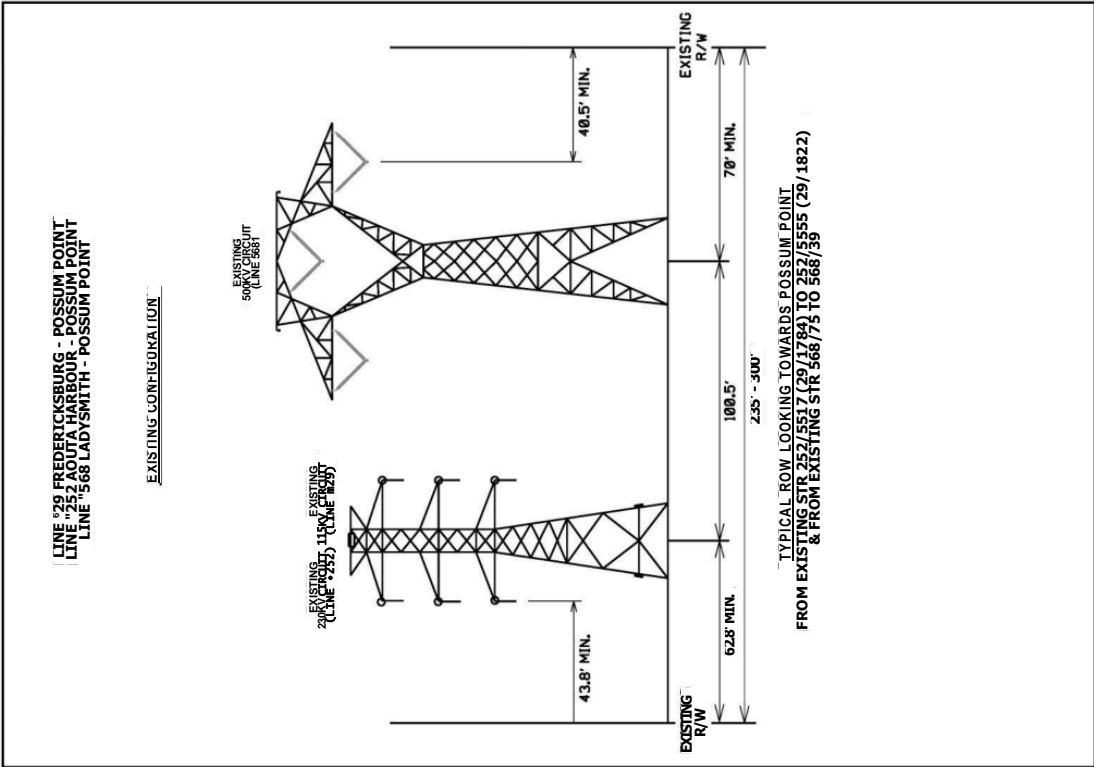
The Company proposes rebuilding the existing 0.1 mile segment northwest of the Fuller Road Substation, requiring additional right-of-way. Starting at Structure #252/5566 (#29/1833), there is no additional right-of-way. As Lines #252 and #29 travel east, the right-of-way will expand to include an additional 67 feet of width at the eastern edge of Mars Station Road. This design aims to minimize lateral loading and line angle on the proposed substation frame structure. To achieve this, the alignment of the last structure before reaching the substation will shift north, necessitating additional right-of-way for proper clearances.

## **II. DESCRIPTION OF THE PROPOSED PROJECT**

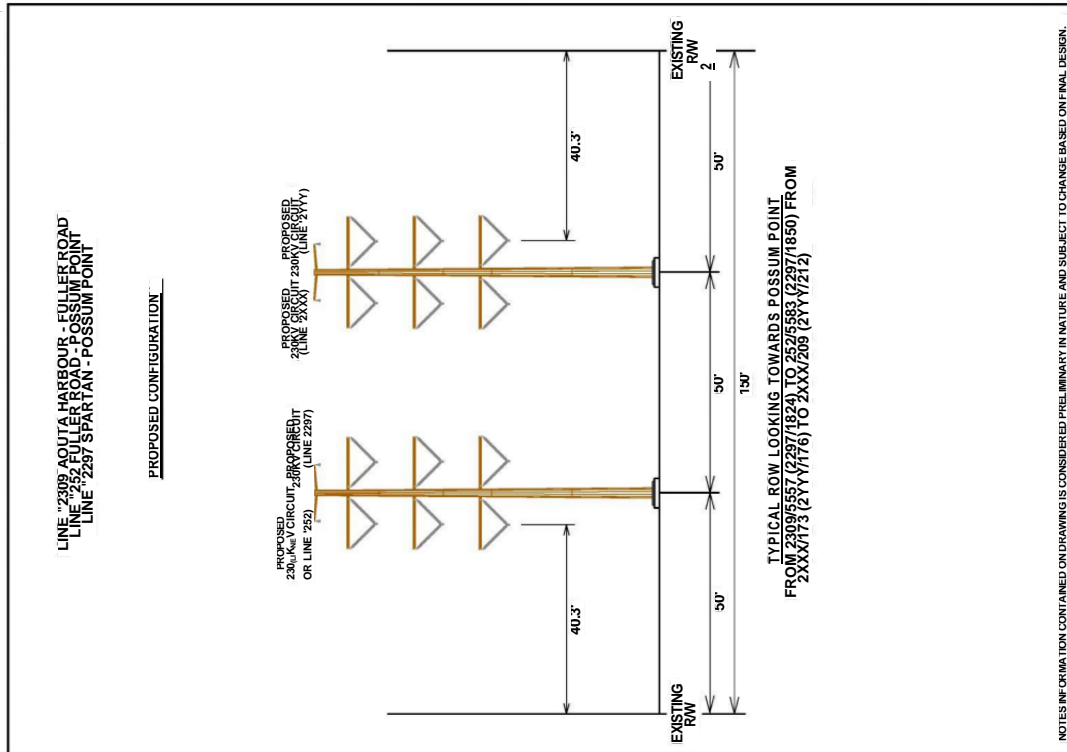
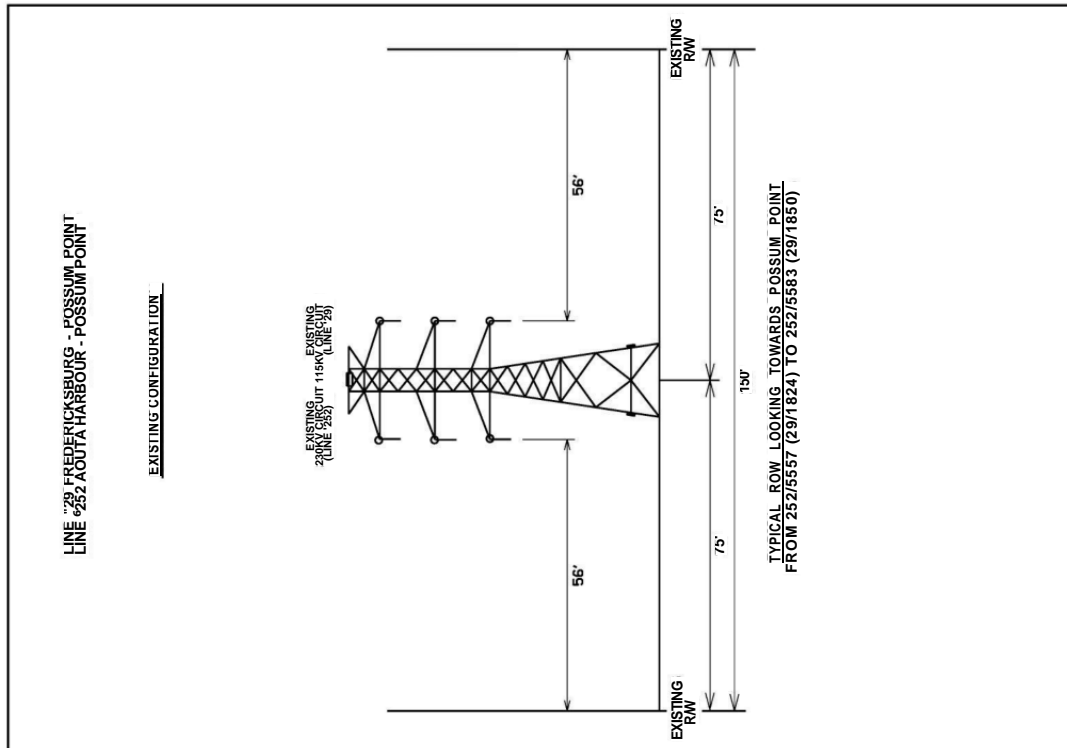
### **A. Right-of-way (“ROW”)**

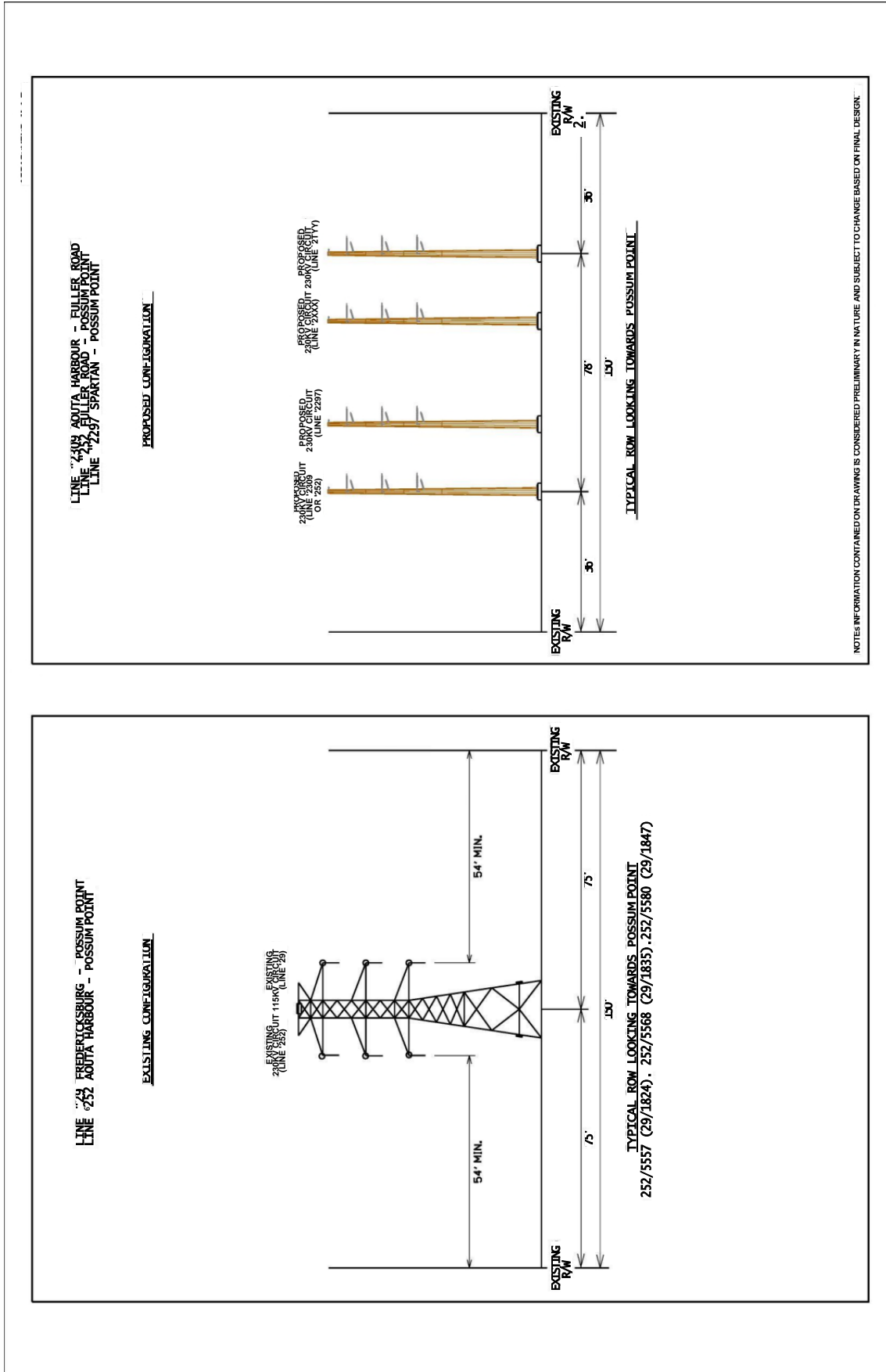
- 5. Provide drawings of the ROW cross section showing typical transmission line structure placements referenced to the edge of the ROW. These drawings should include:**
  - a. ROW width for each cross section drawing;**
  - b. Lateral distance between the conductors and edge of ROW;**
  - c. Existing utility facilities on the ROW; and**
  - d. For lines being rebuilt in existing ROW, provide all of the above (i) as it currently exists, and (ii) as it will exist at the conclusion of the proposed project.**

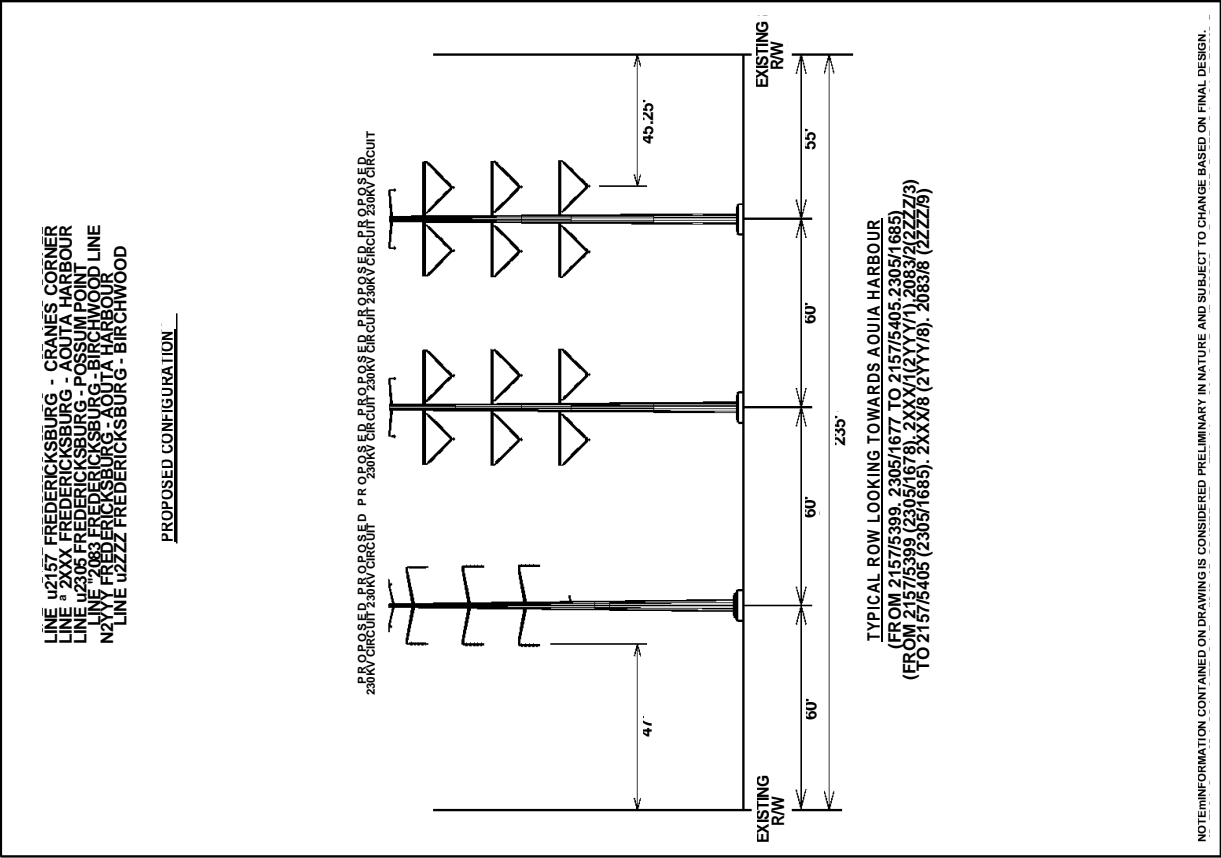
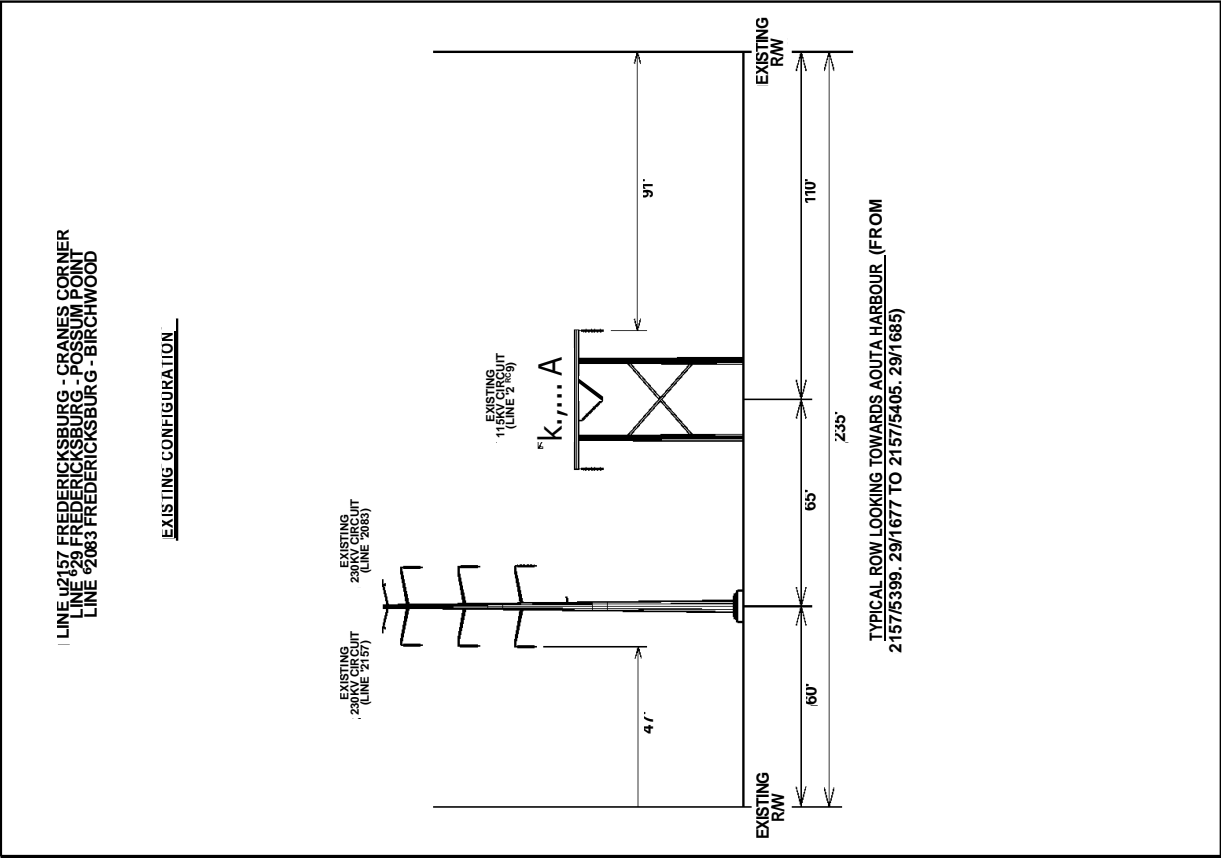
Response: See Attachments II.A.5.a-d.











NOTE: INFORMATION CONTAINED ON DRAWING IS CONSIDERED PRELIMINARY IN NATURE AND SUBJECT TO CHANGE BASED ON FINAL DESIGN.

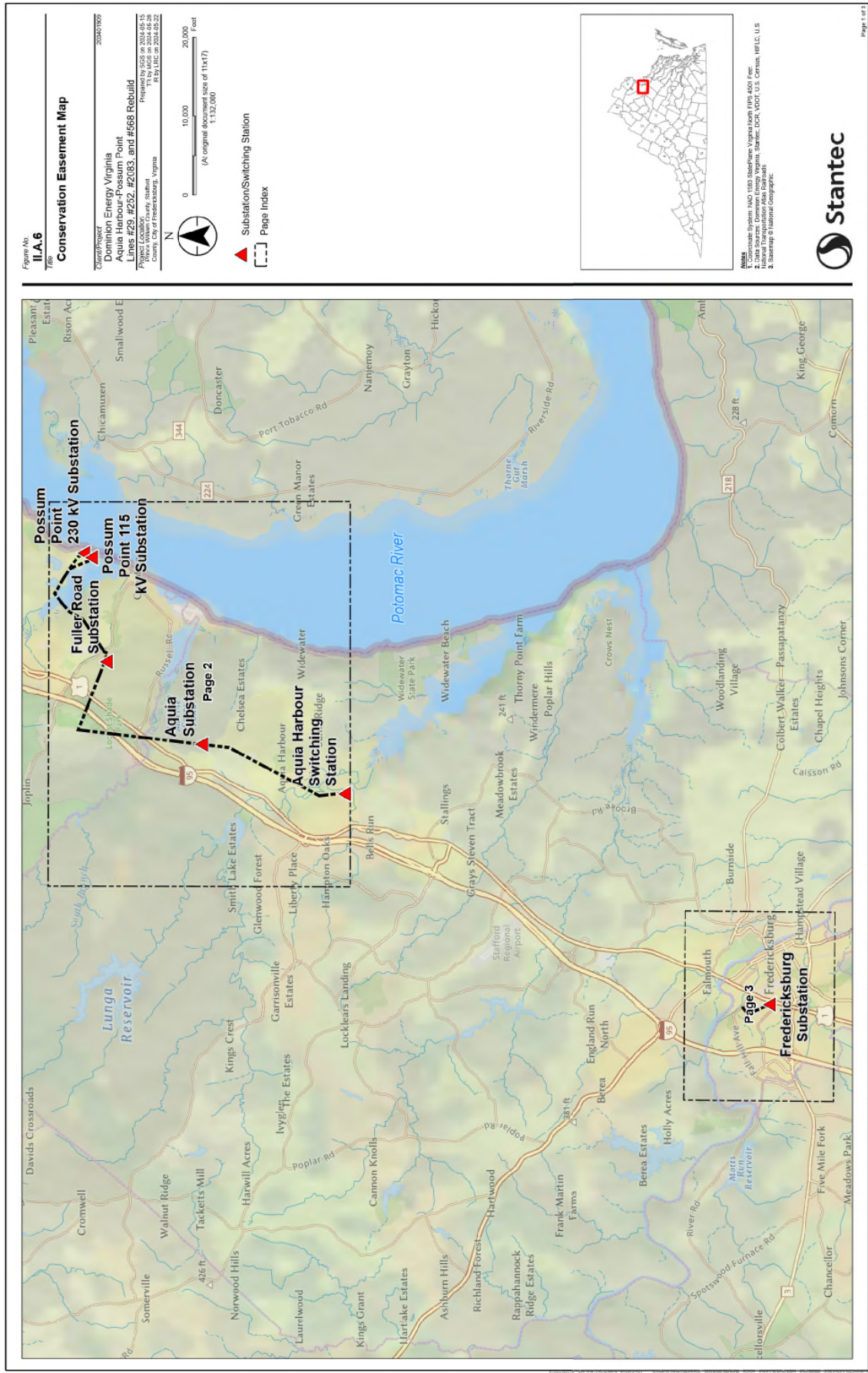
## **II. DESCRIPTION OF THE PROPOSED PROJECT**

### **A. Right-of-way (“ROW”)**

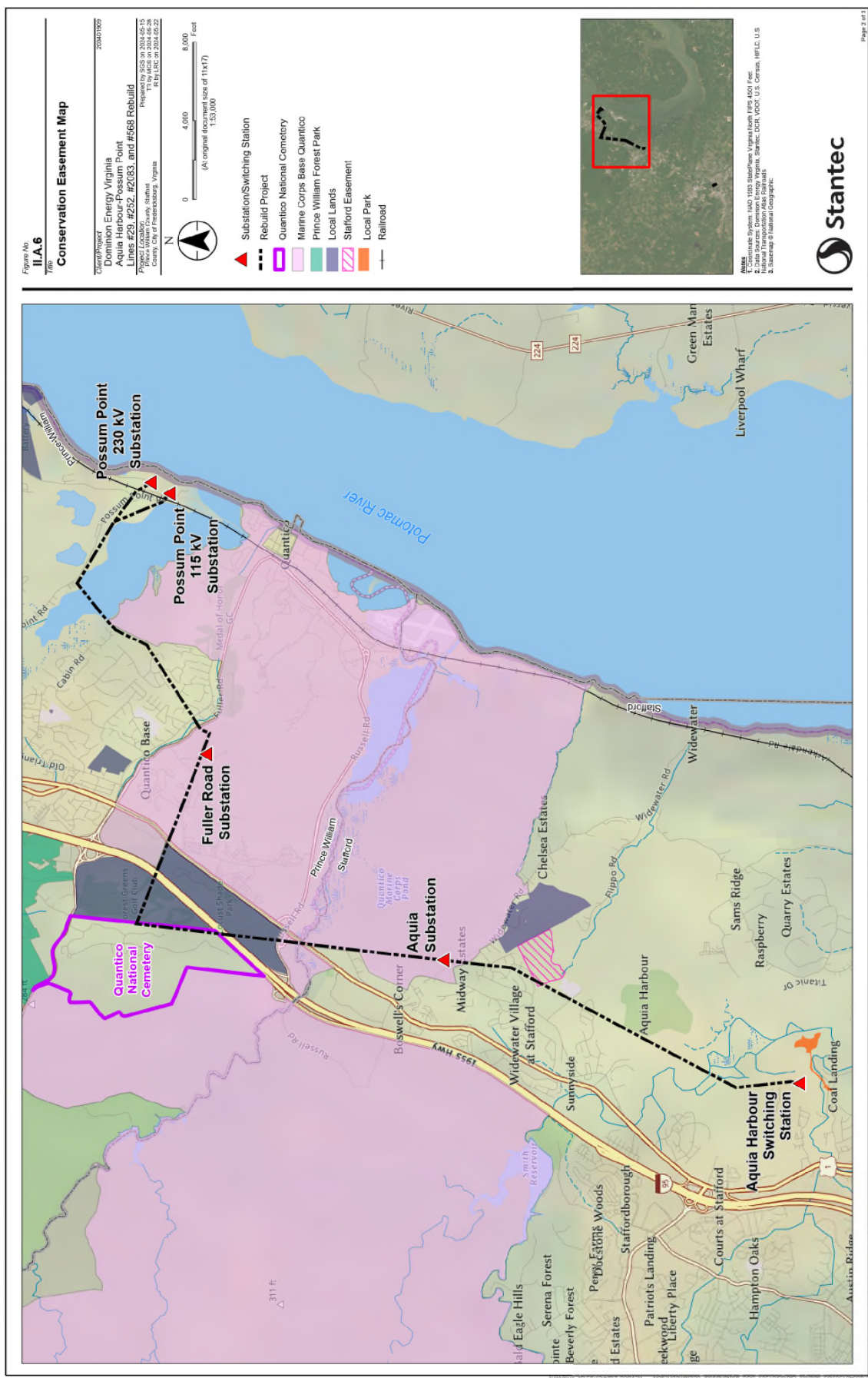
#### **6. Detail what portions of the ROW are subject to existing easements and over what portions new easements will be needed.**

Response: The Company obtained several easements along the existing right-of-way of the Rebuild Project corridor for initial construction of Lines #29 and #252 in late 1940s and early 1950s. The Company obtained several easements along the existing right-of-way of the Rebuild Project corridor for initial construction of Line #568 in 1927. The Company obtained most of easements along the existing right-of-way of the Rebuild Project corridor for initial construction of Line #2083 in 1956. New right-of-way will be required for approximately 0.2 mile east and 0.1 mile west of Fuller Road Substation.

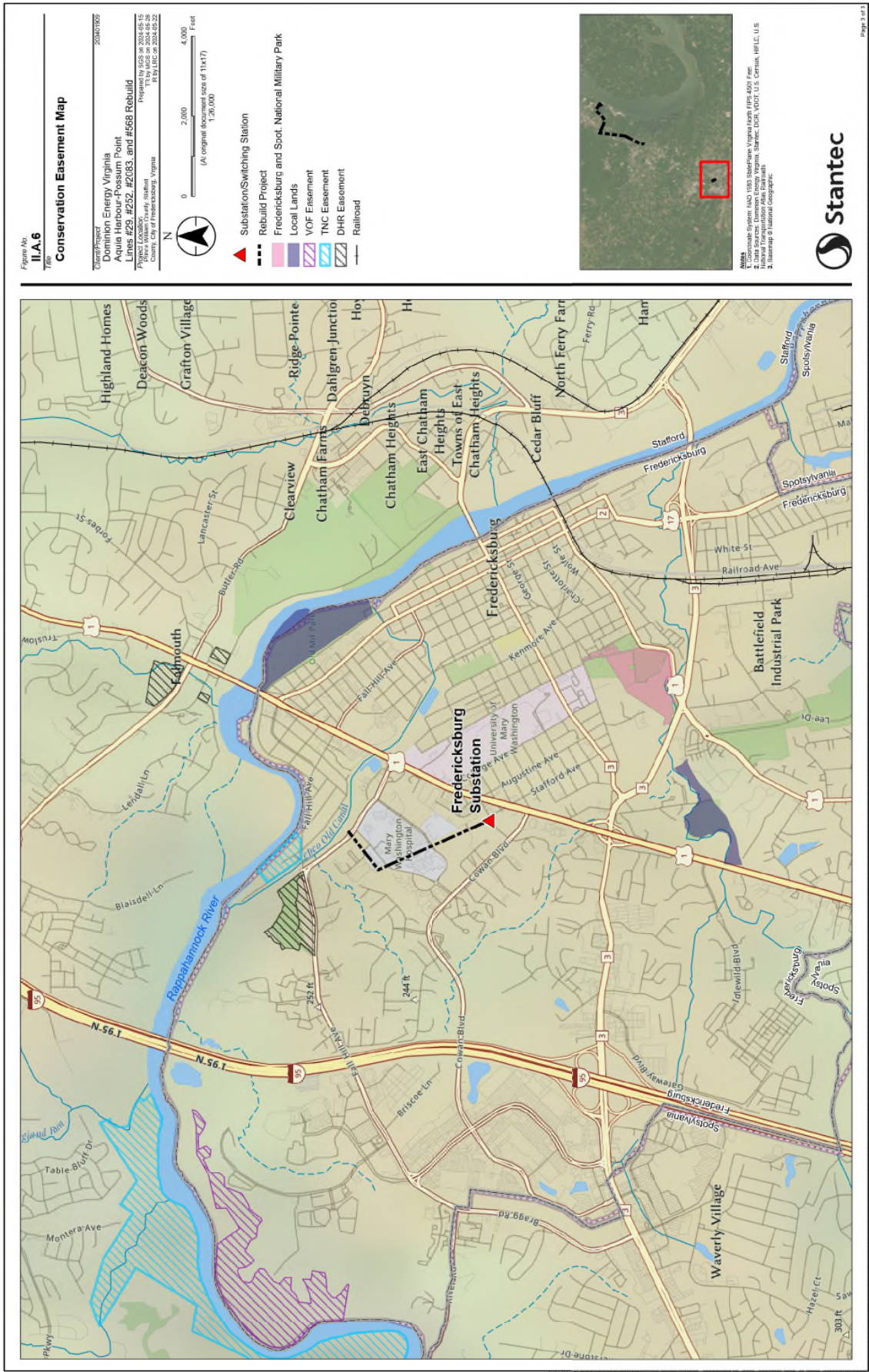
See Attachment II.A.6 for conservation easements in the vicinity of the Rebuild Project, and Section 2.L of the DEQ Supplement for a discussion of potential conservation easements. Conservation easements were established after the existing transmission corridor has been established.











## II. DESCRIPTION OF THE PROPOSED PROJECT

### A. Right-of-way (“ROW”)

#### 7. Detail the proposed ROW clearing methods to be used and the ROW restoration and maintenance practices planned for the proposed project.

Response: The majority of the existing transmission line corridor subject to the Rebuild Project, which ranges from 150 to 300 feet wide, currently is maintained for operation of the existing transmission facilities. However, 0.2 mile of additional right-of-way is needed east of Fuller Road Substation, and a 0.1 mile wedge of additional right-of-way is required west of Fuller Road Substation. Additionally, approximately 65 feet of the Company’s western edge of the right-of-way is unmaintained between Aquia Harbour Station and Aquia Substation but will be required for the Rebuild Project. The Company intends to clear any forestland within new right-of-way and remove any trees encroaching into the existing right-of-way as part of the Rebuild Project.

The trees within newly cleared right-of-way will be cut to be no more than three inches above ground level and no grubbing of roots or stumps will occur, except as needed to install structure foundations. Tree removal within wetland areas and within 100 feet of streams will be accomplished by hand or from equipment placed upon mats. Cut trees from the cleared right-of-way will be limbed and either removed from the right-of-way or mulched and chipped into upland areas. Care will be taken not to leave debris in streams or wetland areas that may cause an impediment to the flow of water. No mulching will occur in wetlands. Erosion control devices will be used where applicable on an ongoing basis, as appropriate, during all clearing and construction activities.

Trimming of tree limbs along the edge of the right-of-way may be conducted to support construction activities for the Rebuild Project. Trees located outside of the right-of-way that are tall enough to potentially impact the transmission facilities, commonly referred to as “danger trees,” may also need to be cut. Danger trees will also be cut to be no more than three inches above ground level, limbed, and will remain where felled. No grubbing of roots or stumps will occur. Debris that is adjacent to homes will be disposed of by chipping or removal. In other areas, debris may be mulched or chipped as practicable. Danger tree removal will be accomplished by hand or from equipment placed on mats in wetland areas and within 100 feet of streams, if applicable. Care will be taken not to leave debris in streams or wetland areas that may cause an impediment to the flow of water. No mulching will occur in wetlands.

Erosion control will be maintained and temporary stabilization for all soil-disturbing activities will be used until the right-of-way has been restored. Upon completion of the Rebuild Project, the Company will restore the right-of-way utilizing site rehabilitation procedures outlined in the Company’s General Erosion

and Sedimentation Control Specifications for the Construction and Maintenance of Electric Transmission Lines that is approved yearly by the Virginia Department of Environmental Quality (“DEQ”). Time of year and weather conditions may affect when permanent stabilization takes place.

In addition to the clearing required within new right-of-way at Fuller Road Substation and encroachments into existing right-of-way between Aquia Harbour Station and Aquia Substation, limited clearing or limbing may be required to accommodate construction access. Clearing will be done in accordance with the Company’s Integrated Vegetation Management Plan (“IVMP”) practice with no grabbing of roots or stump materials. The remainder of the existing right-of-way is currently cleared and maintained.

The right-of-way will continue to be maintained on a regular cycle to prevent interruptions to electric service and provide ready access to the right-of-way in order to patrol and make emergency repairs. Periodic maintenance to control woody growth will consist of hand cutting, machine mowing and/or herbicide application.

## **II. DESCRIPTION OF THE PROPOSED PROJECT**

### **A. Right-of-way (“ROW”)**

#### **8. Indicate the permitted uses of the proposed ROW by the easement landowner and the Applicant.**

Response: Any non-transmission use will be permitted that:

- Is in accordance with the terms of the easement agreement for the right-of-way;
- Is consistent with the safe maintenance and operation of the transmission lines;
- Will not restrict future line design flexibility; and
- Will not permanently interfere with future construction.

Subject to the terms of the easement, examples of typical permitted uses include but are not limited to:

- Agriculture;
- Hiking Trails;
- Fences;
- Perpendicular Road Crossings;
- Perpendicular Utility Crossings;
- Residential Driveways; and
- Wildlife / Pollinator Habitat.



## II. DESCRIPTION OF THE PROPOSED PROJECT

### A. Right-of-way (“ROW”)

9. **Describe the Applicant’s route selection procedures. Detail the feasible alternative routes considered. For each such route, provide the estimated cost and identify and describe the cost classification (e.g. “conceptual cost,” “detailed cost,” etc.). Describe the Applicant’s efforts in considering these feasible alternatives. Detail why the proposed route was selected and other feasible alternatives were rejected. In the event that the proposed route crosses, or one of the feasible routes was rejected in part due to the need to cross, land managed by federal, state, or local agencies or conservation easements or open space easements qualifying under §§ 10.1-1009 – 1016 or §§ 10.1-1700 – 1705 of the Code (or a comparable prior or subsequent provision of the Code), describe the Applicant’s efforts to secure the necessary ROW.**

Response: The Company’s route selection for transmission line rebuild projects begins with a review of the existing right-of-way. This approach generally minimizes impacts on the natural and human environments. This approach also is consistent with FERC Guideline #1 (included as Attachment 1 to these Guidelines), which states that existing rights-of-way should be given priority when adding new transmission facilities, and §§ 56-46.1 and 56-529 of the Code of Virginia, which promote the use of existing rights-of-way for new transmission facilities.

The Rebuild Project is located in existing right-of-way or on Company-owned property, with the exception of a small area (0.2 mile) between Fuller Road Substation and existing Structure #252/5568 (#29/1835) where the Company will need to expand its right of way by approximately 50 feet, and a small area (0.1 mile) northwest of the Fuller Road Substation. Because the statutory preference given to the use of existing rights-of-way, and because additional costs and environmental impacts would be associated with the acquisition of and construction on new right-of-way, the Company did not consider any alternate routes where existing right-of-way is sufficient.

The existing right-of-way crosses the easements and facilities listed in Section II.A.6 and as depicted on Attachment II.A.6.

## II. DESCRIPTION OF THE PROPOSED PROJECT

### A. Right-of-way (“ROW”)

- 10. Describe the Applicant’s construction plans for the project, including how the Applicant will minimize service disruption to the affected load area. Include requested and approved line outage schedules for affected lines as appropriate.**

Response: The Company plans to rebuild the corridor in a manner that minimizes outage durations on Lines #29, #252, #568, and #2083. Assuming that the Commission issues a final order by February 28, 2025, the Company will commence access and foundation construction in the first quarter of 2026.

The Company plans to use the newly built additional circuits as temporary circuits for Line #29 and Line #252 during construction. This will require installing temporary jumpers to connect existing lines to the newly installed additional circuits. Doing so will reduce the outage durations on the lines and allow for segments of the lines to be wrecked and rebuilt during the PJM peak seasons without necessitating an outage. Thus, the Company has submitted outages to support the construction sequence as outlined below:

Season	Work to Be Completed
Spring 2026	<ul style="list-style-type: none"><li>• Install foundations, single circuit structures, and conductor to relocate Line #568 to the east side of the corridor during March through June shoulder season outage.</li><li>• Install foundations, double circuit monopole structures, and conductor for new third and fourth 230 kV circuits.</li><li>• Install temporary configuration between Lines #252 and #29 and newly installed double circuit structures.</li><li>• Wreck and rebuild Line #2083 on double circuit monopoles with one vacant arm between Fredericksburg Substation and Hospital Junction.</li></ul>
Summer 2026	<ul style="list-style-type: none"><li>• Wreck and rebuild deenergized Lines #252 and #29 between installed temporary configuration without any outages.</li><li>• Install foundations where clearances allow to facilitate installation of Line #568 and additional third/fourth 230 kV circuit structures and conductor during next outage season.</li></ul>
Fall 2026	<ul style="list-style-type: none"><li>• Remove temporary configuration on Lines #252 and #29.</li><li>• Install remaining foundations, single circuit structures, and conductor to relocate Line #568 to the east side of the corridor during September through December shoulder season outage.</li><li>• Install foundations, double circuit monopole structures, and conductor for new third and fourth 230 kV circuits.</li></ul>

Season	Work to Be Completed
	<ul style="list-style-type: none"> <li>• Install temporary configuration between Lines #252 and #29 and newly installed double circuit structures.</li> </ul>
Winter 2026	<ul style="list-style-type: none"> <li>• Wreck and rebuild deenergized Lines #252 and #29 between installed temporary configuration without outage.</li> <li>• Install temporary configuration on Line #29 to keep MCBQ energized during Fuller Road Substation work without outage.</li> </ul>
Spring 2027	<ul style="list-style-type: none"> <li>• Remove temporary configuration on Lines #252 and #29.</li> <li>• Wreck Line #252 between Structure #252/5518 and Fuller Road Substation and rebuild on double circuit monopoles.</li> <li>• Wreck Line #29 between Structure #29/1785 and the Quantico Tap. Rebuild on double circuit monopoles.</li> </ul>
Summer 2027	<ul style="list-style-type: none"> <li>• Install all equipment and matting to facilitate crossing of Quantico Creek during next outage.</li> </ul>
Fall 2027	<ul style="list-style-type: none"> <li>• Wreck Line #29 between the Quantico Tap and Possum Point Station. Rebuild on double circuit monopoles.</li> <li>• Wreck Line #252 between the Quantico Tap and Possum Point Station. Rebuild on double circuit monopoles.</li> </ul>
Winter 2027	<ul style="list-style-type: none"> <li>• Continue to wreck Line #29 between the Quantico Tap and Possum Point Station. Rebuild on double circuit monopoles.</li> <li>• Continue to wreck Line #252 between the Quantico Tap and Possum Point Station. Rebuild on double circuit monopoles.</li> </ul>
Spring 2028	<ul style="list-style-type: none"> <li>• Remove all previously installed temporary configurations and jumpers.</li> <li>• Clear, grade and prepare ROW between Fuller Road Substation and future attachment point, Structure #29/3 for 115 kV feed to Quantico Substation.</li> </ul>
Winter 2028	<ul style="list-style-type: none"> <li>• Finalize all Fuller Road Substation work, energize four 230 kV lines.</li> </ul>

This work schedule is subject to final engineering and is contingent upon obtaining necessary outages, the latter of which may be particularly challenging due to the amount of new load growth, rebuilds, and new builds scheduled to occur in this load area.

## **II. DESCRIPTION OF THE PROPOSED PROJECT**

### **A. Right-of-way (“ROW”)**

#### **11. Indicate how the construction of this transmission line follows the provisions discussed in Attachment 1 of these Guidelines.**

Response: As noted in Section II.A.9, Attachment 1 of these Guidelines provides a tool routinely used by the Company in routing its transmission line projects.

The Company utilized Guideline #1 (existing rights-of-way should be given priority when adding additional facilities) by siting the proposed Rebuild Project almost entirely within the existing transmission corridor, as discussed in Section II.A.9.

By utilizing the existing transmission corridor, the proposed Rebuild Project will minimize impact to any site listed on the National Register of Historic Places (“NRHP”). Thus, the Rebuild Project is consistent with Guideline #2 (where practical, rights-of-way should avoid sites listed on the National Register of Historic Places. See Section III.A for a discussion of the Stage I Pre-Application Analysis prepared by Stantec, which is included with the DEQ Supplement as Attachment 2.I.2. The Company will coordinate with the Virginia Department of Historic Resources (“VDHR”) through review of the Stage I Pre-Application Analysis regarding these initial findings.

The Company has communicated with a number of local, state, and federal agencies prior to filing this application consistent with Guideline #4 (where government land is involved the applicant should contact the agencies early in the planning process). See Section III.B and the DEQ Supplement.

The Company follows recommended construction methods on a site-specific basis for typical construction projects (Guidelines #8, #10, #11, #15, #16, #18, and #22).

The Company also utilizes recommended guidelines in the clearing of transmission line rights-of-way, constructing facilities and maintaining rights-of-way after construction. Moreover, secondary uses of rights-of-way that are consistent with the safe maintenance and operation of facilities are permitted.

## II. DESCRIPTION OF THE PROPOSED PROJECT

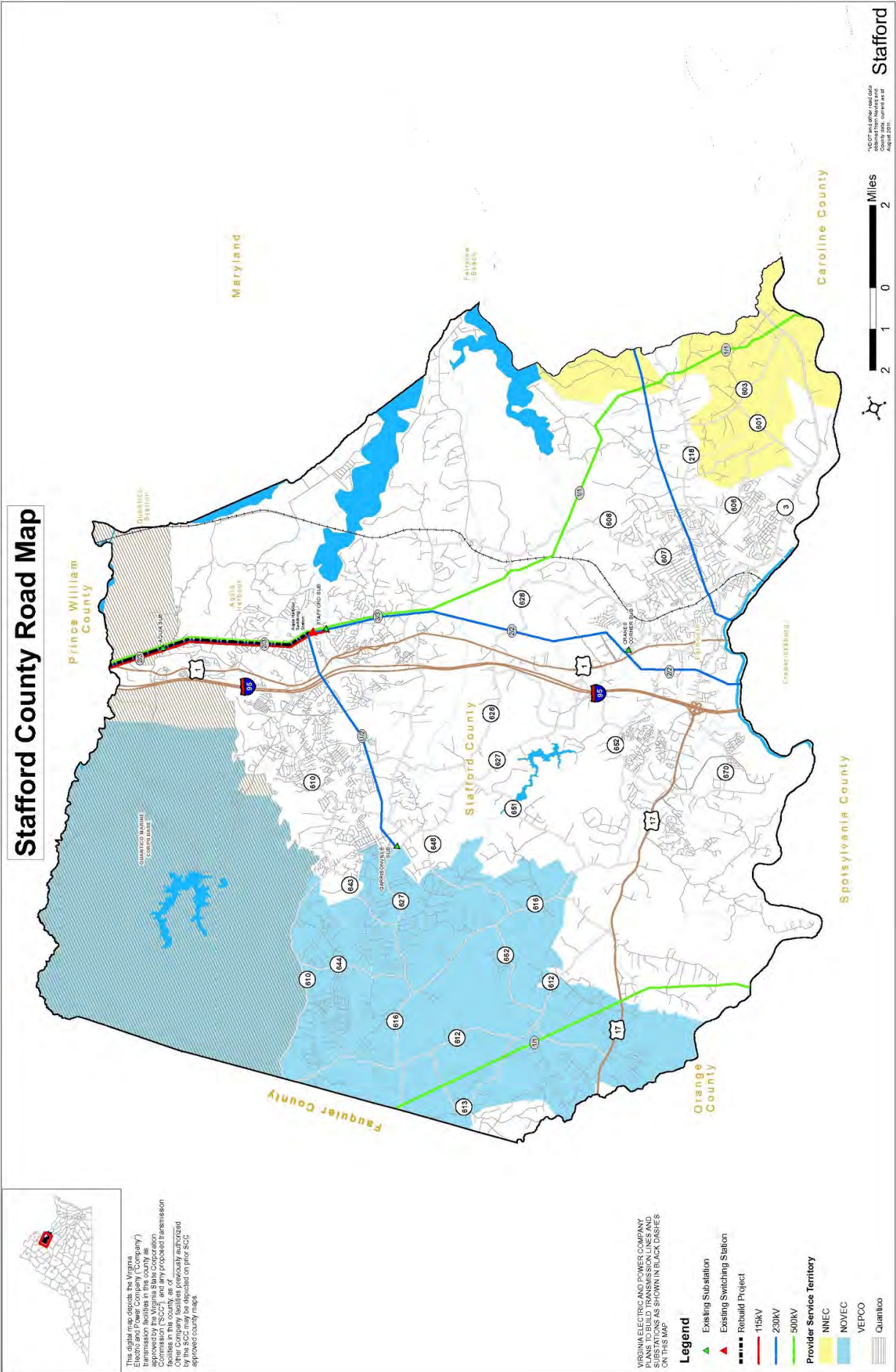
### A. Right-of-way (“ROW”)

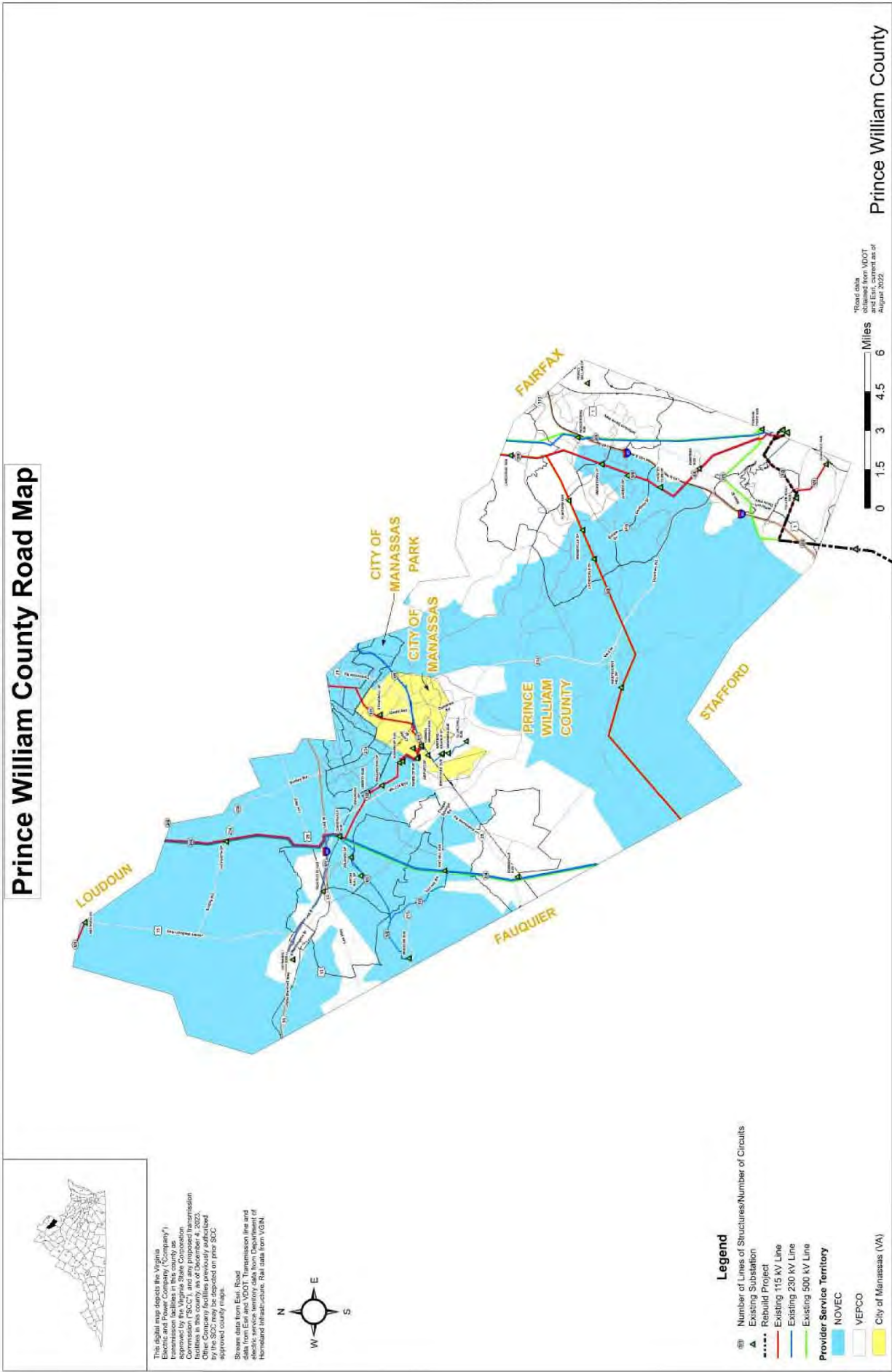
12. a. Detail counties and localities through which the line will pass. If any portion of the line will be located outside of the Applicant’s certificated service area: (1) identify each electric utility affected; (2) state whether any affected electric utility objects to such construction; and (3) identify the length of line(s) proposed to be located in the service area of an electric utility other than the Applicant; and
- b. Provide three (3) color copies of the Virginia Department of Transportation “General Highway Map” for each county and city through which the line will pass. On the maps show the proposed line and all previously approved and certificated facilities of the Applicant. Also, where the line will be located outside of the Applicant’s certificated service area, show the boundaries between the Applicant and each affected electric utility. On each map where the proposed line would be outside of the Applicant’s certificated service area, the map must include a signature of an appropriate representative of the affected electric utility indicating that the affected utility is not opposed to the proposed construction within its service area.

Response:

- a. The Rebuild Project crosses through Stafford County for approximately 5.1 miles, Prince William County for 6.7 miles, and the City of Fredericksburg for 0.7 mile. The Rebuild Project is located entirely within the Company’s service territory.
- b. Electronic versions of Virginia Department of Transportation (“VDOT”) “General Highway Map” for Stafford County, Prince William County, and the City of Fredericksburg have been marked as required and will be made available with the Application. Reduced copies of the map are provided as Attachment II.A.12.b.







## **II. DESCRIPTION OF THE PROPOSED PROJECT**

### **B. Line Design and Operational Features**

- 1. Detail the number of circuits and their design voltage, initial operational voltage, any anticipated voltage upgrade, and transfer capabilities.**

Response: Line #29 will be designed to current 230 kV standards. No voltage upgrades are anticipated. The bundled 768.2 ACSS/TW/HS conductors will have a transfer capability of 1,573 MVA. Line #29 will be rebuilt on double circuit monopole structures.

Line #252 will be designed to current 230 kV standards. No voltage upgrades are anticipated. The bundled 768.2 ACSS/TW/HS conductors will have a transfer capability of 1,573 MVA. Line #252 will be rebuilt on double circuit monopole structures.

Line #2083 will be designed to 230 kV standards with no anticipated voltage upgrade. The bundled 768.2 ACSS/TW/HS conductors will have a transfer capability of 1,573 MVA. Line #2083 will be rebuilt on double circuit monopole structures.

Line #568 will be designed to current 500 kV standards with no anticipated voltage upgrade. Line #568 will be rebuilt on single circuit monopole structures. The proposed bundled 3-1351.5 ACSR (45/7) conductor will have a transfer capability of 4,356 MVA.

The additional double circuit will be designed to current 230 kV standards. No voltage upgrades are anticipated. The bundled 768.2 ACSS/TW/HS conductors will have a transfer capability of 1,573 MVA. These future lines will be constructed on double circuit monopole structures.

## **II. DESCRIPTION OF THE PROPOSED PROJECT**

### **B. Line Design and Operational Features**

- 2. Detail the number, size(s), type(s), coating and typical configurations of conductors. Provide the rationale for the type(s) of conductor(s) to be used.**

Response: Lines #29, #252, and #2083 will have bundled two 768.2 ACSS/TW/HS conductors, which is a Company standard for new 230 kV construction. Line #568 will have bundled triple 1351.5 ACSR (45/7) conductors, which is also a Company standard.

## **II. DESCRIPTION OF THE PROPOSED PROJECT**

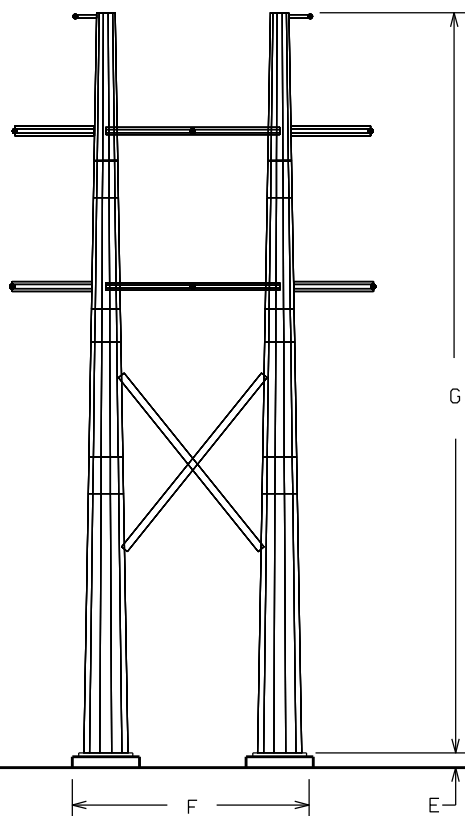
### **B. Line Design and Operational Features**

- 3. With regard to the proposed supporting structures over each portion of the ROW for the preferred route, provide diagrams (including foundation reveal) and descriptions of all the structure types, to include:**
  - a. mapping that identifies each portion of the preferred route;**
  - b. the rationale for the selection of the structure type;**
  - c. the number of each type of structure and the length of each portion of the ROW;**
  - d. the structure material and rationale for the selection of such material;**
  - e. the foundation material;**
  - f. the average width at cross arms;**
  - g. the average width at the base;**
  - h. the maximum, minimum and average structure heights;**
  - i. the average span length; and**
  - j. the minimum conductor-to-ground clearances under maximum operating conditions.**

Response: See Attachments II.B.3.a – II.B.3.o.



**230KV LINE #2309 AQUIA HARBOUR - FULLER ROAD  
230KV LINE #2297 AQUIA HARBOUR - POSSUM POINT**



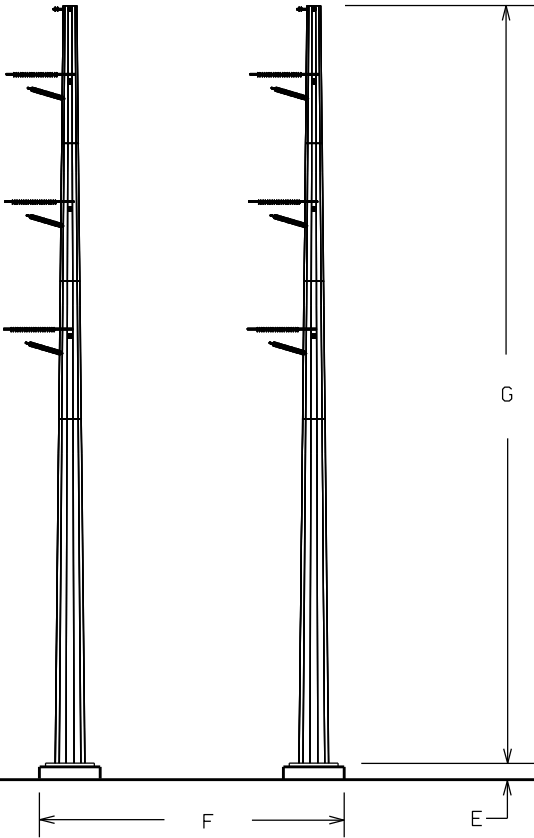
**DOUBLE CIRCUIT DEADEND H-FRAME STRUCTURE**

A. MAPPING OF THE ROUTE:	SEE ATTACHMENT II.B.5
B. RATIONALE FOR STRUCTURE TYPE:	MAINTAINS FLAT CONFIGURATION AT THE SUBSTATION INTERFACE FLAT CONFIGURATION FACILITATES FUTURE CROSSINGS & SWITCH INSTALLATION OPTIONS
C. LENGTH OF R/W (STRUCTURE QTY):	0.26 MILES (2)
D. STRUCTURE MATERIAL: RATIONAL FOR MATERIAL:	WEATHERING STEEL TO MATCH MATERIAL FINISH OF EXISTING STRUCTURES
E. FOUNDATION MATERIAL: AVERAGE FOUNDATION REVEAL:	CONCRETE SEE NOTE 2
F. AVERAGE WIDTH AT BASE:	29.5', 6' DIAMETER FOUNDATION (SEE NOTE 3)
G. MINIMUM STRUCTURE HEIGHT: MAXIMUM STRUCTURE HEIGHT: AVERAGE STRUCTURE HEIGHT:	100' 100' 100'
H. AVERAGE SPAN LENGTH (RANGE):	689' (683' - 695') (WIND SPAN)
I. MINIMUM CONDUCTOR-TO-GROUND:	25.5' (AT MAXIMUM OPERATING TEMPERATURE)

**NOTE:**

1. INFORMATION CONTAINED ON DRAWING IS PRELIMINARY IN NATURE AND SUBJECT TO CHANGE DURING FINAL DESIGN.
2. MINIMUM FOUNDATION REVEAL SHALL BE 1.5'
3. FINAL FOUNDATION DIAMETER SHALL BE BASED UPON FINAL ENGINEERING.
4. STRUCTURE HEIGHTS ARE MEASURED FROM THE STRUCTURE CENTERLINE.

230KV LINE #2309 AQUIA HARBOUR - FULLER ROAD  
230KV LINE #2297 AQUIA HARBOUR - POSSUM POINT  
230KV LINE #252 FULLER ROAD - POSSUM POINT



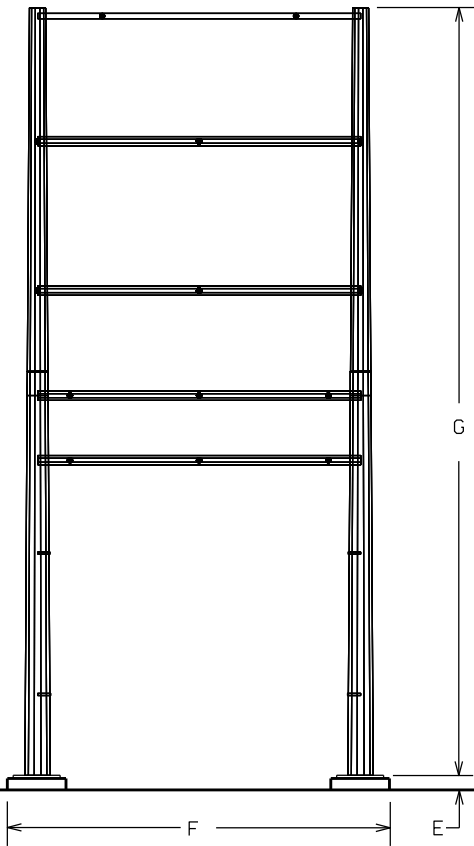
**DOUBLE CIRCUIT DEADEND 2-POLE STRUCTURE**

A. MAPPING OF THE ROUTE:	SEE ATTACHMENT II.B.5
B. RATIONALE FOR STRUCTURE TYPE:	ACCOMODATES EFFICIENT USE R/W, REDUCES BLOWOUT FOOTPRINT. MOST SUITABLE FOR HEAVY ANGLES AND INTERFACE WITH DELIVERY POINTS.
C. LENGTH OF R/W (STRUCTURE QTY):	0.75 MILES (6)
D. STRUCTURE MATERIAL: RATIONAL FOR MATERIAL:	WEATHERING STEEL WEATHERING STEEL WAS SELECTED FOR ITS CORROSION RESISTANCE, ENVIRONMENTAL SUSTAINABILITY DUE TO LOW MAINTENANCE, AESTHETIC APPEAL, LOW COST AND LONGEVITY.
E. FOUNDATION MATERIAL: AVERAGE FOUNDATION REVEAL:	CONCRETE SEE NOTE 2
F. AVERAGE WIDTH AT BASE:	27'-29.5', 6' DIAMETER FOUNDATION (SEE NOTE 3)
G. MINIMUM STRUCTURE HEIGHT: MAXIMUM STRUCTURE HEIGHT: AVERAGE STRUCTURE HEIGHT:	85' 125' 109'
H. AVERAGE SPAN LENGTH (RANGE):	658' (374' - 994') (WIND SPAN)
I. MINIMUM CONDUCTOR-TO-GROUND:	25.5' (AT MAXIMUM OPERATING TEMPERATURE)

**NOTE:**

1. INFORMATION CONTAINED ON DRAWING IS PRELIMINARY IN NATURE AND SUBJECT TO CHANGE DURING FINAL DESIGN.
2. MINIMUM FOUNDATION REVEAL SHALL BE 1.5'
3. FINAL FOUNDATION DIAMETER SHALL BE BASED UPON FINAL ENGINEERING.
4. STRUCTURE HEIGHTS ARE MEASURED FROM THE STRUCTURE CENTERLINE.

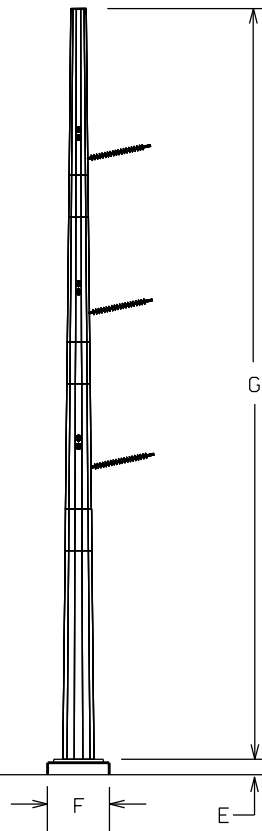
230KV LINE #2297 AQUIA HARBOUR - POSSUM POINT  
230KV LINE #2309 AQUIA HARBOUR - FULLER ROAD



DOUBLE CIRCUIT BACKBONE STRUCTURE

A. MAPPING OF THE ROUTE:	SEE ATTACHMENT II.B.5
B. RATIONALE FOR STRUCTURE TYPE:	MAINTAINS FLAT CONFIGURATION AT THE SUBSTATION INTERFACE
C. LENGTH OF R/W (STRUCTURE QTY):	0.16 MILES (3)
D. STRUCTURE MATERIAL: RATIONAL FOR MATERIAL:	GALVANIZED STEEL GALVANIZED STEEL WAS SELECTED TO MATCH EXISTING GALVANIZED STRUCTURES INSIDE SUBSTATIONS.
E. FOUNDATION MATERIAL: AVERAGE FOUNDATION REVEAL:	CONCRETE SEE NOTE 2
F. AVERAGE WIDTH AT BASE:	46', 6' DIAMETER FOUNDATION (SEE NOTE 3)
G. MINIMUM STRUCTURE HEIGHT: MAXIMUM STRUCTURE HEIGHT: AVERAGE STRUCTURE HEIGHT:	95' 95' 95'
H. AVERAGE SPAN LENGTH (RANGE):	278' (222' - 319') (WIND SPAN)
I. MINIMUM CONDUCTOR-TO-GROUND:	25.5' (AT MAXIMUM OPERATING TEMPERATURE)

- NOTE:**
- 1. INFORMATION CONTAINED ON DRAWING IS PRELIMINARY IN NATURE AND SUBJECT TO CHANGE DURING FINAL DESIGN.
  - 2. MINIMUM FOUNDATION REVEAL SHALL BE 1.5'
  - 3. FINAL FOUNDATION DIAMETER SHALL BE BASED UPON FINAL ENGINEERING.
  - 4. STRUCTURE HEIGHTS ARE MEASURED FROM THE STRUCTURE CENTERLINE.

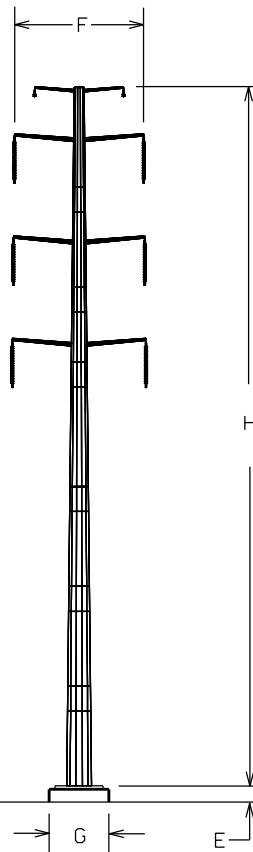
**230KV LINE #2309 AQUIA HARBOUR - FULLER ROAD****SINGLE CIRCUIT DEADEND MONOPOLE STRUCTURE**

A. MAPPING OF THE ROUTE:	SEE ATTACHMENT II.B.5
B. RATIONALE FOR STRUCTURE TYPE:	ACCOMMODATES EFFICIENT USE OF R/W AND REDUCES BLOWOUT FOOTPRINT.
C. LENGTH OF R/W (STRUCTURE QTY):	0.07 MILES (3)
D. STRUCTURE MATERIAL: RATIONAL FOR MATERIAL:	WEATHERING STEEL WEATHERING STEEL WAS SELECTED FOR ITS CORROSION RESISTANCE, ENVIRONMENTAL SUSTAINABILITY DUE TO LOW MAINTENANCE, AESTHETIC APPEAL, LOW COST AND LONGEVITY.
E. FOUNDATION MATERIAL: AVERAGE FOUNDATION REVEAL:	CONCRETE SEE NOTE 2
F. AVERAGE WIDTH AT BASE:	6' DIAMETER FOUNDATION (SEE NOTE 3)
G. MINIMUM STRUCTURE HEIGHT: MAXIMUM STRUCTURE HEIGHT: AVERAGE STRUCTURE HEIGHT:	125' 145' 132'
H. AVERAGE SPAN LENGTH (RANGE):	128' (69' - 200') (WIND SPAN)
I. MINIMUM CONDUCTOR-TO-GROUND:	25.5' (AT MAXIMUM OPERATING TEMPERATURE)

**NOTE:**

1. INFORMATION CONTAINED ON DRAWING IS PRELIMINARY IN NATURE AND SUBJECT TO CHANGE DURING FINAL DESIGN.
2. MINIMUM FOUNDATION REVEAL SHALL BE 1.5'
3. FINAL FOUNDATION DIAMETER SHALL BE BASED UPON FINAL ENGINEERING.
4. STRUCTURE HEIGHTS ARE MEASURED FROM THE STRUCTURE CENTERLINE.

**230KV LINE #2297 AQUIA HARBOUR - POSSUM POINT  
230KV LINE #252 FULLER ROAD - POSSUM POINT**



**DOUBLE CIRCUIT SUSPENSION MONOPOLE STRUCTURE**

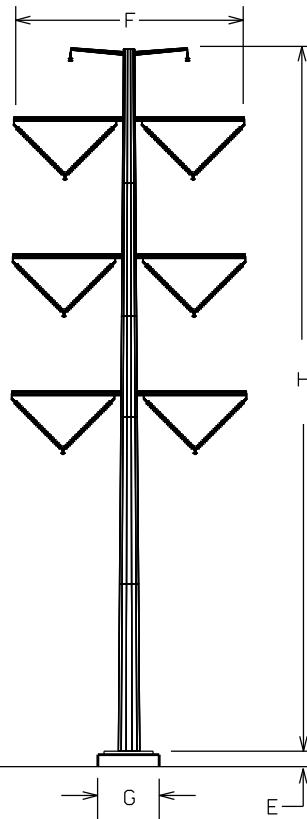
A. MAPPING OF THE ROUTE:	SEE ATTACHMENT II.B.5
B. RATIONALE FOR STRUCTURE TYPE:	ACCOMODATES EFFICIENT USE R/W AND REDUCES BLOWOUT FOOTPRINT
C. LENGTH OF R/W (STRUCTURE QTY):	0.36 MILES (2)
D. STRUCTURE MATERIAL: RATIONAL FOR MATERIAL:	WEATHERING STEEL WEATHERING STEEL WAS SELECTED FOR ITS CORROSION RESISTANCE, ENVIRONMENTAL SUSTAINABILITY DUE TO LOW MAINTENANCE, AESTHETIC APPEAL, LOW COST AND LONGEVITY.
E. FOUNDATION MATERIAL: AVERAGE FOUNDATION REVEAL:	CONCRETE SEE NOTE 2
F. AVERAGE WIDTH AT CROSS ARM:	24'
G. AVERAGE WIDTH AT BASE:	6' DIAMETER FOUNDATION (SEE NOTE 3)
H. MINIMUM STRUCTURE HEIGHT: MAXIMUM STRUCTURE HEIGHT: AVERAGE STRUCTURE HEIGHT:	140' 140' 140'
I. AVERAGE SPAN LENGTH (RANGE):	950' (896' - 1003') (WIND SPAN)
J. MINIMUM CONDUCTOR-TO-GROUND:	25.5' (AT MAXIMUM OPERATING TEMPERATURE)

**NOTE:**

1. INFORMATION CONTAINED ON DRAWING IS PRELIMINARY IN NATURE AND SUBJECT TO CHANGE DURING FINAL DESIGN.
2. MINIMUM FOUNDATION REVEAL SHALL BE 1.5'
3. FINAL FOUNDATION DIAMETER SHALL BE BASED UPON FINAL ENGINEERING.
4. STRUCTURE HEIGHTS ARE MEASURED FROM THE STRUCTURE CENTERLINE.



**230KV LINE #2297 AQUIA HARBOUR - POSSUM POINT**  
**230KV LINE #2309 AQUIA HARBOUR - FULLER ROAD**  
**230KV LINE #252 FULLER ROAD - POSSUM POINT**



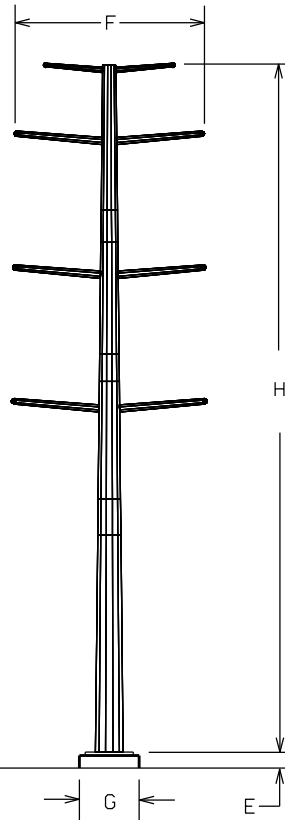
**DOUBLE CIRCUIT SUSPENSION MONOPOLE STRUCTURE**

A. MAPPING OF THE ROUTE:	SEE ATTACHMENT II.B.5
B. RATIONALE FOR STRUCTURE TYPE:	ACCOMMODATES EFFICIENT USE OF R/W AND REDUCES BLOWOUT FOOTPRINT.
C. LENGTH OF R/W (STRUCTURE QTY):	17.93 MILES (147)
D. STRUCTURE MATERIAL: RATIONAL FOR MATERIAL:	WEATHERING STEEL & GALVANIZED STEEL WEATHERING STEEL WAS SELECTED FOR ITS CORROSION RESISTANCE, ENVIRONMENTAL SUSTAINABILITY DUE TO LOW MAINTENANCE, AESTHETIC APPEAL, LOW COST AND LONGEVITY. GALVANIZED STEEL WAS SELECTED FOR STRUCTURES REQUIRING THE INSTALLATION OF ANTENNAS
E. FOUNDATION MATERIAL: AVERAGE FOUNDATION REVEAL:	CONCRETE SEE NOTE 2
F. AVERAGE WIDTH AT CROSS ARM:	35'
G. AVERAGE WIDTH AT BASE:	6' DIAMETER FOUNDATION (SEE NOTE 3)
H. MINIMUM STRUCTURE HEIGHT: MAXIMUM STRUCTURE HEIGHT: AVERAGE STRUCTURE HEIGHT:	100' 165' 125'
I. AVERAGE SPAN LENGTH (RANGE):	644' (407' - 985') (WIND SPAN)
J. MINIMUM CONDUCTOR-TO-GROUND:	25.5' (AT MAXIMUM OPERATING TEMPERATURE)

**NOTE:**

1. INFORMATION CONTAINED ON DRAWING IS PRELIMINARY IN NATURE AND SUBJECT TO CHANGE DURING FINAL DESIGN.
2. MINIMUM FOUNDATION REVEAL SHALL BE 1.5'
3. FINAL FOUNDATION DIAMETER SHALL BE BASED UPON FINAL ENGINEERING.
4. STRUCTURE HEIGHTS ARE MEASURED FROM THE STRUCTURE CENTERLINE.

**230KV LINE #2297 AQUIA HARBOUR - POSSUM POINT  
230KV LINE #2309 AQUIA HARBOUR - FULLER ROAD  
230KV LINE #252 FULLER ROAD - POSSUM POINT**



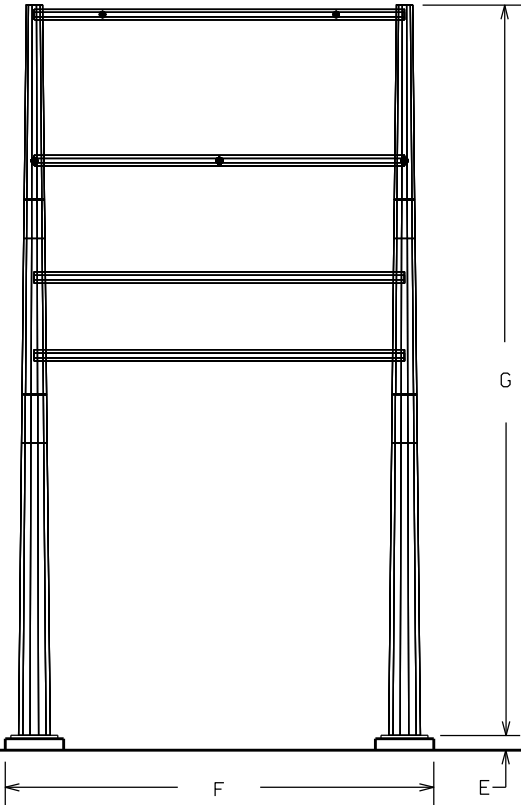
**DOUBLE CIRCUIT DEADEND MONOPOLE STRUCTURE**

A. MAPPING OF THE ROUTE:	SEE ATTACHMENT II.B.5
B. RATIONALE FOR STRUCTURE TYPE:	ACCOMODATES EFFICIENT USE R/W AND REDUCES BLOWOUT FOOTPRINT
C. LENGTH OF R/W (STRUCTURE QTY):	4.28 MILES (43)
D. STRUCTURE MATERIAL: RATIONAL FOR MATERIAL:	WEATHERING STEEL WEATHERING STEEL WAS SELECTED FOR ITS CORROSION RESISTANCE, ENVIRONMENTAL SUSTAINABILITY DUE TO LOW MAINTENANCE, AESTHETIC APPEAL, LOW COST AND LONGEVITY.
E. FOUNDATION MATERIAL: AVERAGE FOUNDATION REVEAL:	CONCRETE SEE NOTE 2
F. AVERAGE WIDTH AT CROSS ARM:	27' - 32'
G. AVERAGE WIDTH AT BASE:	6' DIAMETER FOUNDATION (SEE NOTE 3)
H. MINIMUM STRUCTURE HEIGHT: MAXIMUM STRUCTURE HEIGHT: AVERAGE STRUCTURE HEIGHT:	90' 185' 118'
I. AVERAGE SPAN LENGTH (RANGE):	524' (285' - 721') (WIND SPAN)
J. MINIMUM CONDUCTOR-TO-GROUND:	25.5' (AT MAXIMUM OPERATING TEMPERATURE)

**NOTE:**

1. INFORMATION CONTAINED ON DRAWING IS PRELIMINARY IN NATURE AND SUBJECT TO CHANGE DURING FINAL DESIGN.
2. MINIMUM FOUNDATION REVEAL SHALL BE 1.5'
3. FINAL FOUNDATION DIAMETER SHALL BE BASED UPON FINAL ENGINEERING.
4. STRUCTURE HEIGHTS ARE MEASURED FROM THE STRUCTURE CENTERLINE.

230KV LINE #2297 AQUIA HARBOUR - POSSUM POINT

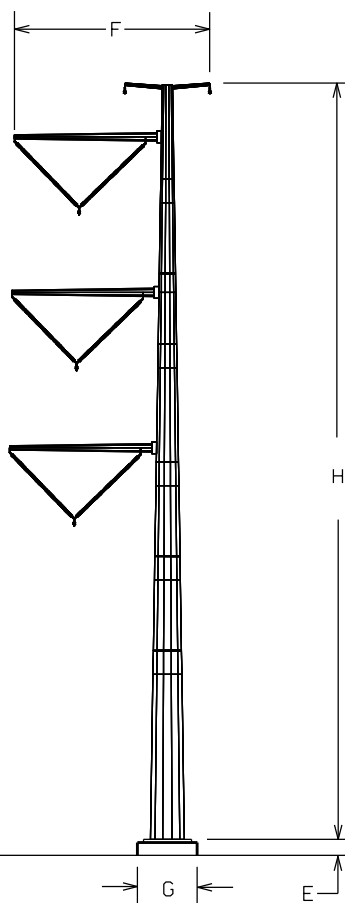


SINGLE CIRCUIT BACKBONE STRUCTURE

A. MAPPING OF THE ROUTE:	SEE ATTACHMENT II.B.5
B. RATIONALE FOR STRUCTURE TYPE:	MAINTAINS FLAT CONFIGURATION AT THE SUBSTATION INTERFACE
C. LENGTH OF R/W (STRUCTURE QTY):	0.02 MILES (1)
D. STRUCTURE MATERIAL: RATIONAL FOR MATERIAL:	GALVANIZED STEEL GALVANIZED STEEL WAS SELECTED TO MATCH EXISTING GALVANIZED STRUCTURES INSIDE SUBSTATIONS.
E. FOUNDATION MATERIAL: AVERAGE FOUNDATION REVEAL:	CONCRETE SEE NOTE 2
F. AVERAGE WIDTH AT BASE:	46', 6' DIAMETER FOUNDATION (SEE NOTE 3)
G. MINIMUM STRUCTURE HEIGHT: MAXIMUM STRUCTURE HEIGHT: AVERAGE STRUCTURE HEIGHT:	75' 75' 75'
H. AVERAGE SPAN LENGTH (RANGE):	110' (WIND SPAN)
I. MINIMUM CONDUCTOR-TO-GROUND:	25.5' (AT MAXIMUM OPERATING TEMPERATURE)

NOTE:

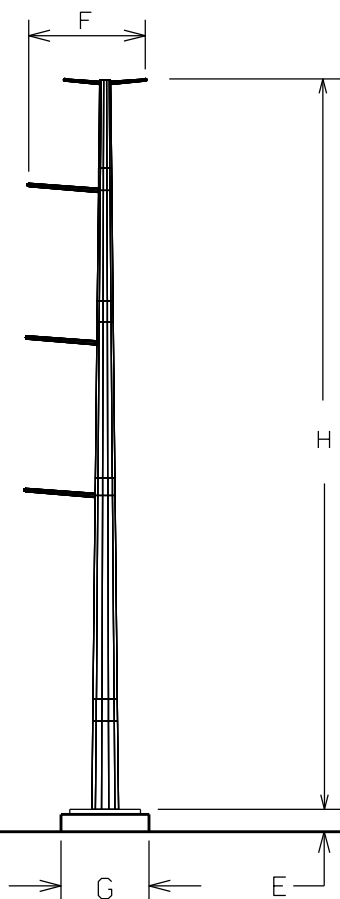
1. INFORMATION CONTAINED ON DRAWING IS PRELIMINARY IN NATURE AND SUBJECT TO CHANGE DURING FINAL DESIGN.
2. MINIMUM FOUNDATION REVEAL SHALL BE 1.5'
3. FINAL FOUNDATION DIAMETER SHALL BE BASED UPON FINAL ENGINEERING.
4. STRUCTURE HEIGHTS ARE MEASURED FROM THE STRUCTURE CENTERLINE.

**500KV LINE #568 POSSUM POINT - LADYSMITH****SINGLE CIRCUIT SUSPENSION MONOPOLE STRUCTURE**

A. MAPPING OF THE ROUTE:	SEE ATTACHMENT II.B.5
B. RATIONALE FOR STRUCTURE TYPE:	ACCOMODATES EFFICIENT USE R/W AND REDUCES BLOWOUT FOOTPRINT
C. LENGTH OF R/W (STRUCTURE QTY):	5.2 MILES (30)
D. STRUCTURE MATERIAL: RATIONAL FOR MATERIAL:	WEATHERING STEEL WEATHERING STEEL WAS SELECTED FOR ITS CORROSION RESISTANCE, ENVIRONMENTAL SUSTAINABILITY DUE TO LOW MAINTENANCE, AESTHETIC APPEAL, LOW COST AND LONGEVITY.
E. FOUNDATION MATERIAL: AVERAGE FOUNDATION REVEAL:	CONCRETE SEE NOTE 2
F. AVERAGE WIDTH AT CROSS ARM:	42'
G. AVERAGE WIDTH AT BASE:	6' DIAMETER FOUNDATION (SEE NOTE 3)
H. MINIMUM STRUCTURE HEIGHT: MAXIMUM STRUCTURE HEIGHT: AVERAGE STRUCTURE HEIGHT:	160' 195' 179'
I. AVERAGE SPAN LENGTH (RANGE):	915' (685' - 1,214') (WIND SPAN)
J. MINIMUM CONDUCTOR-TO-GROUND:	30.9' (AT MAXIMUM OPERATING TEMPERATURE)

**NOTE:**

1. INFORMATION CONTAINED ON DRAWING IS PRELIMINARY IN NATURE AND SUBJECT TO CHANGE DURING FINAL DESIGN.
2. MINIMUM FOUNDATION REVEAL SHALL BE 1.5'
3. FINAL FOUNDATION DIAMETER SHALL BE BASED UPON FINAL ENGINEERING.
4. STRUCTURE HEIGHTS ARE MEASURED FROM THE STRUCTURE CENTERLINE.

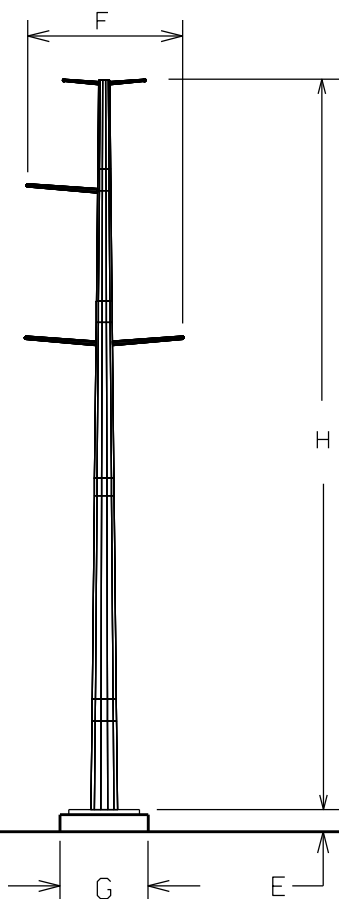
**500KV LINE #568 POSSUM POINT - LADYSMITH****SINGLE CIRCUIT DEADEND MONOPOLE STRUCTURE**

A. MAPPING OF THE ROUTE:	SEE ATTACHMENT II.B.5
B. RATIONALE FOR STRUCTURE TYPE:	ACCOMMODATES EFFICIENT USE OF R/W AND REDUCES BLOWOUT FOOTPRINT.
C. LENGTH OF R/W (STRUCTURE QTY):	0.6 MILES (7)
D. STRUCTURE MATERIAL: RATIONAL FOR MATERIAL:	WEATHERING STEEL WEATHERING STEEL WAS SELECTED FOR ITS CORROSION RESISTANCE, ENVIRONMENTAL SUSTAINABILITY DUE TO LOW MAINTENANCE, AESTHETIC APPEAL, LOW COST AND LONGEVITY.
E. FOUNDATION MATERIAL: AVERAGE FOUNDATION REVEAL:	CONCRETE SEE NOTE 2
F. AVERAGE WIDTH AT CROSS ARM:	28'
G. AVERAGE WIDTH AT BASE:	6' DIAMETER FOUNDATION (SEE NOTE 3)
H. MINIMUM STRUCTURE HEIGHT: MAXIMUM STRUCTURE HEIGHT: AVERAGE STRUCTURE HEIGHT:	160' 185' 175'
I. AVERAGE SPAN LENGTH (RANGE):	454' (297' - 560') (WIND SPAN)
J. MINIMUM CONDUCTOR-TO-GROUND:	30.9' (AT MAXIMUM OPERATING TEMPERATURE)

**NOTE:**

1. INFORMATION CONTAINED ON DRAWING IS PRELIMINARY IN NATURE AND SUBJECT TO CHANGE DURING FINAL DESIGN.
2. MINIMUM FOUNDATION REVEAL SHALL BE 1.5'
3. FINAL FOUNDATION DIAMETER SHALL BE BASED UPON FINAL ENGINEERING.
4. STRUCTURE HEIGHTS ARE MEASURED FROM THE STRUCTURE CENTERLINE.

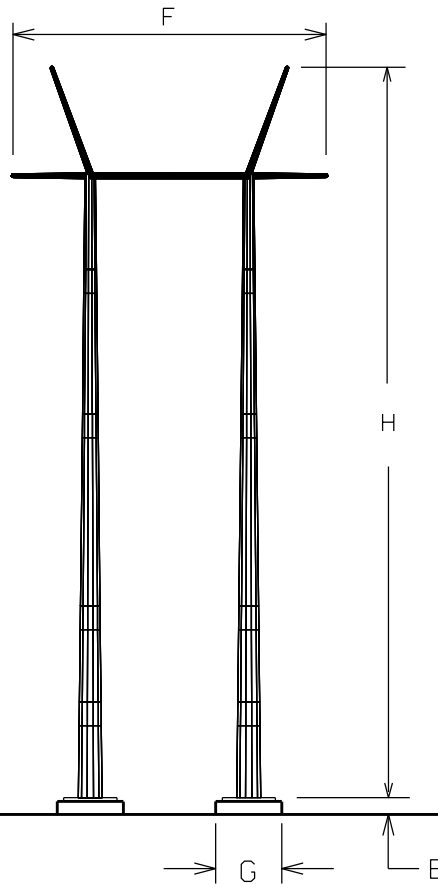


**500KV LINE #568 POSSUM POINT - LADYSMITH****SINGLE CIRCUIT DEADEND MONOPOLE STRUCTURE**

A. MAPPING OF THE ROUTE:	SEE ATTACHMENT II.B.5
B. RATIONALE FOR STRUCTURE TYPE:	ACCOMMODATES EFFICIENT USE OF R/W AND REDUCES BLOWOUT FOOTPRINT.
C. LENGTH OF R/W (STRUCTURE QTY):	0.16 MILES (1)
D. STRUCTURE MATERIAL: RATIONAL FOR MATERIAL:	WEATHERING STEEL WEATHERING STEEL WAS SELECTED FOR ITS CORROSION RESISTANCE, ENVIRONMENTAL SUSTAINABILITY DUE TO LOW MAINTENANCE, AESTHETIC APPEAL, LOW COST AND LONGEVITY.
E. FOUNDATION MATERIAL: AVERAGE FOUNDATION REVEAL:	CONCRETE SEE NOTE 2
F. AVERAGE WIDTH AT CROSS ARM:	38'
G. AVERAGE WIDTH AT BASE:	6' DIAMETER FOUNDATION (SEE NOTE 3)
H. MINIMUM STRUCTURE HEIGHT: MAXIMUM STRUCTURE HEIGHT: AVERAGE STRUCTURE HEIGHT:	180' 180' 180'
I. AVERAGE SPAN LENGTH (RANGE):	855' (WIND SPAN)
J. MINIMUM CONDUCTOR-TO-GROUND:	30.9' (AT MAXIMUM OPERATING TEMPERATURE)

**NOTE:**

1. INFORMATION CONTAINED ON DRAWING IS PRELIMINARY IN NATURE AND SUBJECT TO CHANGE DURING FINAL DESIGN.
2. MINIMUM FOUNDATION REVEAL SHALL BE 1.5'
3. FINAL FOUNDATION DIAMETER SHALL BE BASED UPON FINAL ENGINEERING.
4. STRUCTURE HEIGHTS ARE MEASURED FROM THE STRUCTURE CENTERLINE.

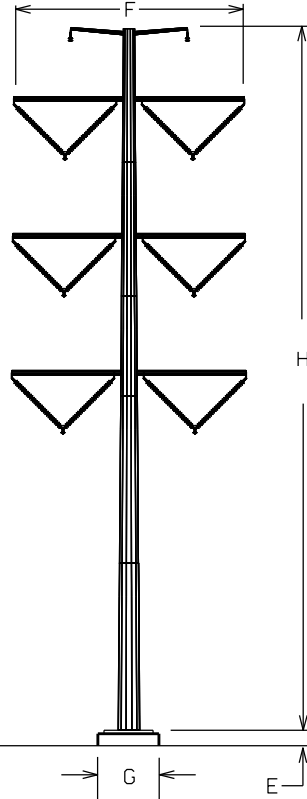
**500KV LINE #568 POSSUM POINT - LADYSMITH****SINGLE CIRCUIT DEADEND H-FRAME STRUCTURE**

A. MAPPING OF THE ROUTE:	SEE ATTACHMENT II.B.5
B. RATIONALE FOR STRUCTURE TYPE:	FACILITATES PHASE ROLL FROM VERTICAL TO FLAT AT THE INTERFACE WITH EXISTING CONDUCTOR
C. LENGTH OF R/W (STRUCTURE QTY):	0.13 MILES (2)
D. STRUCTURE MATERIAL: RATIONAL FOR MATERIAL:	WEATHERING STEEL WEATHERING STEEL WAS SELECTED FOR ITS CORROSION RESISTANCE, ENVIRONMENTAL SUSTAINABILITY DUE TO LOW MAINTENANCE, AESTHETIC APPEAL, LOW COST AND LONGEVITY.
E. FOUNDATION MATERIAL: AVERAGE FOUNDATION REVEAL:	CONCRETE SEE NOTE 2
F. AVERAGE WIDTH AT CROSS ARM:	66'
G. AVERAGE WIDTH AT BASE:	6' DIAMETER FOUNDATION (SEE NOTE 3)
H. MINIMUM STRUCTURE HEIGHT: MAXIMUM STRUCTURE HEIGHT: AVERAGE STRUCTURE HEIGHT:	125' 150' 137'
I. AVERAGE SPAN LENGTH (RANGE):	351' (320' - 381') (WIND SPAN)
J. MINIMUM CONDUCTOR-TO-GROUND:	30.9' (AT MAXIMUM OPERATING TEMPERATURE)

**NOTE:**

1. INFORMATION CONTAINED ON DRAWING IS PRELIMINARY IN NATURE AND SUBJECT TO CHANGE DURING FINAL DESIGN.
2. MINIMUM FOUNDATION REVEAL SHALL BE 1.5'
3. FINAL FOUNDATION DIAMETER SHALL BE BASED UPON FINAL ENGINEERING.
4. STRUCTURE HEIGHTS ARE MEASURED FROM THE STRUCTURE CENTERLINE.

230KV LINE #2157 FREDERICKSBURG - CRANES CORNER  
 230KV LINE #2305 FREDERICKSBURG - AQUIA HARBOUR  
 230KV LINE #2104 CRANES CORNER - SPARTAN  
 230KV LINE #2297 SPARTAN - AQUIA HARBOUR  
 230KV LINE #2083 & #2ZZZ FREDERICKSBURG - BIRCHWOOD  
 230KV LINE #2XXX & #2YYY FREDERICKSBURG - AQUIA HARBOUR



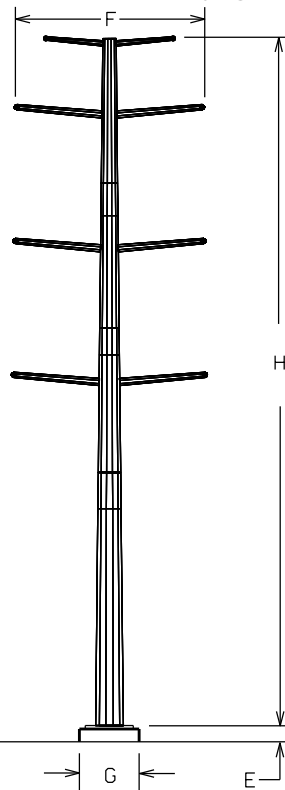
### DOUBLE CIRCUIT SUSPENSION MONOPOLE STRUCTURE

A. MAPPING OF THE ROUTE:	SEE ATTACHMENT II.B.5
B. RATIONALE FOR STRUCTURE TYPE:	ACCOMMODATES EFFICIENT USE OF R/W AND REDUCES BLOWOUT FOOTPRINT.
C. LENGTH OF R/W (STRUCTURE QTY):	12.5 MILES (151)
D. STRUCTURE MATERIAL: RATIONAL FOR MATERIAL:	WEATHERING STEEL WEATHERING STEEL WAS SELECTED FOR ITS CORROSION RESISTANCE, ENVIRONMENTAL SUSTAINABILITY DUE TO LOW MAINTENANCE, AESTHETIC APPEAL, LOW COST AND LONGEVITY.
E. FOUNDATION MATERIAL: AVERAGE FOUNDATION REVEAL:	CONCRETE SEE NOTE 2
F. AVERAGE WIDTH AT CROSS ARM:	36'
G. AVERAGE WIDTH AT BASE:	6' DIAMETER FOUNDATION (SEE NOTE 3)
H. MINIMUM STRUCTURE HEIGHT: MAXIMUM STRUCTURE HEIGHT: AVERAGE STRUCTURE HEIGHT:	100' 120' 108.75'
I. AVERAGE SPAN LENGTH (RANGE):	448' (340' -524') (WIND SPAN)
J. MINIMUM CONDUCTOR-TO-GROUND:	25.5' (AT MAXIMUM OPERATING TEMPERATURE)

#### NOTE:

1. INFORMATION CONTAINED ON DRAWING IS PRELIMINARY IN NATURE AND SUBJECT TO CHANGE DURING FINAL DESIGN.
2. MINIMUM FOUNDATION REVEAL SHALL BE 1.5'
3. FINAL FOUNDATION DIAMETER SHALL BE BASED UPON FINAL ENGINEERING.
4. STRUCTURE HEIGHTS ARE MEASURED FROM THE STRUCTURE CENTERLINE.

230KV LINE #2157 FREDERICKSBURG - CRANES CORNER  
 230KV LINE #2305 FREDERICKSBURG - AQUIA HARBOUR  
 230KV LINE #2104 CRANES CORNER - SPARTAN  
 230KV LINE #2297 SPARTAN - AQUIA HARBOUR  
 230KV LINE #2083 & #2ZZZ FREDERICKSBURG - BIRCHWOOD  
 230KV LINE #2XXX & #2YYY FREDERICKSBURG - AQUIA HARBOUR



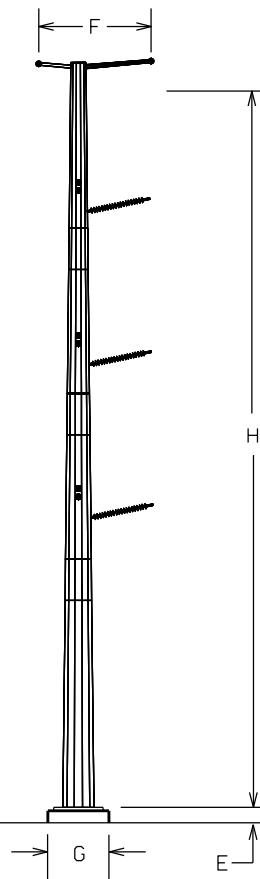
### DOUBLE CIRCUIT DEADEND MONOPOLE STRUCTURE

A. MAPPING OF THE ROUTE:	SEE ATTACHMENT II.B.5
B. RATIONALE FOR STRUCTURE TYPE:	ACCOMODATES EFFICIENT USE R/W AND REDUCES BLOWOUT FOOTPRINT
C. LENGTH OF R/W (STRUCTURE QTY):	12.5 MILES (50)
D. STRUCTURE MATERIAL: RATIONAL FOR MATERIAL:	WEATHERING STEEL WEATHERING STEEL WAS SELECTED FOR ITS CORROSION RESISTANCE, ENVIRONMENTAL SUSTAINABILITY DUE TO LOW MAINTENANCE, AESTHETIC APPEAL, LOW COST AND LONGEVITY.
E. FOUNDATION MATERIAL: AVERAGE FOUNDATION REVEAL:	CONCRETE SEE NOTE 2
F. AVERAGE WIDTH AT CROSS ARM:	27'
G. AVERAGE WIDTH AT BASE:	6' DIAMETER FOUNDATION (SEE NOTE 3)
H. MINIMUM STRUCTURE HEIGHT: MAXIMUM STRUCTURE HEIGHT: AVERAGE STRUCTURE HEIGHT:	100' 115' 112'
I. AVERAGE SPAN LENGTH (RANGE):	156' (64' - 305') (WIND SPAN)
J. MINIMUM CONDUCTOR-TO-GROUND:	25.5' (AT MAXIMUM OPERATING TEMPERATURE)

#### NOTE:

1. INFORMATION CONTAINED ON DRAWING IS PRELIMINARY IN NATURE AND SUBJECT TO CHANGE DURING FINAL DESIGN.
2. MINIMUM FOUNDATION REVEAL SHALL BE 1.5'
3. FINAL FOUNDATION DIAMETER SHALL BE BASED UPON FINAL ENGINEERING.
4. STRUCTURE HEIGHTS ARE MEASURED FROM THE STRUCTURE CENTERLINE.

**230KV LINE #2083 FREDERICKSBURG - BIRCHWOOD  
230KV LINE #2YYY FREDERICKSBURG - AQUIA HARBOUR**



**SINGLE CIRCUIT DEADEND MONOPOLE STRUCTURE**

A. MAPPING OF THE ROUTE:	SEE ATTACHMENT II.B.5
B. RATIONALE FOR STRUCTURE TYPE:	ACCOMMODATES EFFICIENT USE OF R/W AND REDUCES BLOWOUT FOOTPRINT.
C. LENGTH OF R/W (STRUCTURE QTY):	12.5 MILES (4)
D. STRUCTURE MATERIAL: RATIONAL FOR MATERIAL:	WEATHERING STEEL WEATHERING STEEL WAS SELECTED FOR ITS CORROSION RESISTANCE, ENVIRONMENTAL SUSTAINABILITY DUE TO LOW MAINTENANCE, AESTHETIC APPEAL, LOW COST AND LONGEVITY.
E. FOUNDATION MATERIAL: AVERAGE FOUNDATION REVEAL:	CONCRETE SEE NOTE 2
F. AVERAGE WIDTH AT CROSS ARM:	13'
G. AVERAGE WIDTH AT BASE:	6' DIAMETER FOUNDATION (SEE NOTE 3)
H. MINIMUM STRUCTURE HEIGHT: MAXIMUM STRUCTURE HEIGHT: AVERAGE STRUCTURE HEIGHT:	115' 115' 115'
I. AVERAGE SPAN LENGTH (RANGE):	99' (47' - 163') (WIND SPAN)
J. MINIMUM CONDUCTOR-TO-GROUND:	25.5' (AT MAXIMUM OPERATING TEMPERATURE)

**NOTE:**

1. INFORMATION CONTAINED ON DRAWING IS PRELIMINARY IN NATURE AND SUBJECT TO CHANGE DURING FINAL DESIGN.
2. MINIMUM FOUNDATION REVEAL SHALL BE 1.5'
3. FINAL FOUNDATION DIAMETER SHALL BE BASED UPON FINAL ENGINEERING.
4. STRUCTURE HEIGHTS ARE MEASURED FROM THE STRUCTURE CENTERLINE.



**II. DESCRIPTION OF THE PROPOSED PROJECT**

**B. Line Design and Operational Features**

- 4. With regard to the proposed supporting structures for all feasible alternate routes, provide the maximum, minimum and average structure heights with respect to the whole route.**

Response: Not applicable.

## II. DESCRIPTION OF THE PROPOSED PROJECT

### B. Line Design and Operational Features

5. For lines being rebuilt, provide mapping showing existing and proposed structure heights for each individual structure within the ROW, as proposed in the application.

Response: See Attachment II.B.5 for existing and proposed structure locations.

The proposed approximate structure heights are from the conceptual design created to estimate the cost of the proposed Rebuild Project and are subject to change based on final engineering design. The approximate structure heights do not include foundation reveal and assume equal leg lengths based on the centerline ground elevation. The following table provides a breakdown of existing and proposed structure heights, generally grouped by segment.

Existing Structure Number Ckt. 1	Existing Structure Number Ckt. 2	Existing Structure Height (ft.)	Proposed Structure Number Ckt. 1	Proposed Structure Number Ckt. 2	Proposed Structure Height (ft)	Attachment II.B.3 Structure Type
252/5517	29/1784	95	2309/5517	2297/1784	*	II.B.3.c
252/5518	29/1785	107.5	2309/5518	2297/1785	100	II.B.3.a
252/5519	29/1786	106	2309/5519	2297/1786	120	II.B.3.f
252/5520	29/1787	126	2309/5520	2297/1787	125	II.B.3.f
-	-	-	2309/5520A	2297/1787A	120	II.B.3.f
252/5521	29/1788	117	2309/5521	2297/1788	95	II.B.3.g
-	-	-	2309/5521A	2297/1788A	120	II.B.3.f
252/5522	29/1789	131	2309/5522	2297/1789	130	II.B.3.f
252/5523	29/1790	144.5	2309/5523	2297/1790	125	II.B.3.f
-	-	-	2309/5523A	2297/1790A	125	II.B.3.f
252/5524	29/1791	105.5	2309/5524	2297/1791	100	II.B.3.f
-	-	-	2309/5524A	2297/1791A	125	II.B.3.f
252/5525	29/1792	142	2309/5525	2297/1792	155	II.B.3.f
252/5526	29/1793	110.5	2309/5526	2297/1793	135	II.B.3.f
252/5527	29/1794	107.5	2309/5527	2297/1794	145	II.B.3.f
252/5528	29/1795	106	2309/5528	2297/1795	120	II.B.3.f
-	-	-	2309/5528A	2297/1795A	120	II.B.3.g
252/5529	29/1796	106	2309/5529	2297/1796	100	II.B.3.f
-	-	-	2309/5529A	2297/1796A	135	II.B.3.f
252/5530	29/1797	127	2309/5530	2297/1797	105	II.B.3.f
-	-	-	2309/5530A	2297/1797A	120	II.B.3.f
252/5531	29/1792	142	2309/5531	2297/1798	140	II.B.3.f

Existing Structure Number Ckt. 1	Existing Structure Number Ckt. 2	Existing Structure Height (ft.)	Proposed Structure Number Ckt. 1	Proposed Structure Number Ckt. 2	Proposed Structure Height (ft)	Attachment II.B.3 Structure Type
-	-	-	2309/5531A	2297/1798A	130	II.B.3.f
252/5532	29/1799	117	2309/5532	2297/1799	110	II.B.3.f
-	-	-	2309/5532A	2297/1799A	125	II.B.3.f
252/5533	29/1800	124.5	2309/5533	2297/1800	110	II.B.3.f
252/5534	29/1801	106.5	2309/5534	2297/1801	115	II.B.3.g
-	-	-	2309/5534A	2297/1801A	120	II.B.3.f
252/5535	29/1802	133	2309/5535	2297/1802	135	II.B.3.f
252/5536	29/1803	112	2309/5536	2297/1803	130	II.B.3.f
-	-	-	2309/5536A	2297/1803A	135	II.B.3.f
252/5537	29/1804	106.5	2309/5537	2297/1804	110	II.B.3.f
-	-	-	2309/5537A	2297/1804A	120	II.B.3.g
252/5537A	-	70	2309/5537B	-	*	-
-	-	-	2297/1804B	-	145	II.B.3.d
-	-	-	2297/1804D	-	125	II.B.3.d
252/5538	29/1805	117	2309/5538	2297/1805	120	II.B.3.g
252/5539	29/1806	111.5	2309/5539	2297/1806	140	II.B.3.f
252/5540	29/1807	107.5	2309/5540	2297/1807	105	II.B.3.f
252/5541	29/1808	109	2309/5541	2297/1808	120	II.B.3.f
252/5542	29/1809	112.5	2309/5542	2297/1809	115	II.B.3.f
252/5543	29/1810	121.5	2309/5543	2297/1810	105	II.B.3.f
-	-	-	2309/5543A	2297/1810A	125	II.B.3.f
252/5544	29/1811	131.5	2309/5544	2297/1811	125	II.B.3.f
252/5545	29/1812	111	2309/5545	2297/1812	130	II.B.3.f
252/5546	29/1813	111	2309/5546	2297/1813	140	II.B.3.f
-	-	-	2309/5546A	2297/1813A	160	II.B.3.f
252/5547	29/1814	108	2309/5547	2297/1814	135	II.B.3.f
252/5548	29/1815	111.5	2309/5548	2297/1815	135	II.B.3.f
-	-	-	2309/5548A	2297/1815A	130	II.B.3.f
252/5549	29/1816	106.5	2309/5549	2297/1816	100	II.B.3.g
-	-	-	2309/5549A	2297/1816A	130	II.B.3.f
252/5550	29/1817	137	2309/5550	2297/1817	155	II.B.3.f
252/5551	29/1818	165	2309/5551	2297/1818	165	II.B.3.f
252/5552	29/1819	136.5	2309/5552	2297/1819	125	II.B.3.g
-	-	-	2309/5552A	2297/1819A	145	II.B.3.f
252/5553	29/1820	111	2309/5553	2297/1820	110	II.B.3.f
252/5554	29/1821	113.5	2309/5554	2297/1821	120	II.B.3.f

Existing Structure Number Ckt. 1	Existing Structure Number Ckt. 2	Existing Structure Height (ft.)	Proposed Structure Number Ckt. 1	Proposed Structure Number Ckt. 2	Proposed Structure Height (ft)	Attachment II.B.3 Structure Type
-	-	-	2309/5554A	2297/1821A	125	II.B.3.f
252/5555	29/1822	110	2309/5555	2297/1822	100	II.B.3.g
252/5556	29/1823	73.5	2309/5556	2297/1823	90	II.B.3.b
-	-	-	2309/5556A	2297/1823A	95	II.B.3.g
252/5557	29/1824	122	2309/5557	2297/1824	110	II.B.3.f
252/5558	29/1825	112.5	2309/5558	2297/1825	95	II.B.3.g
252/5559	29/1826	142	2309/5559	2297/1826	115	II.B.3.f
-	-	-	2309/5559A	2297/1826A	135	II.B.3.f
252/5560	29/1827	144	2309/5560	2297/1827	110	II.B.3.g
-	-	-	2309/5560A	2297/1827A	140	II.B.3.f
252/5561	29/1828	141.5	2309/5561	2297/1828	140	II.B.3.f
252/5562	29/1829	108.5	2309/5562	2297/1829	120	II.B.3.f
252/5563	29/1830	106.5	2309/5563	2297/1830	125	II.B.3.f
252/5564	29/1831	106.5	2309/5564	2297/1831	120	II.B.3.f
252/5565	29/1832	112.5	2309/5565	2297/1832	105	II.B.3.f
-	-	-	2309/5565A	2297/1832A	140	II.B.3.f
-	-	-	2309/5565B	2297/1832B	125	II.B.3.g
252/5566	29/1833	129	2309/5566	2297/1833	145	II.B.3.g
252/5566A	-	76.5	2309/5566A	2297/1833A	95	II.B.3.c
252/5567	29/1834	110.5	252/5567	2297/1834	185	II.B.3.g
252/5568	29/1835	106.5	252/5568	2297/1835	115	II.B.3.b
252/5569	29/1836	111	252/5569	2297/1836	90	II.B.3.g
-	-	-	252/5569A	2297/1836A	125	II.B.3.f
252/5570	29/1837	111.5	252/5570	2297/1837	115	II.B.3.f
252/5571	29/1838	109.5	252/5571	2297/1838	110	II.B.3.f
-	-	-	252/5571A	2297/1838A	145	II.B.3.f
252/5572	29/1839	109	252/5572	2297/1839	110	II.B.3.f
252/5573	29/1840	106.5	252/5573	2297/1840	100	II.B.3.f
-	-	-	252/5573A	2297/1840A	140	II.B.3.f
252/5574	29/1841	107	252/5574	2297/1841	120	II.B.3.f
252/5575	29/1842	119	252/5575	2297/1842	125	II.B.3.g
-	-	-	252/5575A	2297/1842A	100	II.B.3.f
252/5576	29/1843	146	252/5576	2297/1843	105	II.B.3.f
252/5577	29/1844	106.5	252/5577	2297/1844	115	II.B.3.g
-	-	-	252/5577A	2297/1844A	115	II.B.3.g
252/5578	29/1845	141.5	252/5578	2297/1845	140	II.B.3.e

Existing Structure Number Ckt. 1	Existing Structure Number Ckt. 2	Existing Structure Height (ft.)	Proposed Structure Number Ckt. 1	Proposed Structure Number Ckt. 2	Proposed Structure Height (ft)	Attachment II.B.3 Structure Type
252/5579	29/1846	141.5	252/5579	2297/1846	140	II.B.3.e
252/5580	29/1847	116.5	252/5580	2297/1847	125	II.B.3.b
252/5581	29/1848	146.5	252/5581	2297/1848	120	II.B.3.f
-	-	-	252/5581A	2297/1848A	125	II.B.3.f
252/5582	29/1849	143.5	252/5582	2297/1849	120	II.B.3.f
252/5583	29/1850	116.5	252/5583	2297/1850	105	II.B.3.g
252/5584	-	73.5	252/5584	2297/1851	155	II.B.3.f
252/5585	-	80	252/5585	2297/1852	155	II.B.3.f
252/5587	-	74	252/5586	2297/1853	120	II.B.3.g
252/5588	-	121	252/5587	-	95	II.B.3.d
-	2078/10	-	252/5588	2078/10	*	-
-	-	-	2XXX/115	2YYY/118	100	II.B.3.a
-	-	-	2XXX/116	2YYY/119	120	II.B.3.f
-	-	-	2XXX/117	2YYY/120	125	II.B.3.f
-	-	-	2XXX/118	2YYY/121	120	II.B.3.f
-	-	-	2XXX/119	2YYY/122	100	II.B.3.g
-	-	-	2XXX/120	2YYY/123	125	II.B.3.f
-	-	-	2XXX/121	2YYY/124	130	II.B.3.f
-	-	-	2XXX/122	2YYY/125	125	II.B.3.f
-	-	-	2XXX/123	2YYY/126	125	II.B.3.f
-	-	-	2XXX/124	2YYY/127	115	II.B.3.f
-	-	-	2XXX/125	2YYY/128	125	II.B.3.f
-	-	-	2XXX/126	2YYY/129	155	II.B.3.f
-	-	-	2XXX/127	2YYY/130	135	II.B.3.f
-	-	-	2XXX/128	2YYY/131	135	II.B.3.f
-	-	-	2XXX/129	2YYY/132	120	II.B.3.f
-	-	-	2XXX/130	2YYY/133	125	II.B.3.g
-	-	-	2XXX/131	2YYY/134	100	II.B.3.f
-	-	-	2XXX/132	2YYY/135	135	II.B.3.f
-	-	-	2XXX/133	2YYY/136	105	II.B.3.f
-	-	-	2XXX/134	2YYY/137	125	II.B.3.f
-	-	-	2XXX/135	2YYY/138	140	II.B.3.f
-	-	-	2XXX/136	2YYY/139	130	II.B.3.f
-	-	-	2XXX/137	2YYY/140	115	II.B.3.f
-	-	-	2XXX/138	2YYY/141	125	II.B.3.f
-	-	-	2XXX/139	2YYY/142	115	II.B.3.f



Existing Structure Number Ckt. 1	Existing Structure Number Ckt. 2	Existing Structure Height (ft.)	Proposed Structure Number Ckt. 1	Proposed Structure Number Ckt. 2	Proposed Structure Height (ft)	Attachment II.B.3 Structure Type
-	-	-	2XXX/140	2YYY/143	115	II.B.3.g
-	-	-	2XXX/141	2YYY/144	120	II.B.3.f
-	-	-	2XXX/142	2YYY/145	135	II.B.3.f
-	-	-	2XXX/143	2YYY/146	135	II.B.3.f
-	-	-	2XXX/144	2YYY/147	130	II.B.3.f
-	-	-	2XXX/145	2YYY/148	110	II.B.3.f
-	-	-	2XXX/146	2YYY/149	115	II.B.3.g
-	-	-	2XXX/147	2YYY/150	105	II.B.3.g
-	-	-	2XXX/148	2YYY/151	140	II.B.3.f
-	-	-	2XXX/149	2YYY/152	105	II.B.3.f
-	-	-	2XXX/150	2YYY/153	120	II.B.3.f
-	-	-	2XXX/151	2YYY/154	125	II.B.3.f
-	-	-	2XXX/152	2YYY/155	110	II.B.3.f
-	-	-	2XXX/153	2YYY/156	125	II.B.3.f
-	-	-	2XXX/154	2YYY/157	125	II.B.3.f
-	-	-	2XXX/155	2YYY/158	130	II.B.3.f
-	-	-	2XXX/156	2YYY/159	140	II.B.3.f
-	-	-	2XXX/157	2YYY/160	160	II.B.3.f
-	-	-	2XXX/158	2YYY/161	135	II.B.3.f
-	-	-	2XXX/159	2YYY/162	135	II.B.3.f
-	-	-	2XXX/160	2YYY/163	125	II.B.3.f
-	-	-	2XXX/161	2YYY/164	100	II.B.3.g
-	-	-	2XXX/162	2YYY/165	130	II.B.3.f
-	-	-	2XXX/163	2YYY/166	135	II.B.3.f
-	-	-	2XXX/164	2YYY/167	140	II.B.3.f
-	-	-	2XXX/165	2YYY/168	110	II.B.3.g
-	-	-	2XXX/166	2YYY/169	140	II.B.3.f
-	-	-	2XXX/167	2YYY/170	125	II.B.3.f
-	-	-	2XXX/168	2YYY/171	125	II.B.3.f
-	-	-	2XXX/169	2YYY/172	125	II.B.3.f
-	-	-	2XXX/170	2YYY/173	100	II.B.3.g
-	-	-	2XXX/171	2YYY/174	85	II.B.3.b
-	-	-	2XXX/172	2YYY/175	95	II.B.3.g
-	-	-	2XXX/173	2YYY/176	110	II.B.3.f
-	-	-	2XXX/174	2YYY/177	95	II.B.3.g
-	-	-	2XXX/175	2YYY/178	110	II.B.3.f

Existing Structure Number Ckt. 1	Existing Structure Number Ckt. 2	Existing Structure Height (ft.)	Proposed Structure Number Ckt. 1	Proposed Structure Number Ckt. 2	Proposed Structure Height (ft)	Attachment II.B.3 Structure Type
-	-	-	2XXX/176	2YYY/179	135	II.B.3.f
-	-	-	2XXX/177	2YYY/180	110	II.B.3.g
-	-	-	2XXX/178	2YYY/181	140	II.B.3.f
-	-	-	2XXX/179	2YYY/182	140	II.B.3.f
-	-	-	2XXX/180	2YYY/183	120	II.B.3.f
-	-	-	2XXX/181	2YYY/184	120	II.B.3.f
-	-	-	2XXX/182	2YYY/185	120	II.B.3.f
-	-	-	2XXX/183	2YYY/186	105	II.B.3.f
-	-	-	2XXX/184	2YYY/187	140	II.B.3.f
-	-	-	2XXX/185	2YYY/188	145	II.B.3.g
-	-	-	2XXX/186	2YYY/189	95	II.B.3.c
-	-	-	2XXX/187	2YYY/190	185	II.B.3.g
-	-	-	2XXX/188	2YYY/191	115	II.B.3.b
-	-	-	2XXX/189	2YYY/192	95	II.B.3.g
-	-	-	2XXX/190	2YYY/193	120	II.B.3.f
-	-	-	2XXX/191	2YYY/194	120	II.B.3.f
-	-	-	2XXX/192	2YYY/195	120	II.B.3.f
-	-	-	2XXX/193	2YYY/196	155	II.B.3.f
-	-	-	2XXX/194	2YYY/197	110	II.B.3.f
-	-	-	2XXX/195	2YYY/198	100	II.B.3.f
-	-	-	2XXX/196	2YYY/199	145	II.B.3.f
-	-	-	2XXX/197	2YYY/200	120	II.B.3.f
-	-	-	2XXX/198	2YYY/201	115	II.B.3.g
-	-	-	2XXX/199	2YYY/202	105	II.B.3.f
-	-	-	2XXX/200	2YYY/203	100	II.B.3.f
-	-	-	2XXX/201	2YYY/204	120	II.B.3.g
-	-	-	2XXX/202	2YYY/205	115	II.B.3.g
-	-	-	2XXX/203	2YYY/206	140	II.B.3.f
-	-	-	2XXX/204	2YYY/207	140	II.B.3.f
-	-	-	2XXX/205	2YYY/208	125	II.B.3.b
-	-	-	2XXX/206	2YYY/209	125	II.B.3.f
-	-	-	2XXX/207	2YYY/210	125	II.B.3.f
-	-	-	2XXX/208	2YYY/211	120	II.B.3.f
-	-	-	2XXX/209	2YYY/212	105	II.B.3.g
29/1851	-	56	2XXX/210	2YYY/213	105	II.B.3.f
29/1852	-	66	2XXX/211	2YYY/214	105	II.B.3.f

Existing Structure Number Ckt. 1	Existing Structure Number Ckt. 2	Existing Structure Height (ft.)	Proposed Structure Number Ckt. 1	Proposed Structure Number Ckt. 2	Proposed Structure Height (ft)	Attachment II.B.3 Structure Type
29/1853	-	68	2XXX/212	2YYY/215	105	II.B.3.f
29/1854	-	56	2XXX/213	2YYY/216	130	II.B.3.g
-	-	-	2XXX/214	2YYY/217	160	II.B.3.g
-	-	-	2XXX/215	2YYY/218	165	II.B.3.g
-	-	-	2XXX/216	2YYY/219	145	II.B.3.g
568/37	-	113.5	568/37	-	125	II.B.3.l
568/38	-	159	568/38	-	150	II.B.3.l
568/39	-	157.5	568/39	-	180	II.B.3.k
568/40	-	111	568/40	-	175	II.B.3.i
568/41	-	96.5	568/41	-	185	II.B.3.i
568/42	-	98.5	568/42	-	165	II.B.3.i
568/43	-	97	568/43	-	170	II.B.3.i
568/44	-	127.5	568/44	-	180	II.B.3.i
568/45	-	107	568/45	-	170	II.B.3.j
568/46	-	122	568/46	-	180	II.B.3.i
568/47	-	93	568/47	-	165	II.B.3.i
568/48	-	108.5	568/48	-	175	II.B.3.i
568/49	-	109	568/49	-	180	II.B.3.i
568/50	-	116.5	568/50	-	195	II.B.3.i
568/51	-	118	568/51	-	180	II.B.3.i
568/52	-	120	568/52	-	160	II.B.3.j
568/53	-	106	568/53	-	160	II.B.3.i
568/54	-	93	568/54	-	160	II.B.3.i
568/55	-	98	568/55	-	185	II.B.3.i
568/56	-	113	568/56	-	175	II.B.3.j
568/57	-	117.5	568/57	-	195	II.B.3.i
568/58	-	109.5	568/58	-	190	II.B.3.i
568/59	-	113.5	568/59	-	180	II.B.3.i
568/60	-	122.5	568/60	-	185	II.B.3.j
568/61	-	123	568/61	-	195	II.B.3.i
568/62	-	139	568/62	-	195	II.B.3.i
568/63	-	122.5	568/63	-	195	II.B.3.i
568/64	-	127	568/64	-	180	II.B.3.i
568/65	-	97.5	568/65	-	175	II.B.3.j
568/66	-	96.5	568/66	-	185	II.B.3.i
568/67	-	103.5	-	-	**	-

Existing Structure Number Ckt. 1	Existing Structure Number Ckt. 2	Existing Structure Height (ft.)	Proposed Structure Number Ckt. 1	Proposed Structure Number Ckt. 2	Proposed Structure Height (ft)	Attachment II.B.3 Structure Type
568/68	-	97	568/68	-	180	II.B.3.i
568/69	-	142.5	568/69	-	185	II.B.3.j
568/70	-	109	568/70	-	170	II.B.3.i
-	-	-	568/70A	-	185	II.B.3.i
568/71	-	134.5	568/71	-	180	II.B.3.i
568/72	-	139.5	568/72	-	170	II.B.3.i
-	-	-	568/72A	-	180	II.B.3.i
568/73	-	69.5	568/73	-	175	II.B.3.j
568/74	-	107.5	568/74	-	170	II.B.3.i
568/75	-	110	568/75	-	165	II.B.3.i
2083/1A	2090/1A		2080/1A	2090/1A	*	N/A
		N/A	2083/1B	-	115	II.B.3.n
		N/A	2083/1C	-	115	II.B.3.n
		N/A	2083/1D	-	115	II.B.3.o
		N/A	2083/2	2ZZZ/3	115	II.B.3.n
		N/A	2083/3	2ZZZ/4	120	II.B.3.m
		N/A	2083/4	2ZZZ/5	100	II.B.3.m
		N/A	2083/5	2ZZZ/6	105	II.B.3.m
		N/A	2083/6	2ZZZ/7	100	II.B.3.n
		N/A	2083/7	2ZZZ/8	110	II.B.3.m
		N/A	2083/8	2ZZZ/9	115	II.B.3.n
2157/5406	2083/9	115	2083/9	2ZZZ/10	*	N/A
Minimum		56.0			85.0	
Maximum		165.0			195.0	
Average		113.9			130.9	

\*Existing structures that are not being replaced and are excluded from minimum, maximum, and average calculations.

\*\*Existing structures that are being removed and not replaced; excluded from minimum, maximum and average calculations.

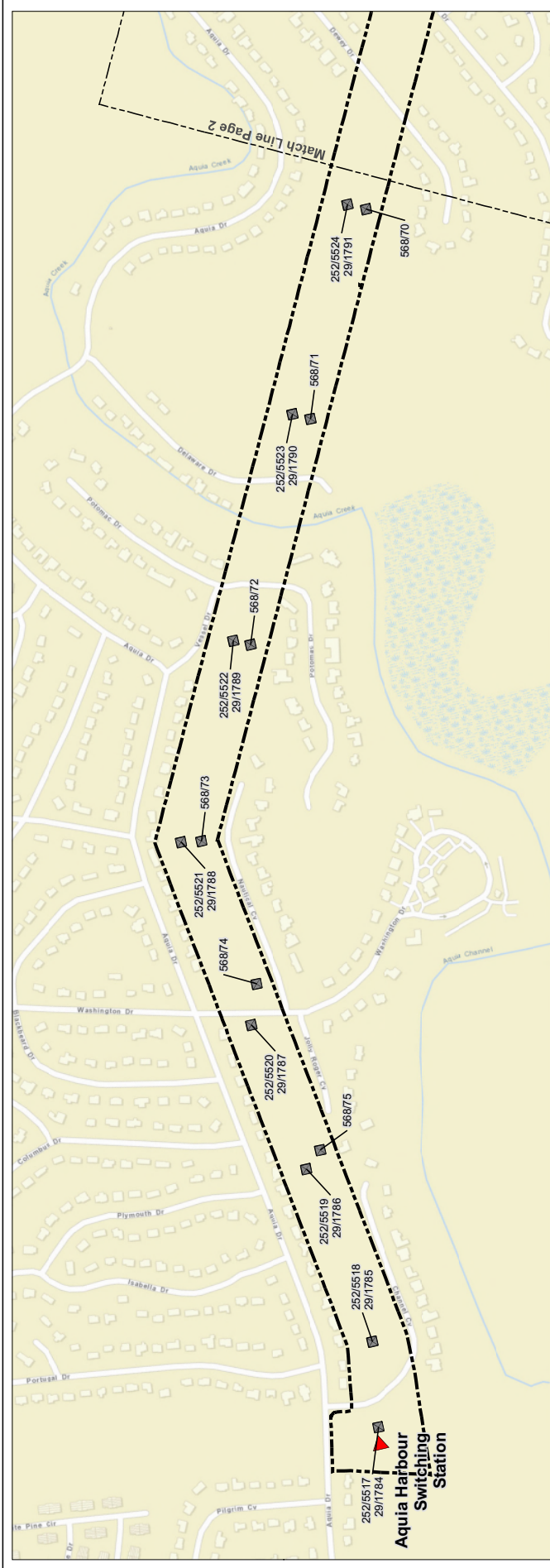
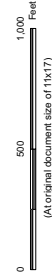


Table II.B.5a

Existing Structure Number	252/5517	29/1784	252/5518	29/1785	252/5519	29/1786	252/5520	29/1787	252/5521	29/1788	252/5522	29/1789	252/5523	29/1790	252/5524	29/1791
Existing Structure Height (ft)																
Existing Structure Height (ft)	95	107.5	107.5	106	126	117	131	144.5	105.5							

Existing Structure Number	568/75	568/74	568/73	568/72	568/71	568/70
Existing Structure Height (ft)	110	107.5	69.5	139.5	134.5	109

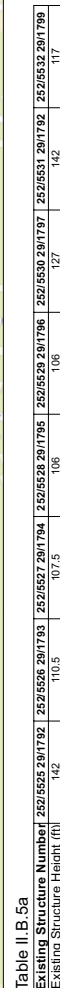


Prepared by JPK on 2024-07-18  
Reviewed by JPK on 2024-07-18  
R by LRC 2024-07-18  
203401909

Client/Project  
Dominion Energy Virginia  
Aquia Harbour - Possum Point  
Lines #29, #252, #2083, and #568 Rebuild  
Figure No.

Title  
**Existing Structures**

Notes  
1. Coordinate System: NAD 1983 StatePlane Virginia South FIPS 4502 Feet  
2. Elevation: Mean Sea Level (MSL)  
3. Blinnings © ESR Word Street Map



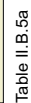
Existing Structure Number	568/69	568/68	568/67	568/66	568/65	568/64	568/63	568/62
Eveling Structure Height (ft)	142.5	07	103.5	06.5	07.5	127	172.5	130



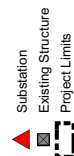
**Notes**  
1. Coordinate System: NAD 1983 StatePlane Virginia South FIPS 4502 Feet  
2. Data Sources: Dominion Energy Virginia, Stantec, U.S. Census Bureau  
3. Basemap © ESRI World Street Map

Page 2 of 9





Existing Structure Number	568/62	568/61	568/60	568/59	568/58	568/57	568/56	568/55
Elevation Structure Height (ft)	130	123	122.5	113.5	100.5	117.5	113	08



0 500 1,000 Feet  
(At original document size of 11x17)  
15,000



<i>Title</i>	Existing Structures
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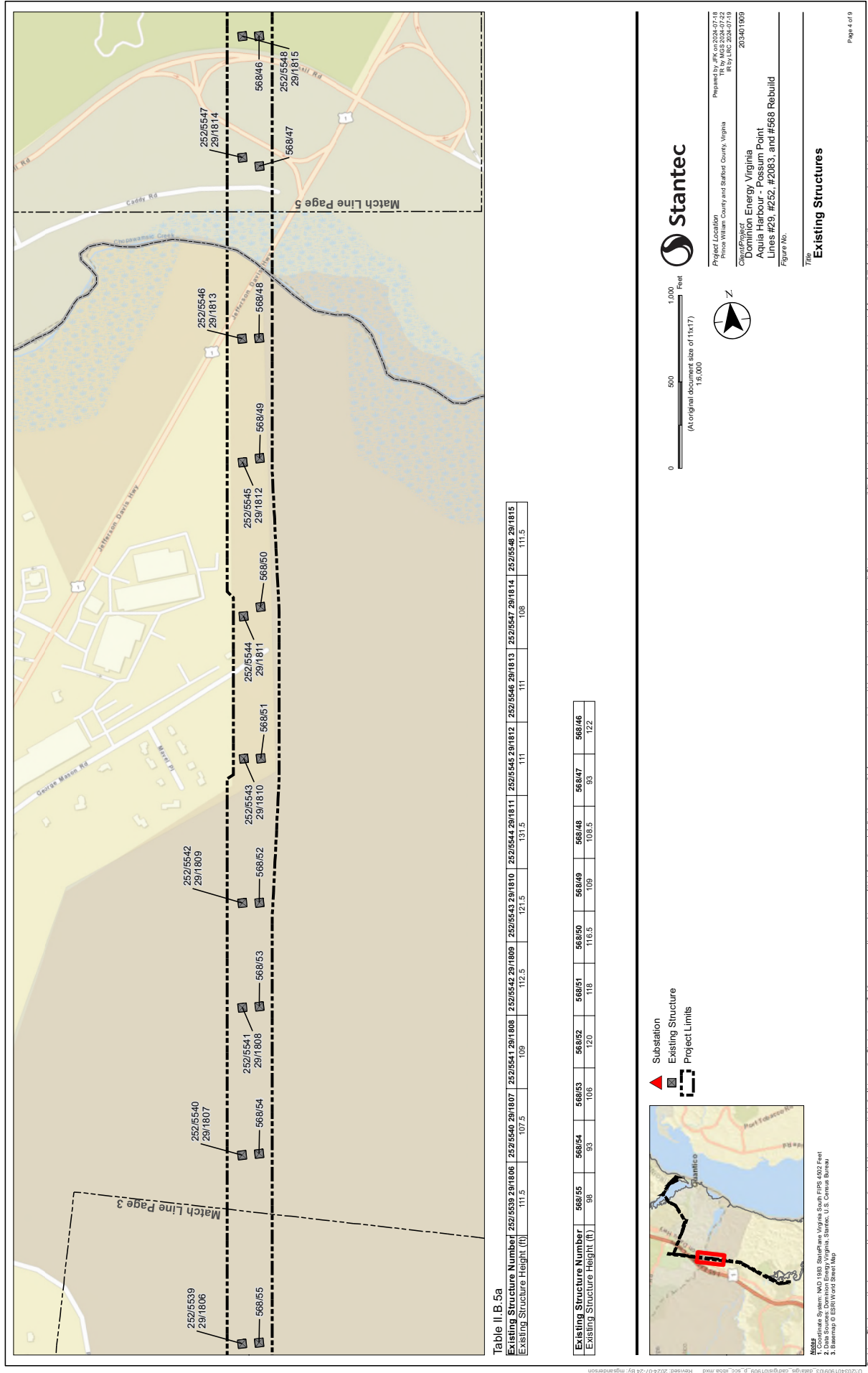






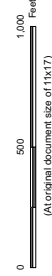
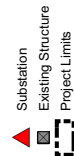
Table II.B.5a

Existing Structure Number	252/5556	29/1823	252/5557	29/1824	252/5558	29/1825	252/5559	29/1826	252/5560	29/1827	252/5561	29/1828	252/5562	29/1829	252/5563	29/1830
Existing Structure Height (ft)	110	73.5	122	112.5	142	144	141.5	108.5	108.5	106.5						

Existing Structure Number	568/39	568/38	568/37
Existing Structure Height (ft)	157.5	159	113.5



Notes:  
1. Coordinate System: NAD 1983, StatePlane Virginia South FIPS 4602 Feet  
2. Elevation: Mean Sea Level (MSL)  
3. Basemap: © ESRI World Street Map



Project Location  
Prince William County and Stafford County, Virginia

Prepared by JPK on 2024-07-18  
Reviewed by JPK on 2024-07-18  
R by LRC 2024-07-18

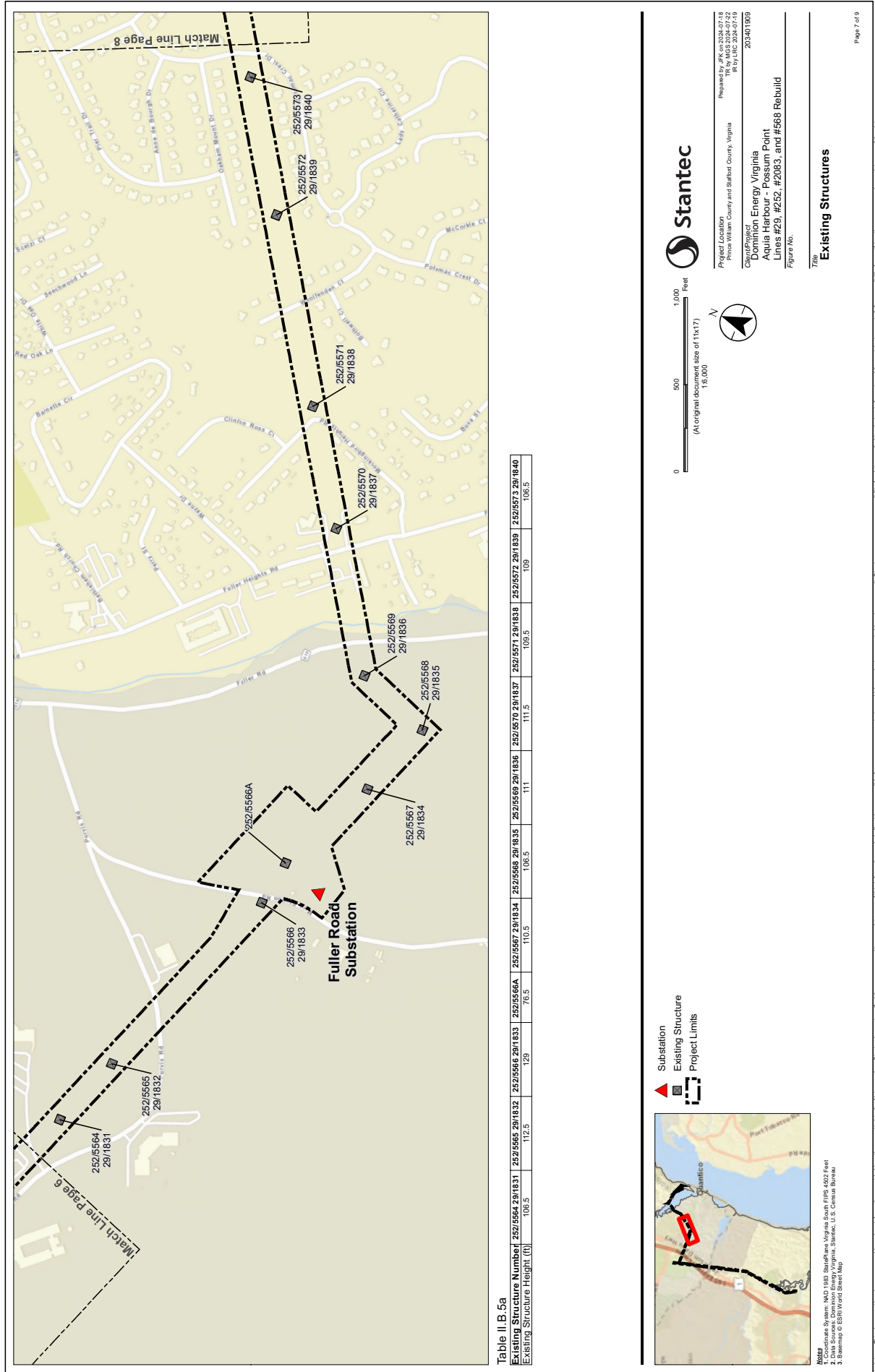
203401909

Client/Project  
Dominion Energy Virginia  
Aquia Harbour - Possum Point  
Lines #29, #252, #2083, and #568 Rebuild

Figure No.

Title  
Existing Structures





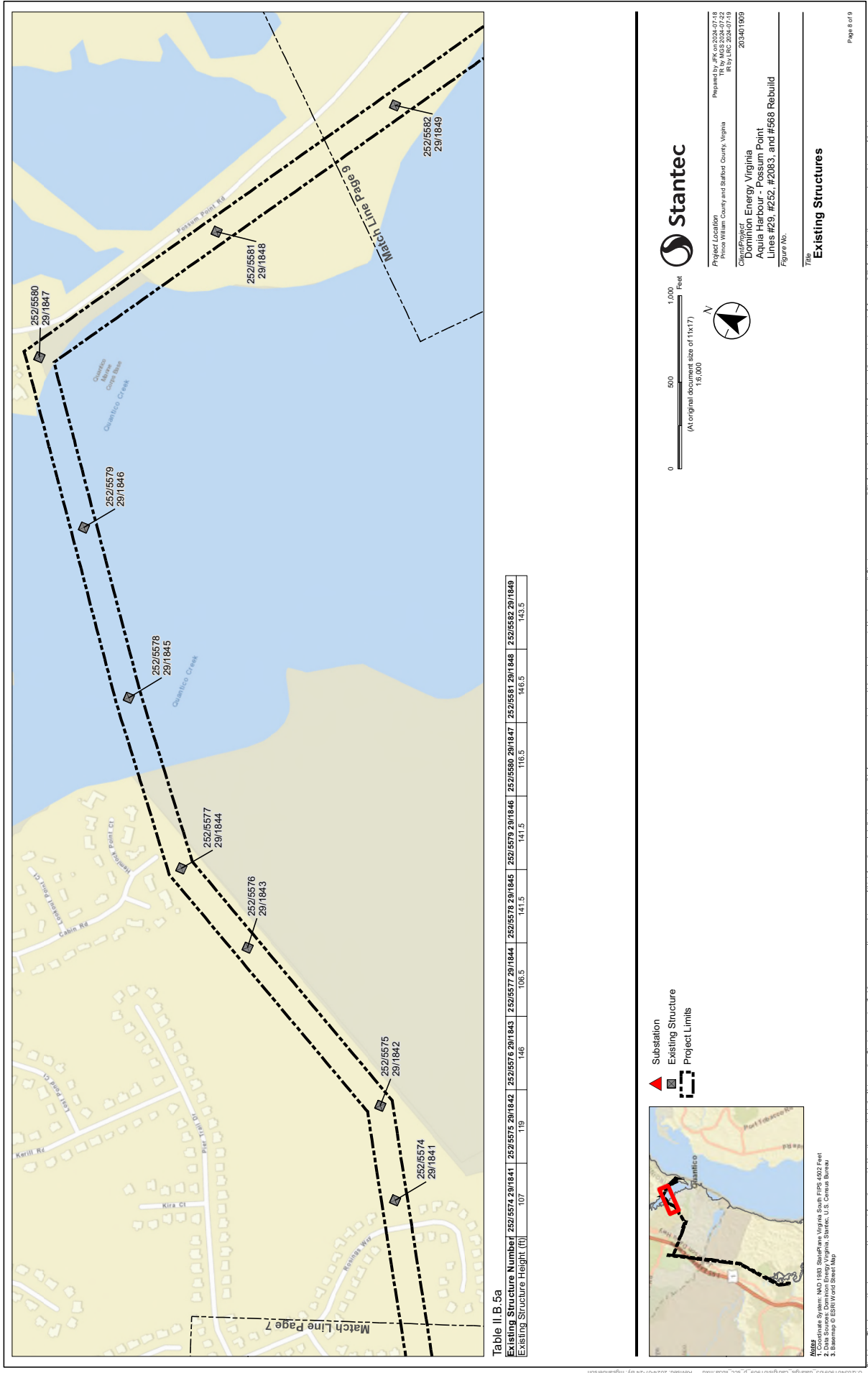
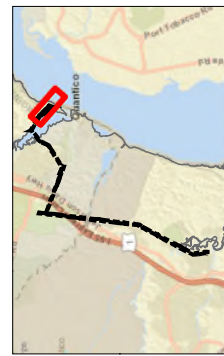




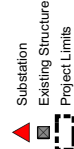


Table II.B.5a

Existing Structure Number	252/5582	29/1849	252/5583	29/1850	252/5584	252/5585	252/5587	252/5588
Existing Structure Height (ft)	143.5	116.5	73.5	80	74	121		



Notes:  
1. Coordinate System: NAD 1983, StatePlane Virginia South FIPS 4602 Feet  
2. Elevation: Mean Sea Level (MSL)  
3. Boundary: © ESRI World Street Map

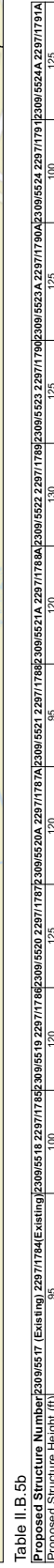


0 500 1,000 Feet  
(Original document size of 11x17)  
1:5,000



Project Location  
Prince William County and Stafford County, Virginia  
Client/Project  
Dominion Energy Virginia  
Aquaria Harbour - Possum Point  
Lines #29, #252, #2083, and #568 Rebuild  
Figure No.  
203401909

Title  
Existing Structures



Proposed Structure Number	568775	568774	568773	56872A	56872	56871	56870A	56870
Proposed Structure Height (ft)	165	170	175	180	170	180	185	170

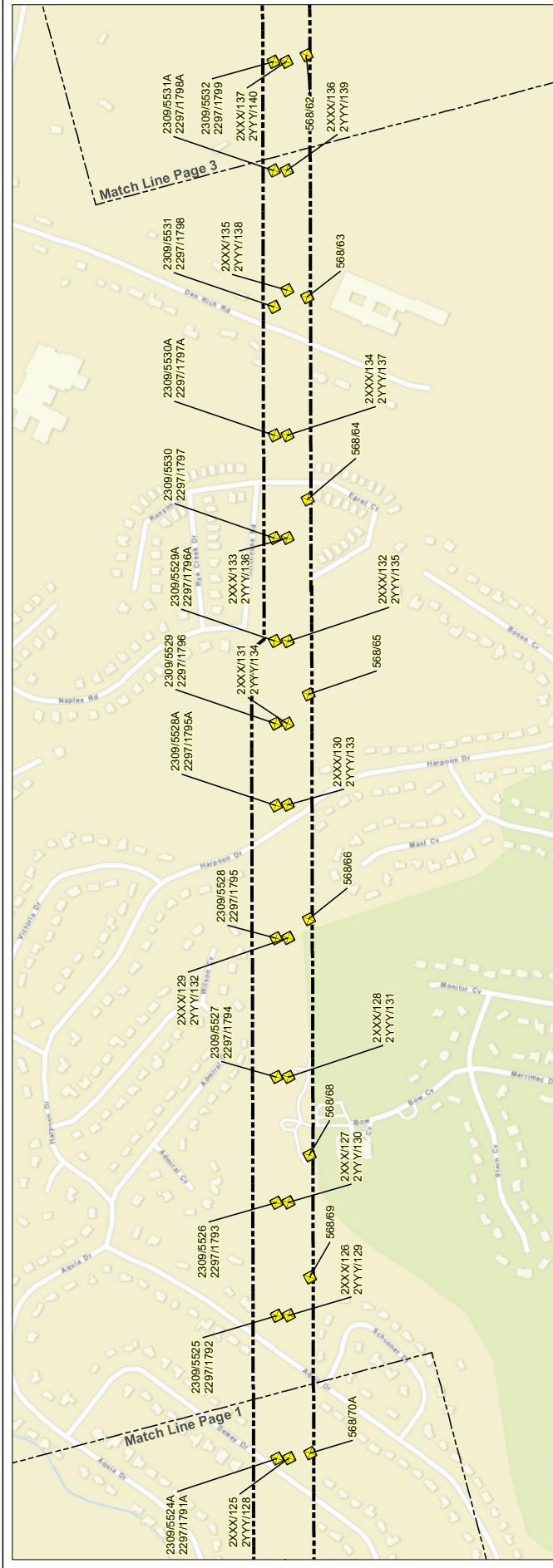


Table II.B.5b

[illegible]

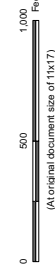
Proposed Structure Number	2XXX/125	2YYY/128	2XXX/126	2YYY/129	2XXX/127	2YYY/130	2XXX/128	2YYY/131	2XXX/129	2YYY/132	2XXX/130	2YYY/133	2XXX/131	2YYY/134	2XXX/132	2YYY/135	2XXX/133	2YYY/136	2XXX/134	2YYY/137	2XXX/135	2YYY/138	2XXX/136	2YYY/139	2XXX/137	2YYY/140
Proposed Structure Height (ft)	125	125	145	145	195	195	195	195	120	125	100	100	135	135	105	105	135	135	125	125	140	140	130	130	115	115

Proposed Structure Number	568/70A	568/69	568/68	568/66	568/65	568/64	568/63	568/62
Proposed Structure Height (ft)	195	195	190	185	175	190	195	195



**Notes**  
 1. Coordinate System: NAD 1983 StatePlane Virginia South FIPS 4502 Feet  
 2. Data Sources: Dominion Energy Virginia, Startec, U.S. Census Bureau  
 3. Basemap © ESRI World Street Map

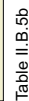
## Proposed Structure Project Limits







<p><b>Project Location</b>          Prince William County and Stafford County, Virginia</p>	<p>Prepared by JRF on 2024-07-19          TR W AGS 2024-07-22          R By LRC 2024-07-19</p>
<p><b>Client/Project</b>          Dominion Energy Virginia          Aquia Harbour - Possum Point          Lines #29, #252, #2083, and #568 Rebuild</p>	<p>203401909</p>

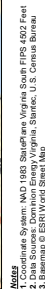
<i>Title</i>	Proposed Structures
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Page 2 of 9



Proposed Structure Number	2XXX/137	2YYY/140	2XXX/138	2YYY/141	2XXX/142	2XXX/140	2YYY/143	2XXX/141	2YYY/144	2XXX/142	2YYY/145	2XXX/143	2YYY/144	2XXX/145	2YYY/146	2XXX/147	2YYY/149	2XXX/148	2YYY/151
Proposed Structure Height (ft)	115	115	125	115	115	115	120	120	120	135	135	135	130	110	115	105	140	140	140

 Substation/Switching Station  
 Proposed Structure  
 Existing Structure to Remain  
 Project Limits



(At original document size of 11x17)

0 500 1,000 Feet



*Client/Project*  
**Dominion Energy Virginia**

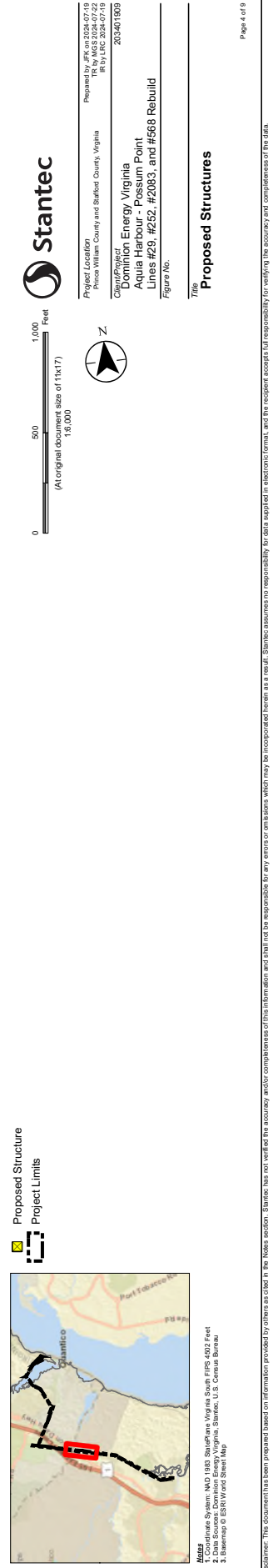
Figure No.

<i>Title</i>	Proposed Structures
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<b>Proposed Structure Number</b>	2XX/X/148	2YY/Y/151	2XX/X/149	2YY/Y/152	2XX/X/150	2YY/Y/153	2XX/X/151	2YY/Y/154	2XX/X/152	2YY/Y/155	2XX/X/153	2YY/Y/156	2XX/X/154	2YY/Y/157	2XX/X/155	2YY/Y/156	2XX/X/157	2YY/Y/158	2XX/X/159	2YY/Y/160	2XX/X/161	2XX/X/162
<b>Proposed Structure Height (ft)</b>	140	140	105	120	120	125	125	125	110	125	125	125	125	125	130	140	160	135	135	135	135	135

Proposed Structure Number	568/55	568/54	568/53	568/52	568/51	568/50	568/49	568/48	568/47	568/46
Proposed Structure Height (ft)	185	160	160	160	180	195	180	175	165	180



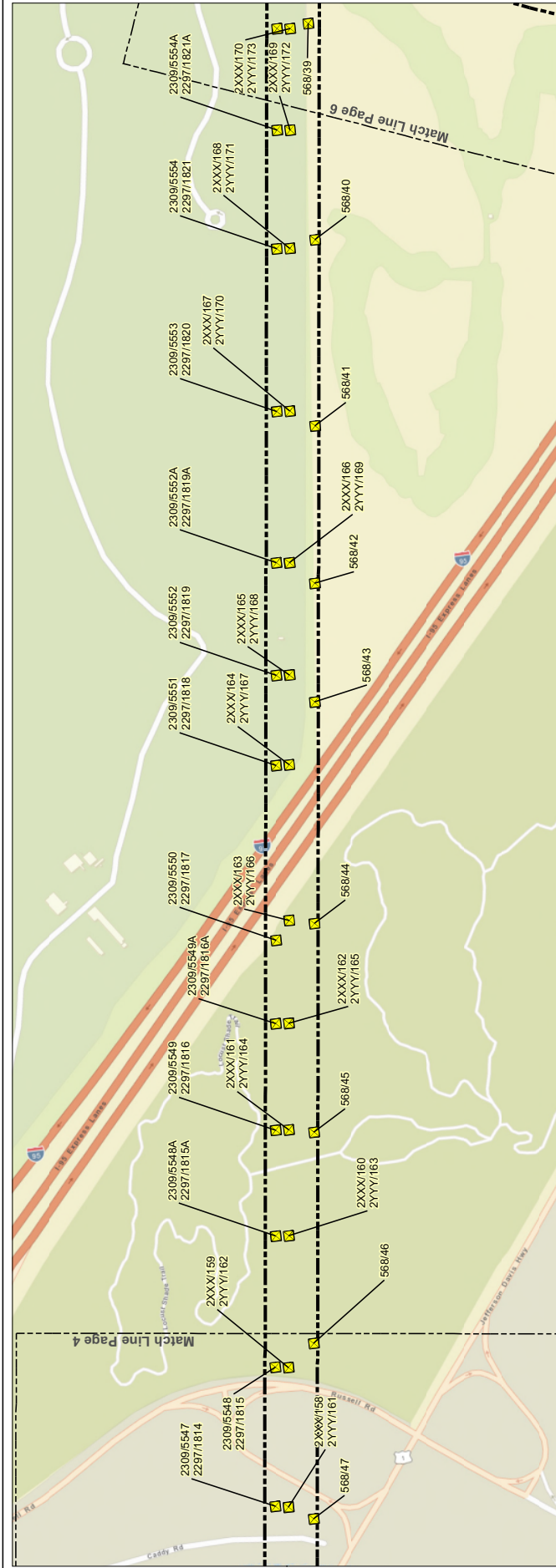


Table II.B.5b

[illegible]

Proposed Structure Number	2XXX/158	2YYY/161	2XXX/162	2XXX/160	2YYY/163	2XXX/161	2YYY/164	2XXX/162	2YYY/165	2XXX/163	2YYY/166	2XXX/164	2YYY/167	2XXX/168	2YYY/169	2XXX/167	2YYY/170	2XXX/168	2YYY/171	2XXX/169	2YYY/172	2XXX/170	2YYY/173
Dressed Structure Height (ft)	135	135	135	135	135	100	100	130	130	135	135	140	140	110	110	140	140	125	125	195	195	100	100

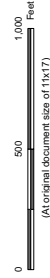
Proposed Structure Number	568/47	568/46	568/45	568/44	568/43	568/42	568/41	568/40	568/39
Proposed Structure Height (ft)	165	180	170	180	170	165	185	175	180



**Notes**

1. Coordinate System: NAD 1983 StatePlane Virginia South FIPS 4502 Feet
2. Data Sources: Dominion Energy Virginia, Startec, U.S. Census Bureau
3. Basemap © ESRI/World Street Map

Proposed Structure  
Project Limits



<p>Project Location          Prince William County and Stafford County, Virginia</p>	<p>Prepared by: JFRC on 2024-07-19          TR by AGS on 2024-07-22          R by LRC on 2024-07-19</p>
<p>Client/Project          Dominion Energy Virginia          Aquia Harbour - Possum Point          Lines #29, #252, #2083, and #568 Rebuild</p>	<p>203401909</p>
<p>Estimate No.</p>	

<i>Title</i>	Proposed Structures
1. <i>Introduction</i>	1.1. <i>Background</i>
2. <i>Methodology</i>	2.1. <i>Data Collection</i>
3. <i>Results</i>	3.1. <i>Analysis</i>
4. <i>Conclusion</i>	4.1. <i>Summary</i>

Page 5 of 9



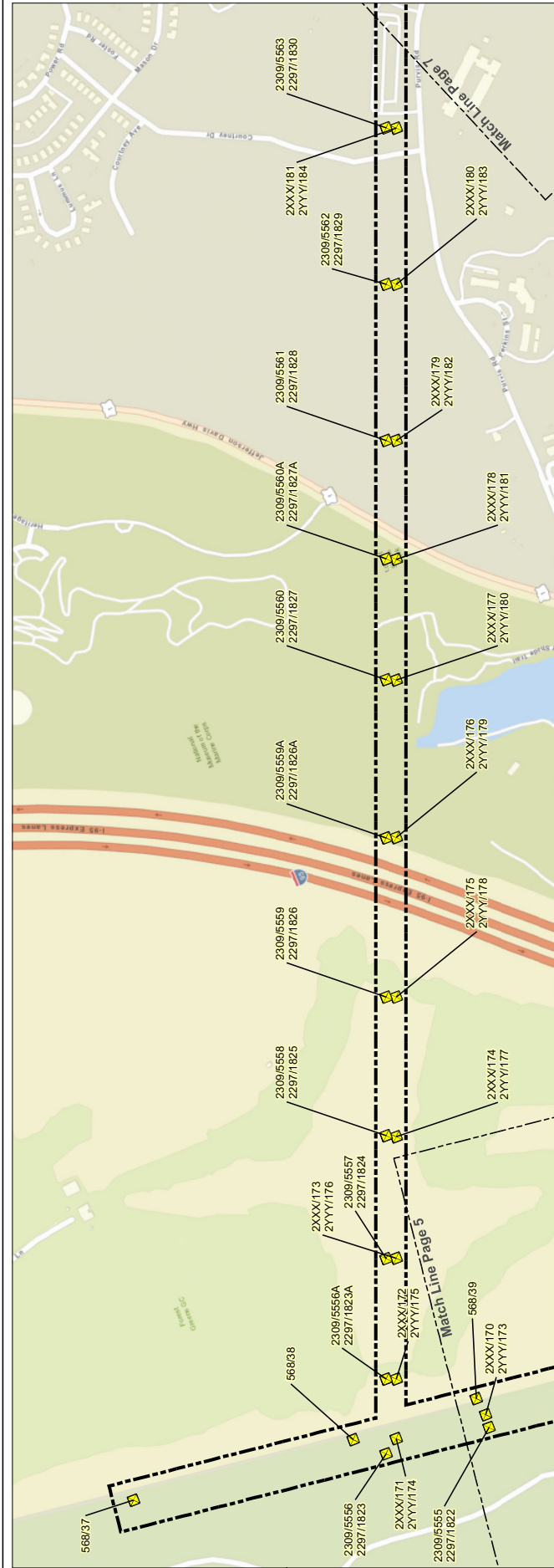


Table II.B.5b

Proposed Structure Number	2309/5555	2297/182	2230/5556	2297/1823	2309/5556A	2297/1823A	2309/5557	2297/1824	2309/5558	2297/1825	2309/5559	2297/1826A	2309/5560A	2297/1827	2309/5561	2297/1828	2309/5562	2297/1829	2309/5563	2297/1830
Proposed Structure Height (ft)	100	90	95	95	110	95	110	110	95	115	135	140	140	140	140	140	170	125		

Proposed Structure Number	2XXX/170	2YYY/173	2XXX/171	2YYY/174	2XXX/172	2YYY/175	2XXX/173	2YYY/176	2XXX/174	2YYY/177	2XXX/175	2YYY/178	2XXX/176	2YYY/179	2XXX/177	2YYY/180	2XXX/178	2YYY/181	2XXX/179	2YYY/182	2XXX/180	2YYY/183	2XXX/181	2YYY/184
Proposed Structure Height (ft)	100	85	95	110	110	95	110	110	95	110	110	135	140	110	110	140	140	140	140	120	120	120	120	120

Proposed Structure Number	568/39	568/38	568/37
Proposed Structure Height (ft)	1.00	1.50	1.75



**Notes**  
1. Coordinate System: NAD 1983 StatePlane Virginia South FIPS 4502 Feet  
2. Data Sources: Dominion Energy Virginia, Santee, U. S. Census Bureau  
3. Basemap © ESRI World Street Map

Proposed Structure  
Project Limits

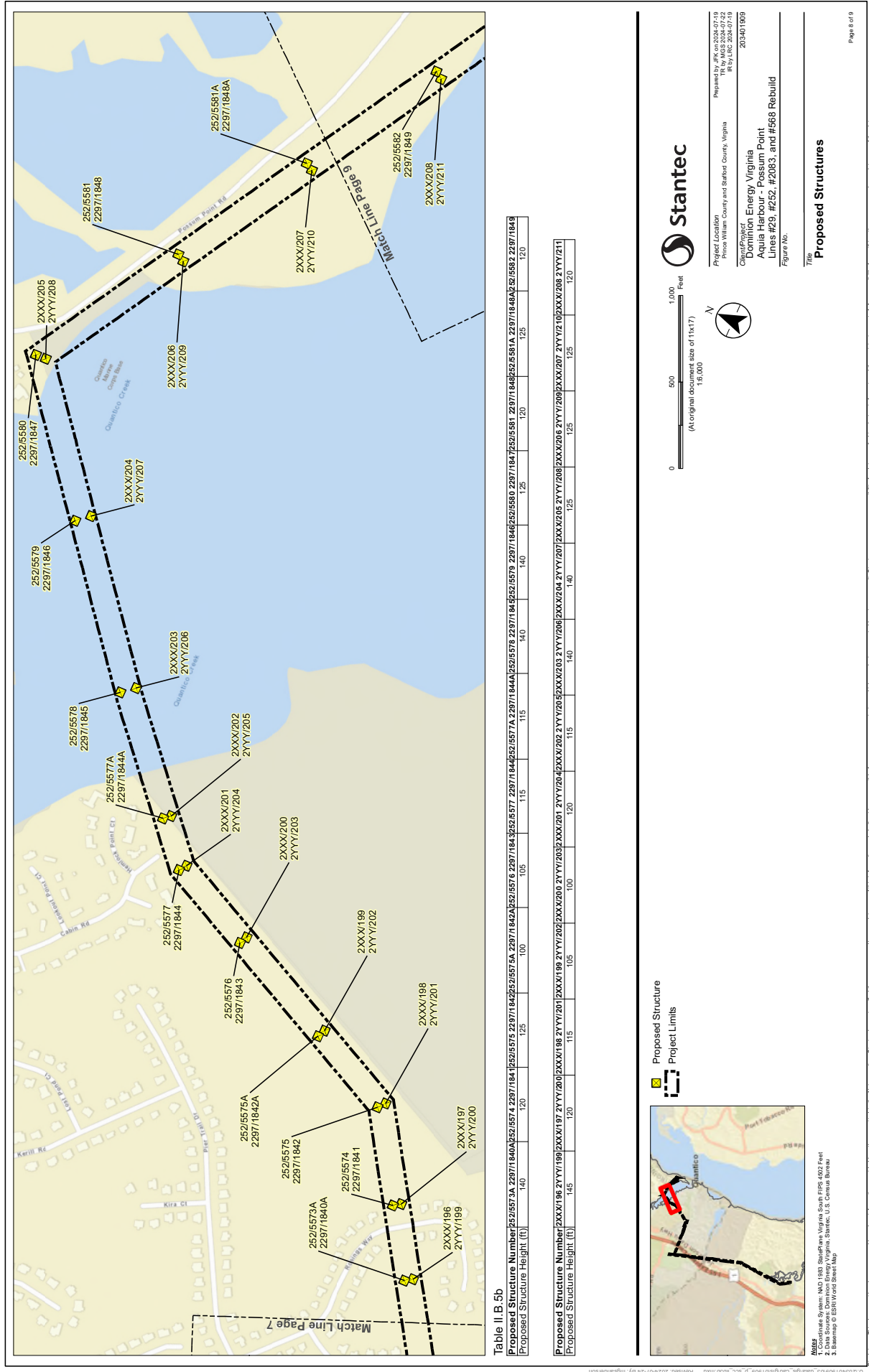


<p>Project Location          Prince William County and Stafford County, Virginia</p>	<p>Client/Project          Dominion Energy Virginia          Aquia Harbour - Possum Point          Lines #29, #252, #2083, and #568 Rebuild</p>	<p>Prepared by: JFRC on 2024-07-19          TR by AGS on 2024-07-22          R by LRC on 2024-07-19</p>
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<i>Title</i>	Proposed Structures
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Page 6 of 9





**Notes**  
1. Coordinate System: NAD 1983 StatePlane Virginia South FIPS 4602 Feet  
2. Elevation: Mean Sea Level  
3. Boundary: © ESRI World Street Map

**Proposed Structures**

Prepared by JPK on 2024-07-19  
Reviewed by JPK on 2024-07-19  
R by LRC 2024-07-19  
203401909  
Project Location: Prince William County and Stafford County, Virginia  
Client/Project: Dominion Energy Virginia  
Aquaria Harbour - Potomac Point  
Lines #29, #252, #2083, and #568 Rebuild  
Figure No.  
Title  
Page 8 of 9



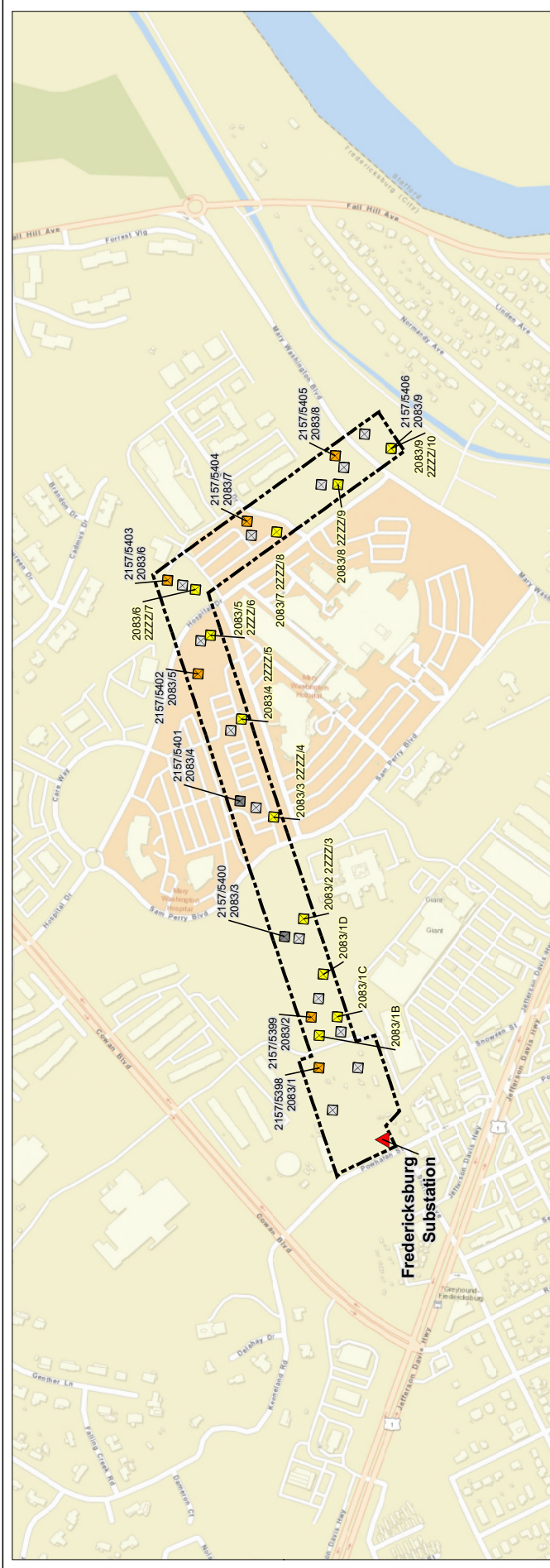


Table II.B.5c

Proposed Structure Number	Existing Structure Number	Proposed Structure Height (ft)	Existing Structure Height (ft)
20831A	2157/5398	115	90
20831B	2157/5399	115	90
20831C	2157/5400	115	90
20831D	2157/5401	115	90
20831E	2157/5402	115	90
20831F	2157/5403	115	90
20831G	2157/5404	115	90
20831H	2157/5405	115	90
20831I	2157/5406	115	90
20831J	2157/5407	115	90
20831K	2157/5408	115	90
20831L	2157/5409	115	90
20831M	2157/5410	115	90
20831N	2157/5411	115	90
20831O	2157/5412	115	90
20831P	2157/5413	115	90
20831Q	2157/5414	115	90
20831R	2157/5415	115	90
20831S	2157/5416	115	90
20831T	2157/5417	115	90
20831U	2157/5418	115	90
20831V	2157/5419	115	90
20831W	2157/5420	115	90
20831X	2157/5421	115	90
20831Y	2157/5422	115	90
20831Z	2157/5423	115	90
20832A	2157/5424	115	90
20832B	2157/5425	115	90
20832C	2157/5426	115	90
20832D	2157/5427	115	90
20832E	2157/5428	115	90
20832F	2157/5429	115	90
20832G	2157/5430	115	90
20832H	2157/5431	115	90
20832I	2157/5432	115	90
20832J	2157/5433	115	90
20832K	2157/5434	115	90
20832L	2157/5435	115	90
20832M	2157/5436	115	90
20832N	2157/5437	115	90
20832O	2157/5438	115	90
20832P	2157/5439	115	90
20832Q	2157/5440	115	90
20832R	2157/5441	115	90
20832S	2157/5442	115	90
20832T	2157/5443	115	90
20832U	2157/5444	115	90
20832V	2157/5445	115	90
20832W	2157/5446	115	90
20832X	2157/5447	115	90
20832Y	2157/5448	115	90
20832Z	2157/5449	115	90
20833A	2157/5450	115	90
20833B	2157/5451	115	90
20833C	2157/5452	115	90
20833D	2157/5453	115	90
20833E	2157/5454	115	90
20833F	2157/5455	115	90
20833G	2157/5456	115	90
20833H	2157/5457	115	90
20833I	2157/5458	115	90
20833J	2157/5459	115	90
20833K	2157/5460	115	90
20833L	2157/5461	115	90
20833M	2157/5462	115	90
20833N	2157/5463	115	90
20833O	2157/5464	115	90
20833P	2157/5465	115	90
20833Q	2157/5466	115	90
20833R	2157/5467	115	90
20833S	2157/5468	115	90
20833T	2157/5469	115	90
20833U	2157/5470	115	90
20833V	2157/5471	115	90
20833W	2157/5472	115	90
20833X	2157/5473	115	90
20833Y	2157/5474	115	90
20833Z	2157/5475	115	90

Project Location  
City of Fredericksburg, Virginia

Client/Project  
Dominion Energy Virginia  
Aquaria Harbour - Possum Point  
Lines #29, #252, #2083, and #568 Rebuild

Figure No.  
2083

Prepared by JPK on 2024-07-19  
Reviewed by JPK on 2024-07-24  
By JPK on 2024-07-24

Scale  
0 500 1,000 Feet  
(Original document size of 11x17)  
1:5,000

North Arrow

Legend

- Substation
- Proposed Structure
- Existing Structure
- Other Existing Structure (PUR-2024-00035)
- Existing Structure to Remain (PUR-2024-00035)
- Project Limits

Notes

- Coordinate System: NAD 1983, StatePlane Virginia South FIPS 4602 Feet
- Scale: As Shown
- Blasmap © ESRI World Street Map

Title  
Existing and Proposed Structures Line  
2083

Page 1 of 1

## II. DESCRIPTION OF THE PROPOSED PROJECT

### B. Line Design and Operational Features

6. Provide photographs for typical existing facilities to be removed, comparable photographs or representations for proposed structures, and visual simulations showing the appearance of all planned transmission structures at identified historic locations within one mile of the proposed centerline and in key locations identified by the Applicant.

Response: (a) *Photographs for typical existing facilities to be removed.*

See Attachments II.B.6.a.i-xi for representative photographs of typical existing structures.

(b) *Comparable photographs or representations for proposed structures.*

See Attachments II.B.6.b.i-xi, for representative photographs of the proposed structures for the Rebuild Project.

(c) *Visual simulations showing the appearance of all planned transmission structures at identified historic locations within one mile of the proposed centerline and in key locations.*

Visual simulations showing the appearance of the proposed transmission structures are provided for historic properties where the Rebuild Project will be visible. These simulations were created using GIS modeling to depict whether the existing and proposed structures are or will be visible from historic properties. Observation points used for the simulations are indicated on the maps. The photo simulation locations are provided on Attachment II.B.6.c.i. Attachment II.B.6.c.ii provides existing photographs and simulations of the proposed structures from the selected observation points, where visible. The table below identifies the historic properties evaluated.

VDHR #	Resource Name	OP <sup>16</sup>	Comments
500-0001/076-0301; 076-5842	Richmond, Fredericksburg, and Potomac Railroad  Cockpit Point Battlefield	1	Existing and Proposed Structures Visible
287-0010	Quantico Marine Base Historic District	2	Proposed Structures Visible in the Background

<sup>16</sup> Observation points are not sequential as some photo locations chosen in the field were eliminated.

<b>VDHR #</b>	<b>Resource Name</b>	<b>OP<sup>16</sup></b>	<b>Comments</b>
287-0010 <sup>17</sup>	Town of Quantico Historic District	3	Not visible
076-5313 <sup>18</sup>	Camp French	4	Not visible
076-0299	Chopawamsic Recreation Demonstration Area	5	Not visible
089-0142 <sup>19</sup>	Crucifix Monument	6	Not visible
089-0103	Aquia Creek Quarries	7	Structures are slightly visible through the trees  Visible structures 568/76A and 568/76 are part of previously filed case PUR-2024-00035
089-0008	Aquia Church	8	Not visible
088-5180 089-0067	Chancellorsville Battlefield Falmouth Historic District	12	Not visible
089-0022 088-5180 111-5296 089-0067	Belmont Chancellorsville Battlefield Battle of Fredericksburg II Falmouth Historic District	13	Not visible
088-5180 089-0067	Chancellorsville Battlefield Falmouth Historic District	14	Not visible

<sup>17</sup> Per VDHR guidance, this resource does not meet the criteria to for analysis within the Stage I. As such, it is only considered within the visual simulations for the response to II.B.6.c.

<sup>18</sup> Per VDHR guidance, this resource does not meet the criteria to for analysis within the Stage I. As such, it is only considered within the visual simulations for the response to II.B.6.c.

<sup>19</sup> Per VDHR guidance, this resource does not meet the criteria to for analysis within the Stage I. As such, it is only considered within the visual simulations for the response to II.B.6.c.



<b>VDHR #</b>	<b>Resource Name</b>	<b>OP<sup>16</sup></b>	<b>Comments</b>
111-5296 089-5082	Battle of Fredericksburg II 105 West Cambridge St.		
089-0067	Falmouth Historic District	15	Not visible
111-5007 111-5295	Carl's Frozen Custard Battle of Fredericksburg I	18	Not visible
111-0147 111-5295 111-0149 111-5295 111-5296 088-5181	Fredericksburg and Spotsylvania Battlefields NMP Fall Hill Battle of Fredericksburg I Battle of Fredericksburg II Salem Church Battlefield	19	Existing and Proposed Structures Visible
111-5473 111-5295 111-5296 088-5181	Allman's Bar-B-Que Battle of Fredericksburg I Battle of Fredericksburg II Salem Church Battlefield	21	Existing and proposed structures only visible from corner of property
111-5267	Elmhurst	22	Not visible
111-5262	Washington Avenue Historic District	23	Not visible
111-0047 111-0009	Kenmore Fredericksburg Historic District Extension	24	Not visible
111-0132	Fredericksburg Historic District	25	Not visible
111-5265 111-0009	Fredericksburg City and Confederate Cemeteries Fredericksburg Historic District Extension	26	Not visible
111-0107 111-0009	John Lewis House	27	Not visible

<b>VDHR #</b>	<b>Resource Name</b>	<b>OP<sup>16</sup></b>	<b>Comments</b>
	Fredericksburg Historic District Extension		
111-0008	Brompton	28	Not visible
089-0067-0031 <sup>20</sup>	Conway House	31	Not visible

---

<sup>20</sup> Per VDHR guidance, this resource does not meet the criteria to for analysis within the Stage I. As such, it is only considered within the visual simulations for the response to II.B.6.c.



Existing Structure Type:  
230kV (Left) And 115kV (Right) Single Circuit  
Wood H-Frame (Tangent)





Existing Structure Type:  
115kV (Left) And 230kV (Right) Single Circuit  
Wood 3-Pole (DDE)







Existing Structure Type:  
230kV Single Circuit Steel H-Frame (DDE)





Existing Structure Type:  
230kV Single Circuit Wood H-Frame and Steel 3-Pole (Tangent)





---

Existing Structure Type:  
115kV Steel Lattice Frame (DDE)





---

Existing Structure Type:  
230kV Single Circuit Steel 3-Pole (DDE)





---

Existing Structure Type:  
230kV Double Circuit Steel Tower (Tangent)





---

Existing Structure Type:  
230kV Double Circuit Steel Tower (DDE)







Existing Structure Type:  
500kV Single Circuit Steel Tower (Tangent)







---

Existing Structure Type:  
500kV Single Circuit Steel Tower (DDE)





---

Existing Structure Type:  
500kV Single Circuit Steel Tower-Line Angle (DDE)







Proposed Structure Type:  
230kV Double Circuit Steel Monopole (Tangent)



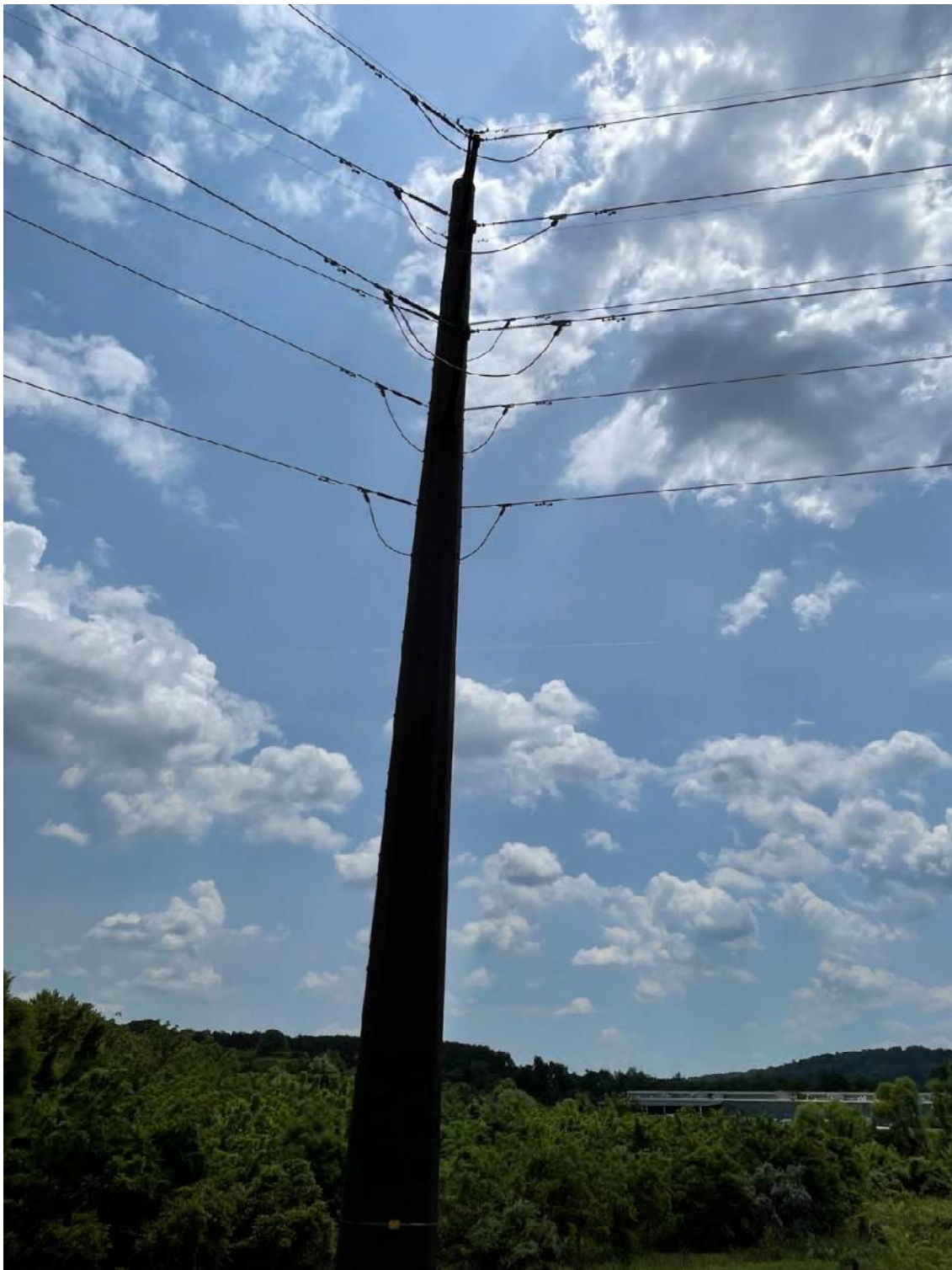
Proposed Structure Type:  
230kV Double Circuit Steel Monopole (DDE)





Proposed Structure Type:  
230kV Double Circuit Steel 2-Pole  
(DDE)





Proposed Structure Type:  
230kV Single Circuit Steel Monopole (DDE)



Proposed Structure Type:  
230kV Double Circuit Steel H-Frame (DDE)





Proposed Structure Type:  
230kV Single Circuit Steel Monopole (Tangent)







Proposed Structure Type:  
500kV Single Circuit Monopole  
(Tangent)





Proposed Structure Type:  
500kV Single Circuit H Frame  
(DDE)



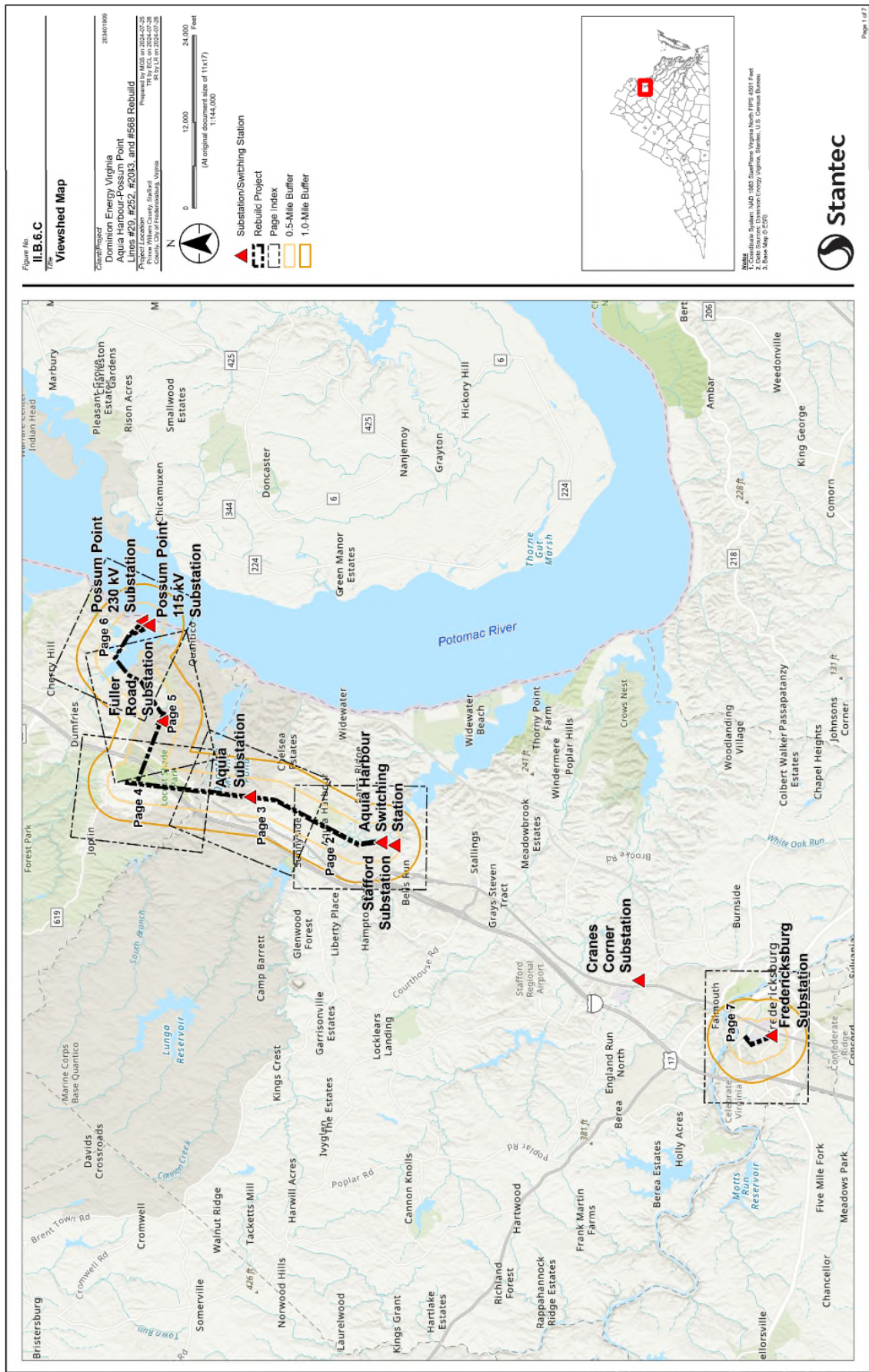


Proposed Structure Type:  
500kV Single Circuit Steel Monopole  
(DDE)

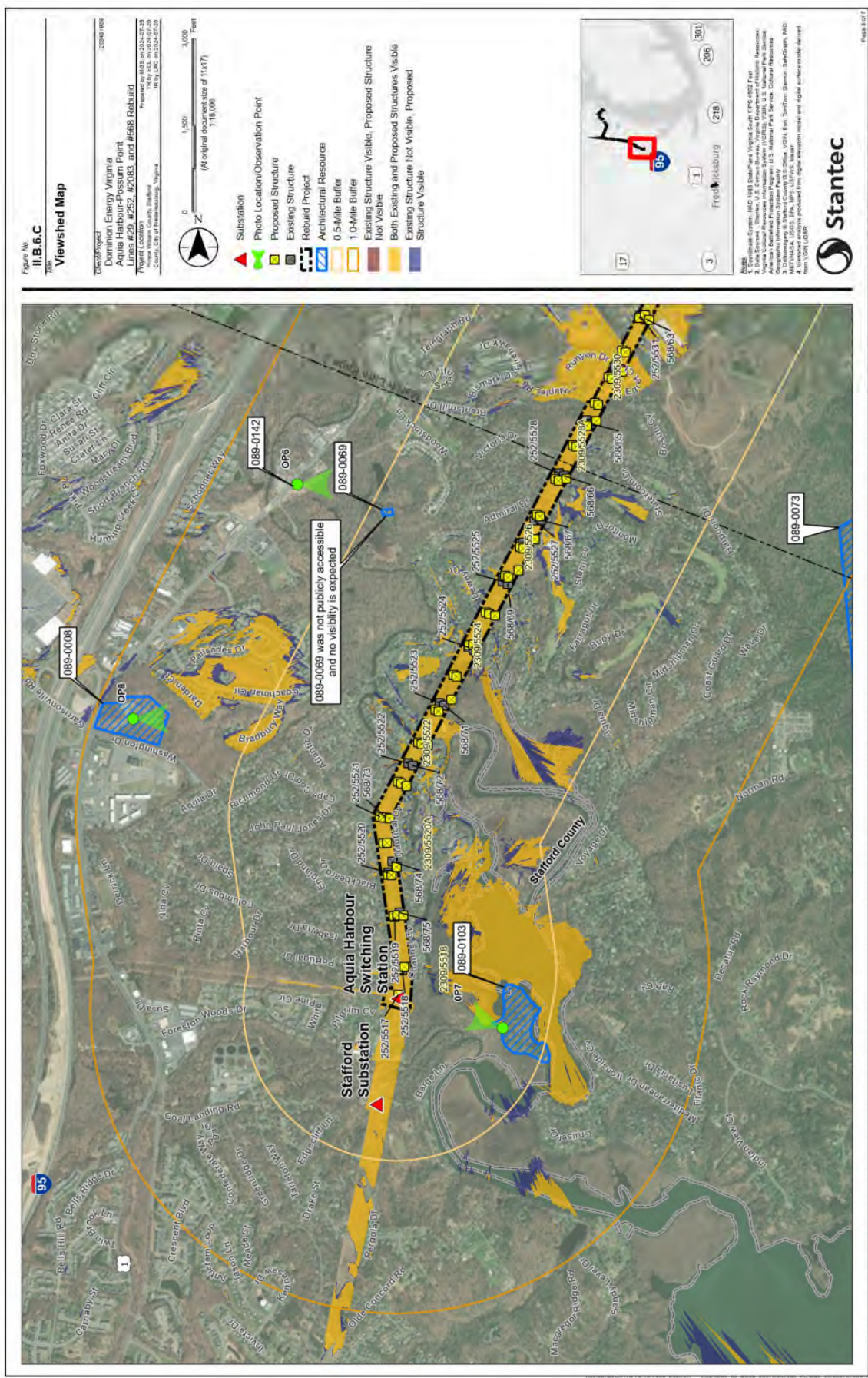












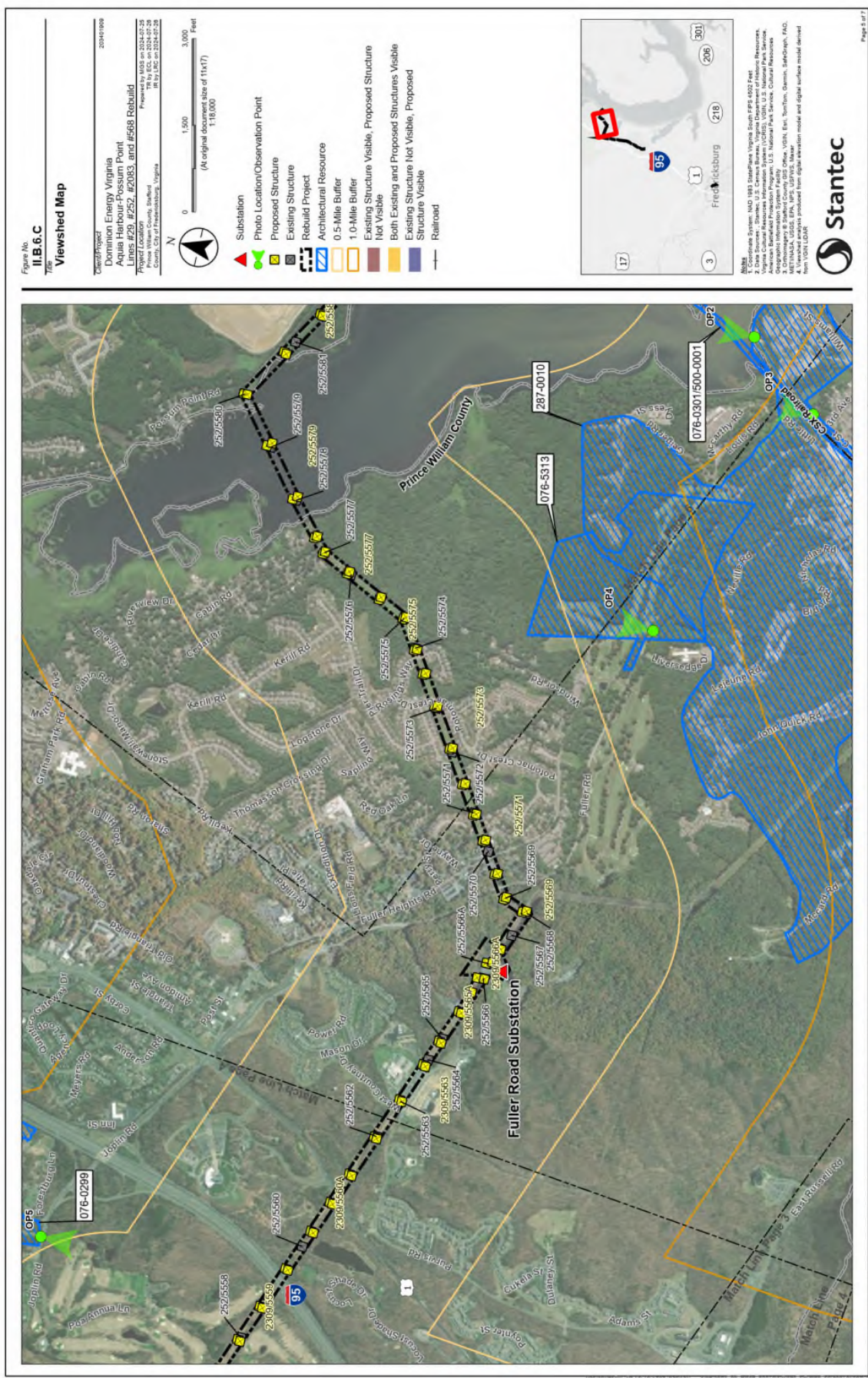




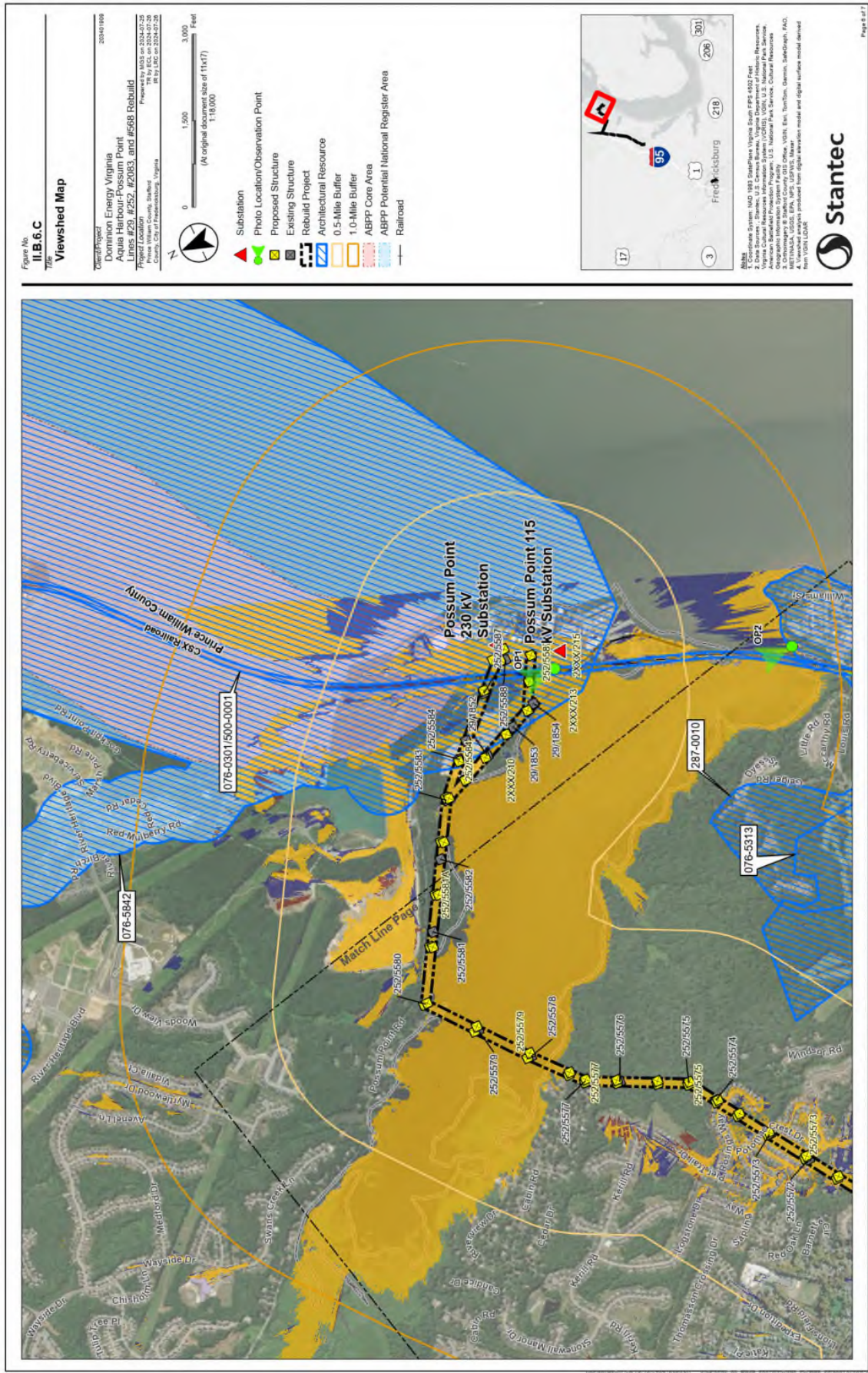




















OP01 – Existing

Photograph provided by Stantec

**OP 1 Existing**  
Richmond, Fredericksburg, and Potomac Railroad (DHR #076-0301  
& #500-0001), and Cockpit Point Battlefield (DHR #076-5842)

# OP01 – Proposed



**OP 1 Proposed**  
Richmond, Fredericksburg, and Potomac Railroad (DHR #076-0301  
& #500-0001), and Cockpit Point Battlefield (DHR #076-5842)

Simulation provided by Stantec



## OP02 – Existing



Photograph provided by Stantec

**OP 2 Existing**  
Quantico Marine Base Historic District (DHR #287-0010)



# OP02 – Proposed



Simulation provided by Stantec



**OP 2 Proposed**  
Quantico Marine Base Historic District (DHR #287-0010)



## OP03 – Existing



Photograph provided by Stantec

**OP 3 Existing**  
Town of Quantico Historic District (DHR #287-0010)



## OP03 – Proposed (No Visibility)



Simulation provided by Stantec

**OP 3 Proposed (No Visibility)**  
Town of Quantico Historic District (DHR #287-0010)



## OP04 – Existing



Photograph provided by Stantec

**OP 4 Existing**  
Camp French (DHR #076-5313)





Simulation provided by Stantec

**OP 4 Proposed (No Visibility)**  
Camp French (DHR #076-5313)

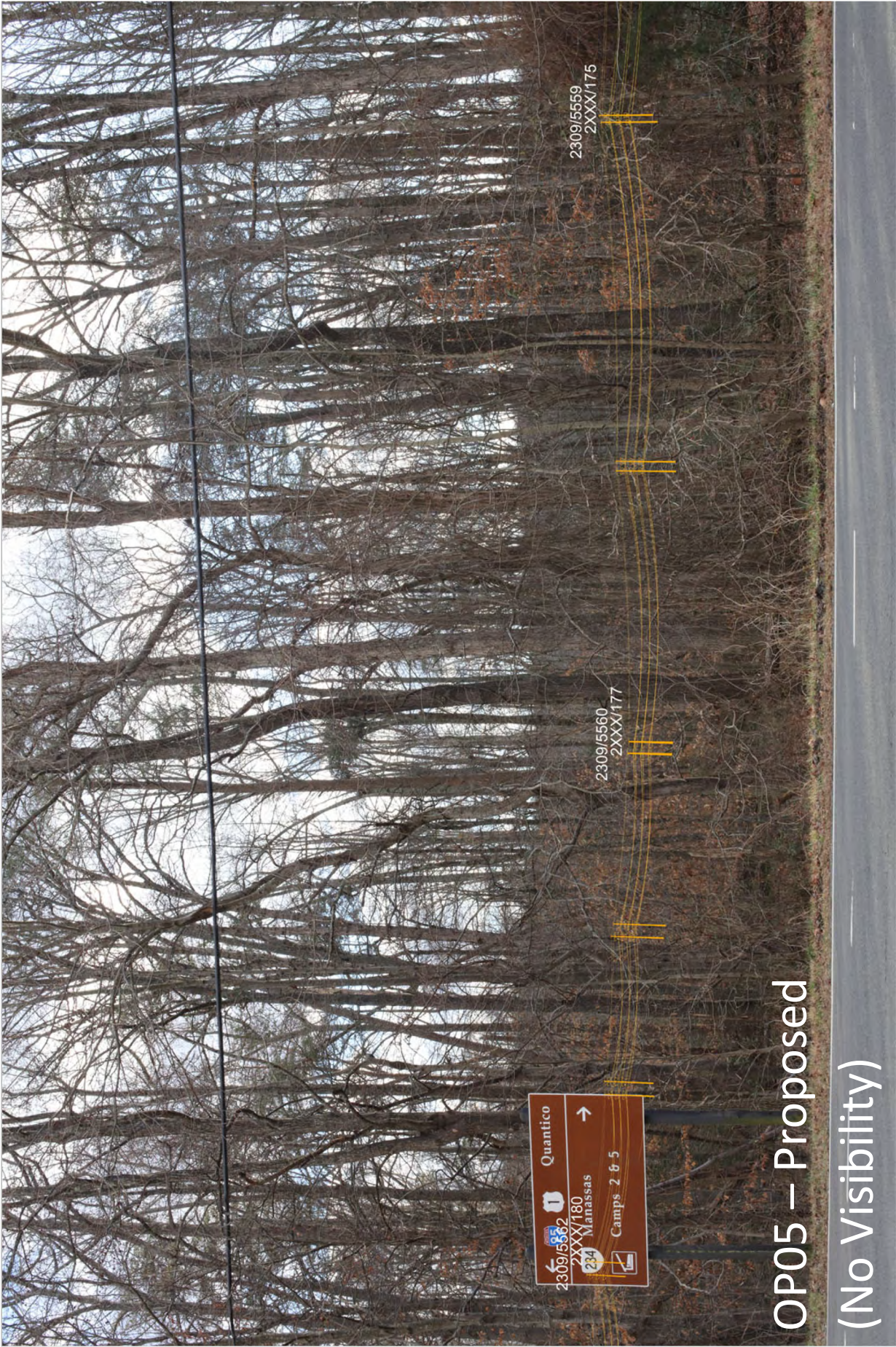




Photograph provided by Stantec

**OP 5 Existing**  
Chopawamsic Recreation Demonstration Area (DHR #076-0299)





**OP 5 Proposed (No Visibility)**  
Chopawamsic Recreation Demonstration Area (DHR #076-0299)

Simulation provided by Stantec





Photograph provided by Stantec

**OP 6 Existing**  
Crucifix Monument (DHR #089-0142)





Simulation provided by Stantec

**OP 6 Proposed (No Visibility)**  
Crucifix Monument (DHR #089-0142)



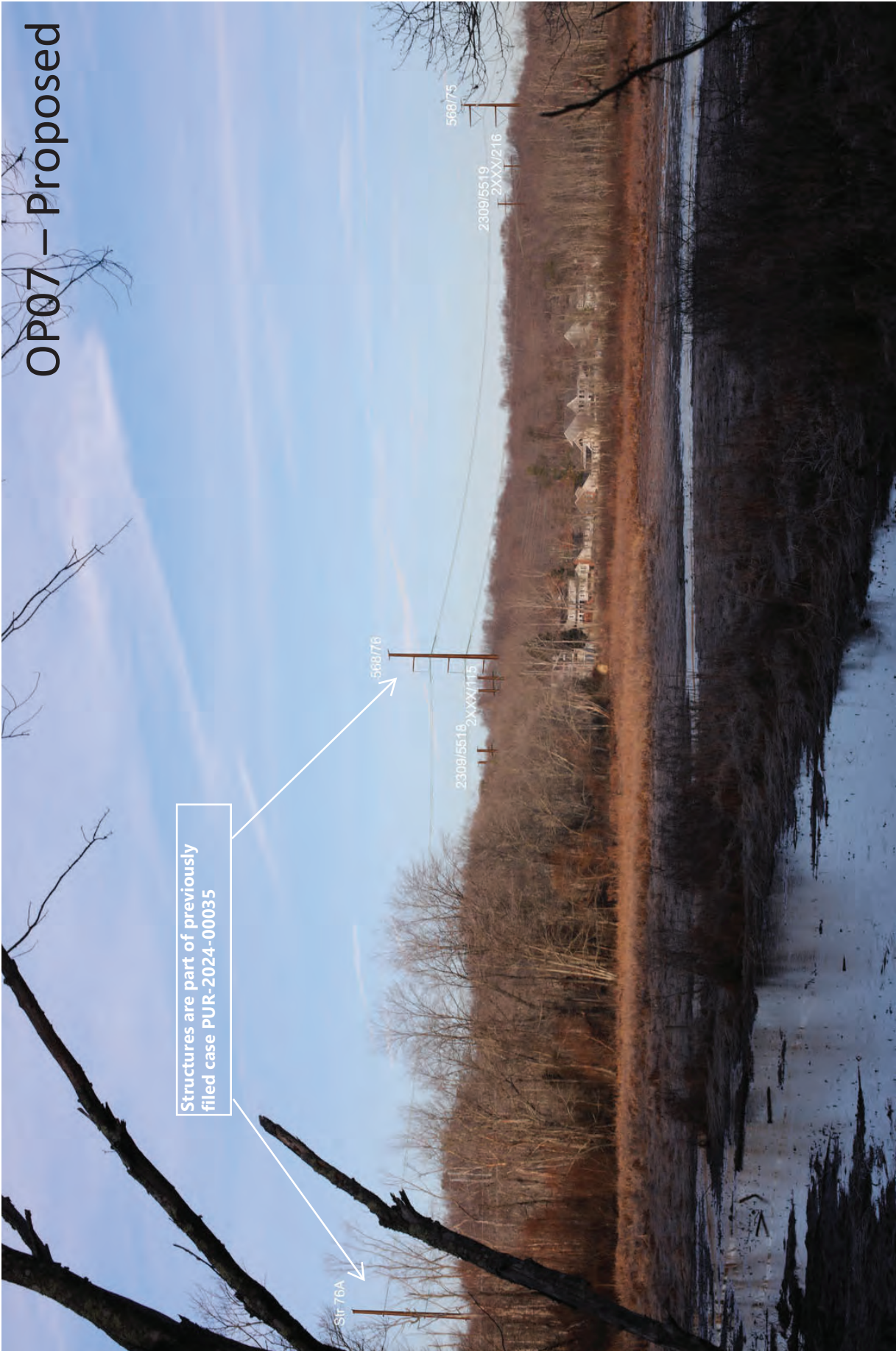
OP07 – Existing



Photograph provided by Stantec

**OP 7 Existing**  
Aquia Creek Quarries (DHR #089-0103)





Simulation provided by Stantec

**OP 7 Proposed**  
Aquia Creek Quarries (DHR #089-0103)





OP08 - Existing

Photograph provided by Stantec

OP 8 Existing  
Aquia Church (DHR #089-0008)





Simulation provided by Stantec

**OP 8 Proposed (No Visibility)**  
Aquia Church (DHR #089-0008)





OP12 – Existing

Photograph provided by Stantec

**OP 12 Existing**  
Chancellorsville Battlefield (DHR #088-5180) and Falmouth Historic District  
(DHR #089-0067)